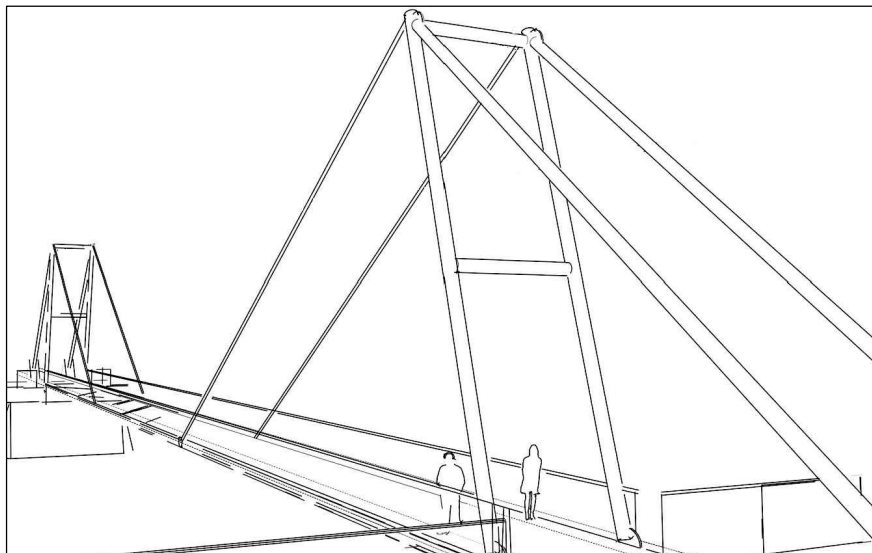


COMUNE DI FRONT



COSTRUZIONE DI PASSERELLA PEDONALE SUL TORRENTE MALONE

PROGETTO ESECUTIVO

Tavola:

E15

Relazione specialistica di calcolo
strutture di fondazione e geotecnica

prog. architettonico

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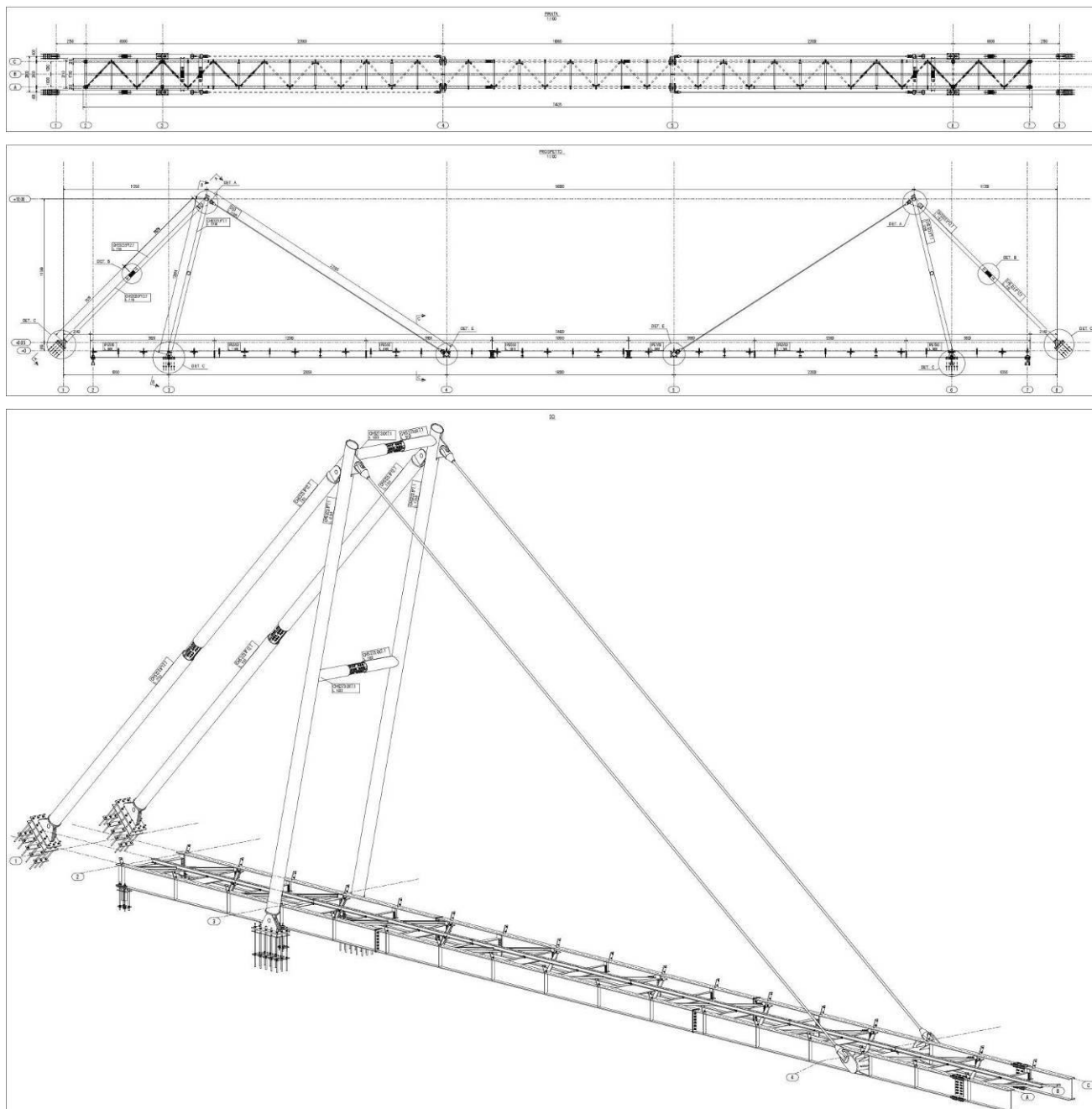
1. INTRODUZIONE

La presente relazione descrive le scelte progettuali, i dati di input e le verifiche delle strutture di fondazione a sostegno di una passerella strallata ciclopeditonale.

Il manufatto in oggetto fa parte di un più ampio progetto di ampliamento dei percorsi ciclabili e pedonali all'interno della Riserva Naturale del Parco della Vauda e serve per l'attraversamento del torrente Malone in adiacenza al ponte carrabile esistente al km 12.550 della s.p.13.

Si tratta di una passerella di 74 m di lunghezza a campata unica strallata di luce netta 62 m e 1.90 m larghezza.

Si riportano di seguito alcune immagini di progetto.



CONSIDERAZIONI PRELIMINARI

1.1. ELENCO ELABORATI GRAFICI

Questo documento è collegato e riferito ai seguenti elaborati grafici:

- Tav. 05-08

1.2. NORMATIVA DI RIFERIMENTO

L'analisi della struttura in oggetto verrà condotta utilizzando i metodi usuali della Scienza delle Costruzioni ed in conformità alle normative e leggi vigenti in Europa:

- D.M. 14 gennaio 2018: Nuove Norme Tecniche Per le Costruzioni;
- Circolare Esplicativa 21 gennaio 2019 n°7/C.S.LL.PP: Istruzioni per l'applicazione delle Norme Tecniche per le Costruzioni;
- UNI ENV 1991-1-4 – Eurocodice 1: Azioni sulle strutture.
- UNI ENV 1993-1-1 – Eurocodice 3: Progettazione delle strutture di acciaio.
- UNI ENV 1993-1-8 – Eurocodice 2: Progettazione delle strutture in calcestruzzo

1.3. CODICI DI CALCOLO

1.3.1. Software per le verifiche delle opere di fondazione e in calcestruzzo

Per il calcolo delle sollecitazioni e per la verifica di travi e pilastri in cemento armato si è fatto ricorso all'elaboratore elettronico utilizzando il seguente programma di calcolo:

DOLMEN WIN (R), versione 19.0 del 2019 prodotto, distribuito ed assistito dalla CDM DOLMEN srl, con sede in Torino, Via Drovetti 9/F.

Questa procedura è sviluppata in ambiente Windows, ed è stata scritta utilizzando i linguaggi Fortran e C. DOLMEN WIN permette l'analisi elastica lineare di strutture tridimensionali con nodi a sei gradi di libertà utilizzando un solutore ad elementi finiti. Gli elementi considerati sono la trave, con eventuali svincoli interni o rotazione attorno al proprio asse, ed il guscio, sia rettangolare che triangolare, avente comportamento di membrana e di piastra. I carichi possono essere applicati sia ai nodi, come forze o coppie concentrate, sia sulle travi, come forze distribuite, trapezie, concentrate, come coppie e come distorsioni termiche. I vincoli sono forniti tramite le sei costanti di rigidezza elastica.

A supporto del programma è fornito un ampio manuale d'uso contenente fra l'altro una vasta serie di test di validazione sia su esempi classici di Scienza delle Costruzioni, sia su strutture particolarmente impegnative e reperibili nella bibliografia specializzata.



1.4. UNITÀ DI MISURA

Le unità di misura utilizzate, dove non espressamente specificato vanno intese come di seguito:

Lunghezza:	m
Tempo:	s
Mass:	kg
Forza:	kN
Tensione:	MPa
Momenti:	kNm
Area:	m ²
Modulo elastico/plastico:	m ³
Momento d'inerzia:	m ⁴
Sezioni trasversali:	m ²

1.5. SISTEMA DI COORDINATE SPAZIALI

1.5.1. Sistema di riferimento globale

- Asse X: Lungo l'asse longitudinale del ponte
- Asse Y: Direzione trasversale
- Asse Z: Direzione verticale ("+" dal suolo verso il cielo)

1.6. PROPRIETÀ MECCANICHE DEI MATERIALI

Le proprietà meccaniche successive vengono usate nei calcoli.

1.6.1. calcestruzzo classe C12/15 per magrone

- resistenza a compressione cubica caratteristica	R_{ck}	=	15	N/mm ²
- resistenza a compressione cilindrica caratteristica	f_{ck}	=	12.4	N/mm ²
- resistenza a compressione cilindrica di calcolo	f_{cd}	=	7.0	N/mm ²
- modulo elastico secante	E	=	27.2	kN/mm ²
- coefficiente riduttivo per le resistenze a lunga durata	α_{cc}	=	0.85	
- coefficiente parziale di sicurezza per il cls	γ_c	=	1.50	

1.6.2. calcestruzzo classe C32/40 per opere in fondazione e in elevazione gettate in opera

- resistenza a compressione cubica caratteristica	R_{ck}	=	40	N/mm ²
- resistenza a compressione cilindrica caratteristica	f_{ck}	=	33.2	N/mm ²
- resistenza a compressione cilindrica di calcolo	f_{cd}	=	18.8	N/mm ²
- modulo elastico secante	E	=	33.6	kN/mm ²
- coefficiente riduttivo per le resistenze a lunga durata	α_{cc}	=	0.85	
- coefficiente parziale di sicurezza per il cls	γ_c	=	1.50	

1.6.3. acciaio B 450 C

- resistenza a trazione caratteristica	f_{tk}	=	540	N/mm ²
- tensione di snervamento caratteristica	f_{yk}	=	450	N/mm ²
- tensione di snervamento di calcolo	f_{yd}	=	391	N/mm ²
- modulo elastico medio	E_{sm}	=	210	kN/mm ²
- coefficiente parziale di sicurezza per l'acciaio	γ_s	=	1.15	

La passerella in progetto è in carpenteria metallica con schema a campata unica strallata e consente l'attraversamento dell'alveo del torrente Malone con distanza netta tra le sponde pari a 61.0m garantendo promiscuità di traffico pedonale con quello ciclabile grazie ad una sede viabile di larghezza 1,90 metri.

L'impalcato appoggia sulle spalle di sponda con interasse teorico di 62m e prosegue sul terreno limitrofo a bordo alveo per altri 6 m per parte prevedendo altre due coppe di appoggi. In campata sono presenti due traverse molto rigide tubolari aggettanti verso l'esterno del ponte a cui sono agganciate 2 coppie di stralli a fune tesata con diametro di 48mm che suddividono la luce in 3 campate di 22/18/22 m. Tali funi sono ancorate in sommità ad una coppia di portali trasversali alti 12m aggettanti verso l'alveo e controbilanciati da due coppie di tiranti passivi tubolari inclinati di 45° che riportano il carico in fondazione oltre al limite dell'impalcato.

Tutte le strutture in acciaio appoggiano sopra due basamenti in calcestruzzo (uno per sponda) direttamente appoggiati sul terreno e gettati in opera costituiti da una spalla profonda in corrispondenza del bordo alveo (a ripristino dell'argine) su cui poggiano i portali trasversali e la campata centrale dell'impalcato e da una parte più superficiale che si estende verso il terreno a bordo alveo per circa 10m su cui sono ancorati i tiranti posteriori e la parte restante dell'impalcato.



2.1. ANCORAGGI CON IL CEMENTO ARMATO

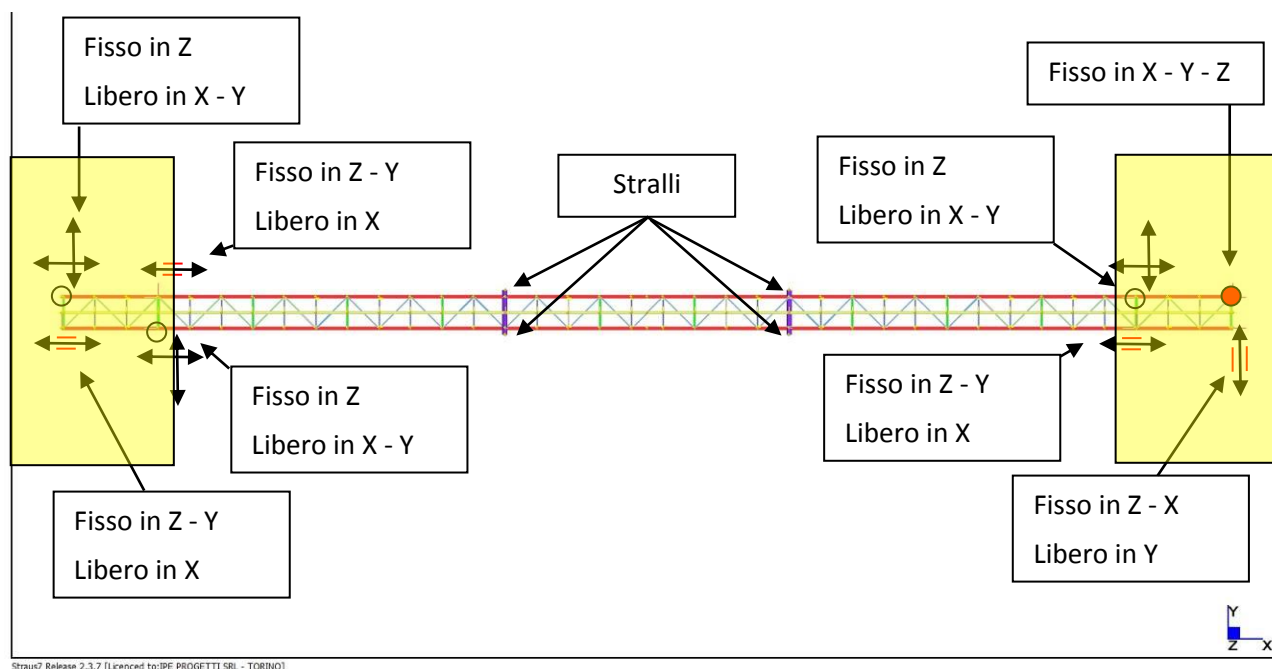
L'impalcato appoggia su blocchi in c.a. posti alle estremità dell'attraversamento con funzione di spalla e argine del torrente. Oltre alla campata centrale che appoggia direttamente sulla spalla sono presenti anche due campate esterne in continuità che si estendono oltre l'argine per ulteriori 6.0m per parte appoggiando a fine campata. Si individuano pertanto 4 appoggi per ciascun lato dell'impalcato.

In corrispondenza degli appoggi della campata centrale sono presenti anche i punti di ancoraggio del portale delegato a sorreggere gli stralli e i tiranti. Oltre le estremità dell'impalcato si collocano inoltre gli ancoraggi dei tiranti passivi posteriori che trovano allettamento in 4 costole rilevate con inclinazione concorde con i tiranti stessi.

2.1.1. Appoggi dell'impalcato

L'impalcato è costituito da 2 travi continue su 4 appoggi solidi e 2 appoggi cedevoli rappresentati dagli stralli. Gli appoggi rigidi sono stati ideati con opportuni gradi di svincolo longitudinale e trasversale in modo da non creare effetti iperstatici e consentire dilatazioni termiche libere.

Di seguito si riporta lo schema degli svincoli a traslazione.



Sul lato destro sono presenti gli unici due vincoli in direzione longitudinale e lungo l'impalcato si alternano vincoli liberi in entrambe le direzioni o solo longitudinalmente.

Lo svincolo è stato garantito progettando appoggi dotati di saponette di teflon che garantiscono spostamenti reciproci tra le piastre di ancoraggio a terra e le travi dell'impalcato asolando in modo opportuno i fori delle bullonature.

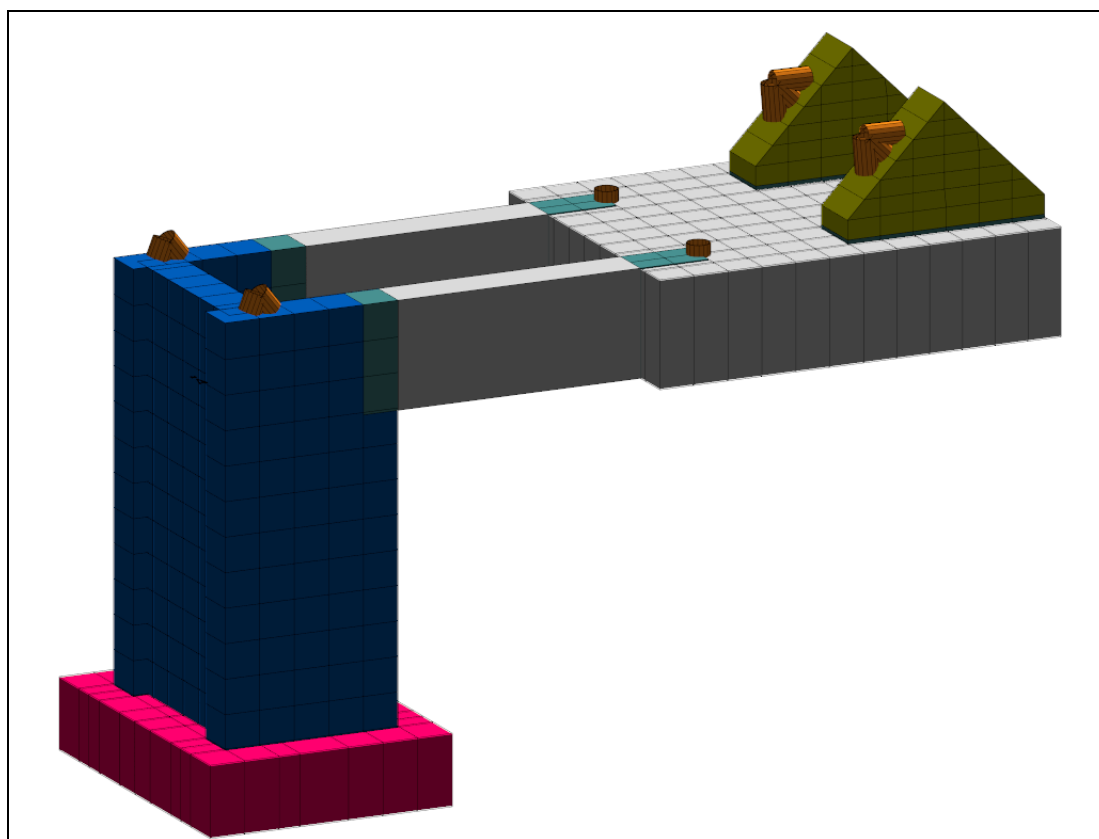
2.1.2. Appoggi del sistema stralli

Il sistema stralli è costituito da 2 portali incernierati alla base con funzione di antenne e da due coppie di tiranti passivi incernierati agli estremi (bielle) con funzione di controbilanciamento del tiro degli stralli costituiti invece da funi in acciaio armonico e tesati opportunamente per esigenze di deformazione.

2.2. STRUTTURA DI FONDAZIONE

I due blocchi di fondazione sono strutturati in modo da sostenere i carichi del manufatto e di assorbire le tensioni indotte dal tiro delle funi. Costruite in conglomerato cementizio armato gettato in opera sono costituite da:

- Plinto a quota inferiore disposto circa 1 m sotto il livello dell'alveo di dimensioni in pianta 460x310 cm e altezza di 100 cm
- paramento verticale che si sviluppa a partire dal plinto per un'altezza di 580 cm e possiede una forma a C rovesciata, costituendo il piano d'appoggio dei due profili tubolari che costituiscono le antenne;
- connessione del paramento verticale con il blocco di ancoraggio rappresentato da un plinto alto 150 cm con dimensioni in pianta pari a 580x460 cm; tale connessione è composta da due travi 60x150 in grado di assorbire il momento generato dall'azione di tiro dei diagonali posteriori
- dalla faccia superiore del blocco d'ancoraggio è prevista la realizzazione di una sporgenza in calcestruzzo armato in cui saranno fissati i tirafondi dei profili tubolari connessi alle antenne, che contrastano il tiro indotto dalle funi, a loro volta connesse con l'impalcato. Tali sporgenze saranno interamente fuori terra e, pertanto, ne è stato previsto il getto con casseri adeguati ad un cemento con finitura superficiale di faccia a vista.



3. DESCRIZIONE DEL MODELLO FEM

3.1. SCHEMATIZZAZIONE DELLA STRUTTURA E DEI VINCOLI

I materiali che costituiscono la struttura sono considerati con il comportamento lineare elastico.

La struttura è stata schematizzata escludendo il contributo degli elementi aventi rigidità e resistenza trascurabili a fronte dei principali. E' quindi stata eseguita una modellazione tridimensionale di tutti gli elementi costituenti la struttura primaria e la struttura secondaria eccetto gli elementi dei parapetti che sono stati introdotti esclusivamente come carichi nodali e dei grigliati inseriti come carico di superficie.

Sono stati utilizzati esclusivamente elementi monodimensionali di tipo "beam" per le travi principali e secondarie e "truss" per gli elementi di controvento considerati reagenti anche a compressione. Gli stralli sono stati schematizzati con elementi "cable" con modulo elastico ridotto e comportamento non lineare.

I vincoli sono tutti di tipo puntuale e inseriti agendo sulle 6 costanti di rigidità.

I carichi sono stati applicati mediante forze nodali o lineari su elementi trave e mediante aree di carico.

3.2. SCHEMATIZZAZIONE DELLE AZIONI

In accordo con le sopracitate normative, sono state considerate nei calcoli le seguenti azioni:

- Pesi propri strutturali;
- Carichi permanenti portati dalla struttura (grigliato e parapetto);
- Carichi variabili di esercizio (carico di traffico da ponte con schema n.5 folla compatta e vento)
- Carichi termici

Ciascuna azione viene caricata sulla struttura tramite:

- Massa propria dell'elemento calcolata in automatico dal software tramite applicazione del peso specifico;
- Carichi di linea per l'applicazione del peso del parapetto e del carico vento trasversale
- Carichi di superficie per l'applicazione del carico di traffico
- Delta termico sulle aste
- Combinazione quadratica degli auto vettori calcolati con analisi dinamica modale per i carichi sismici.

3.3. TIPO DI ANALISI

Il modello della sovrastruttura è stato calcolato adottando l'analisi statica non lineare per la determinazione delle sollecitazioni statiche e l'analisi dinamica modale per la determinazione delle sollecitazioni sismiche. Le sollecitazioni sismiche, una volta calcolate sono state caricate come forze nodali inerziali all'interno di specifici casi di carico per poterne poi performare l'analisi di tipo non lineare.

È stata considerata la non linearità sia geometrica sia del materiale per tenere in conto degli effetti della catenaria.

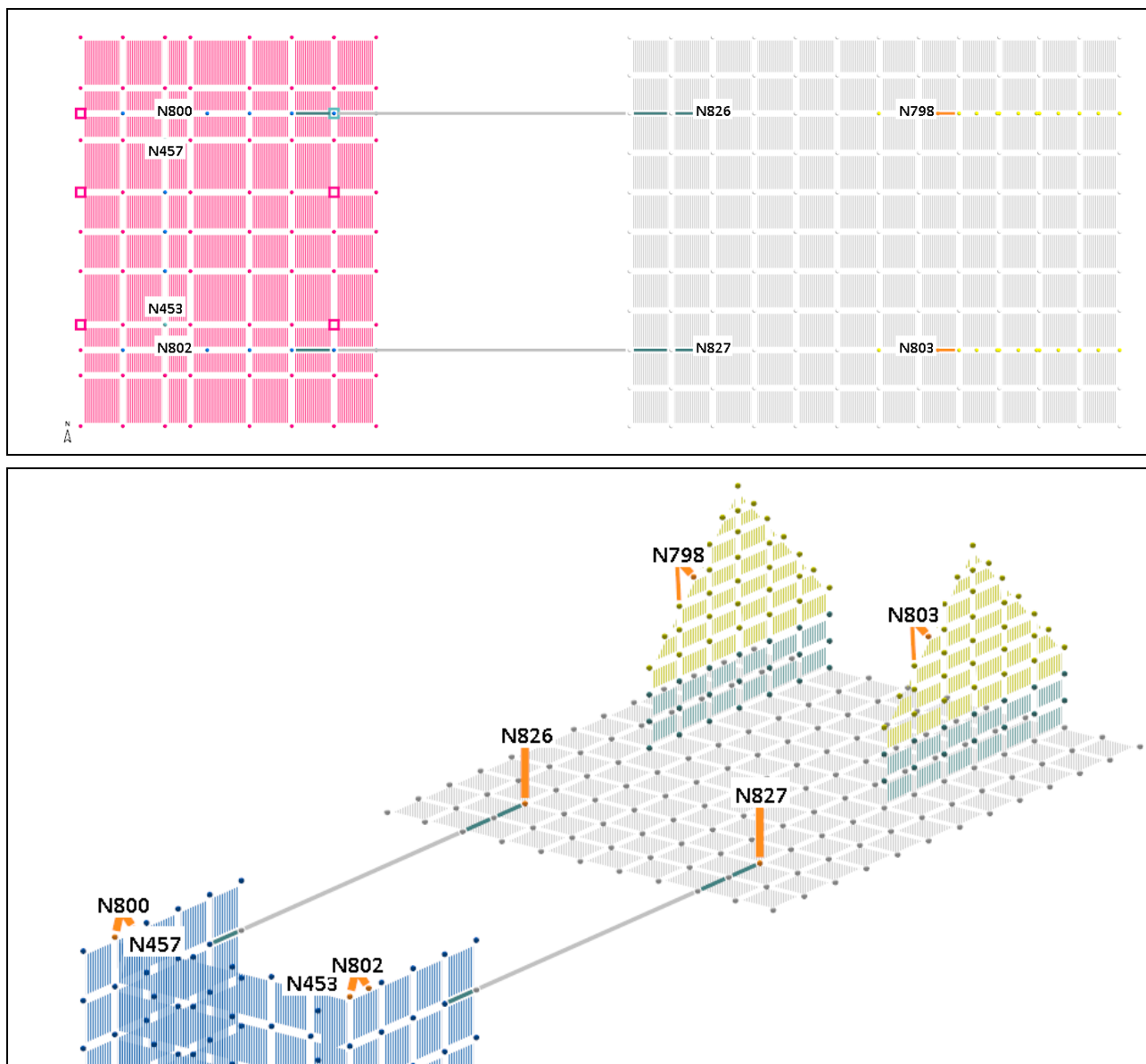
Per quanto riguarda la verifica delle fondazioni si sono analizzate le reazioni vincolari derivante dal modello sopra descritto e sono state prese in considerazione solo quelle dimensionanti per le fondazioni stesse.

L'elenco dei casi considerati è rilevabile dal paragrafo successivo casi di carico.

Il comportamento globale è verificato se i singoli corpi sono verificati. Il calcolo è stato eseguito secondo le normative sopra citate sfruttando principi delle scienze delle costruzioni.

3.4. SCHEMA DELLA STRUTTURA E DEI VINCOLI

Nel seguito vengono riportate delle immagini riepilogative della numerazione dei nodi di interfaccia con le strutture in acciaio.



Di seguito è indicata la corrispondenza tra la numerazione del modello Dolmen per il calcolo delle fondazioni con la numerazione del modello straus per il calcolo della sovrastruttura in acciaio

Nodi Dolmen	Nodi Straus
457	Node 3
453	Node 108
798	Node 117
803	Node 118
826	Node 123
827	Node 124
802	Node 125
800	Node 126

4. REAZIONI VINCOLARI DA MODELLO FEM SOVRASTRUTTURA

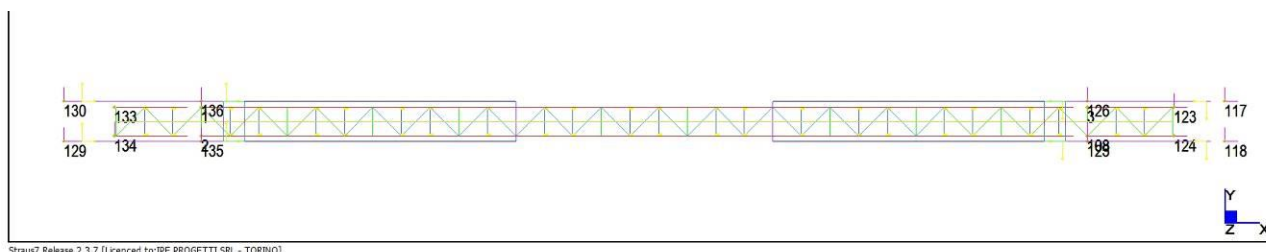
In questo paragrafo riportiamo la progettazione e la verifica dei giunti di base della struttura principale.

4.1. REAZIONI VINCOLARI NEL SISTEMA DI RIFERIMENTO GLOBALE

Nelle seguenti due tabelle vengono mostrati i valori massimi e minimi delle reazioni vincolari (R_x , R_y , R_z), registrate per tutti gli 8+8 punti di vincolo, nelle combinazioni SLU SLE e SLV oltre che nei singoli casi di carico. Tali reazioni sono riferite al sistema di riferimento globale.

Si specifica che i valori mostrati sono le reazioni vincolari applicate dalla fondazione alla struttura d'acciaio come risposta alle forze provenienti dalla struttura stessa. (Ad esempio un segno Z positivo significa che la struttura in acciaio applica una forza di compressione alla fondazione e un segno Z negativo significa che la struttura in acciaio applica una forza di trazione alla fondazione).

4.1.1. Pianta nodi



4.1.2. Reazioni vincolari per casi di carico

	FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Node 1: 1: Peso Proprio	0	0	19	0	0	0
Node 1: 2: Permanenti	0	0	8	0	0	0
Node 1: 3: Vento Y	0	-194	-8	0	0	0
Node 1: 4: VAR DX	0	2	19	0	0	0
Node 1: 5: VAR SX	0	-2	69	0	0	0
Node 1: 6: DT+	0	-2	-5	0	0	0
Node 1: 7: DT-	0	3	-24	0	0	0
Node 2: 1: Peso Proprio	0	0	19	0	0	0
Node 2: 2: Permanenti	0	0	8	0	0	0
Node 2: 3: Vento Y	0	0	-11	0	0	0
Node 2: 4: VAR DX	0	0	69	0	0	0
Node 2: 5: VAR SX	0	0	19	0	0	0
Node 2: 6: DT+	0	0	-5	0	0	0
Node 2: 7: DT-	0	0	-24	0	0	0
Node 3: 1: Peso Proprio	0	0	19	0	0	0
Node 3: 2: Permanenti	0	0	8	0	0	0
Node 3: 3: Vento Y	0	0	-8	0	0	0
Node 3: 4: VAR DX	0	0	18	0	0	0
Node 3: 5: VAR SX	0	0	68	0	0	0
Node 3: 6: DT+	0	0	-10	0	0	0
Node 3: 7: DT-	0	0	-13	0	0	0
Node 108: 1: Peso Proprio	0	0	19	0	0	0
Node 108: 2: Permanenti	0	0	8	0	0	0
Node 108: 3: Vento Y	0	-140	-11	0	0	0
Node 108: 4: VAR DX	0	1	68	0	0	0
Node 108: 5: VAR SX	0	-1	18	0	0	0
Node 108: 6: DT+	0	6	-10	0	0	0
Node 108: 7: DT-	0	-10	-13	0	0	0
Node 117: 1: Peso Proprio	81	0	-67	0	0	0
Node 117: 2: Permanenti	47	0	-43	0	0	0
Node 117: 3: Vento Y	9	-3	-8	0	0	0

Node 117: 4: VAR DX	84	0	-77	0	0	0
Node 117: 5: VAR SX	165	0	-152	0	0	0
Node 117: 6: DT+	12	0	-11	0	0	0
Node 117: 7: DT-	0	0	0	0	0	0
Node 118: 1: Peso Proprio	81	0	-67	0	0	0
Node 118: 2: Permanenti	47	0	-43	0	0	0
Node 118: 3: Vento Y	5	-4	-5	0	0	0
Node 118: 4: VAR DX	165	0	-152	0	0	0
Node 118: 5: VAR SX	84	0	-77	0	0	0
Node 118: 6: DT+	12	0	-11	0	0	0
Node 118: 7: DT-	0	0	0	0	0	0
Node 123: 1: Peso Proprio	0	0	2	0	0	0
Node 123: 2: Permanenti	0	0	3	0	0	0
Node 123: 3: Vento Y	-232	41	6	0	0	0
Node 123: 4: VAR DX	5	-1	1	0	0	0
Node 123: 5: VAR SX	-5	1	-7	0	0	0
Node 123: 6: DT+	-20	-5	7	0	0	0
Node 123: 7: DT-	42	10	9	0	0	0
Node 124: 1: Peso Proprio	0	0	2	0	0	0
Node 124: 2: Permanenti	0	0	3	0	0	0
Node 124: 3: Vento Y	232	0	7	0	0	0
Node 124: 4: VAR DX	-6	0	-7	0	0	0
Node 124: 5: VAR SX	5	0	1	0	0	0
Node 124: 6: DT+	5	0	7	0	0	0
Node 124: 7: DT-	-4	0	9	0	0	0
Node 125: 1: Peso Proprio	-30	0	124	0	0	0
Node 125: 2: Permanenti	-16	0	63	0	0	0
Node 125: 3: Vento Y	10	-9	-43	0	0	0
Node 125: 4: VAR DX	-55	0	221	0	0	0
Node 125: 5: VAR SX	-28	0	112	0	0	0
Node 125: 6: DT+	-4	0	15	0	0	0
Node 125: 7: DT-	0	0	0	0	0	0
Node 126: 1: Peso Proprio	-30	0	124	0	0	0
Node 126: 2: Permanenti	-16	0	63	0	0	0
Node 126: 3: Vento Y	-15	-8	62	0	0	0
Node 126: 4: VAR DX	-28	0	112	0	0	0
Node 126: 5: VAR SX	-55	0	221	0	0	0
Node 126: 6: DT+	-4	0	15	0	0	0
Node 126: 7: DT-	0	0	0	0	0	0
Node 129: 1: Peso Proprio	-81	0	-66	0	0	0
Node 129: 2: Permanenti	-47	0	-43	0	0	0
Node 129: 3: Vento Y	-5	-4	-5	0	0	0
Node 129: 4: VAR DX	-164	0	-152	0	0	0
Node 129: 5: VAR SX	-83	0	-77	0	0	0
Node 129: 6: DT+	0	0	0	0	0	0
Node 129: 7: DT-	-28	0	-26	0	0	0
Node 130: 1: Peso Proprio	-81	0	-66	0	0	0
Node 130: 2: Permanenti	-47	0	-43	0	0	0
Node 130: 3: Vento Y	-10	-3	-9	0	0	0
Node 130: 4: VAR DX	-83	0	-77	0	0	0
Node 130: 5: VAR SX	-164	0	-152	0	0	0
Node 130: 6: DT+	0	0	0	0	0	0
Node 130: 7: DT-	-28	0	-26	0	0	0
Node 133: 1: Peso Proprio	0	0	2	0	0	0
Node 133: 2: Permanenti	0	0	3	0	0	0
Node 133: 3: Vento Y	0	0	6	0	0	0
Node 133: 4: VAR DX	0	0	1	0	0	0
Node 133: 5: VAR SX	0	0	-7	0	0	0
Node 133: 6: DT+	0	0	4	0	0	0
Node 133: 7: DT-	0	0	16	0	0	0
Node 134: 1: Peso Proprio	0	0	2	0	0	0
Node 134: 2: Permanenti	0	0	3	0	0	0
Node 134: 3: Vento Y	0	98	7	0	0	0
Node 134: 4: VAR DX	0	-2	-7	0	0	0

Node 134: 5: VAR SX	0	2	1	0	0	0
Node 134: 6: DT+	0	2	4	0	0	0
Node 134: 7: DT-	0	-3	16	0	0	0
Node 135: 1: Peso Proprio	30	0	124	0	0	0
Node 135: 2: Permanenti	16	0	62	0	0	0
Node 135: 3: Vento Y	-10	-9	-43	0	0	0
Node 135: 4: VAR DX	55	0	220	0	0	0
Node 135: 5: VAR SX	28	0	111	0	0	0
Node 135: 6: DT+	0	0	0	0	0	0
Node 135: 7: DT-	9	0	37	0	0	0
Node 136: 1: Peso Proprio	30	0	124	0	0	0
Node 136: 2: Permanenti	16	0	62	0	0	0
Node 136: 3: Vento Y	15	-8	62	0	0	0
Node 136: 4: VAR DX	28	0	111	0	0	0
Node 136: 5: VAR SX	55	0	220	0	0	0
Node 136: 6: DT+	0	0	0	0	0	0
Node 136: 7: DT-	9	0	37	0	0	0

4.1.3. Reazioni vincolari SLE

	FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Node 1: 8: SLE full	0	0	144	0	0	0
Node 1: 9: SLEr T1+	0	-119	148	0	0	0
Node 1: 10: SLEr T1-	0	-116	134	0	0	0
Node 1: 11: SLEr T2+	0	-117	70	0	0	0
Node 1: 12: SLEr T2-	0	-113	56	0	0	0
Node 1: 13: SLEr T3+	0	-119	63	0	0	0
Node 1: 14: SLEr T3-	0	-116	49	0	0	0
Node 1: 15: SLEr T4+	0	-116	110	0	0	0
Node 1: 16: SLEr T4-	0	-113	96	0	0	0
Node 1: 17: SLEr T5+	0	-118	153	0	0	0
Node 1: 18: SLEr T5-	0	-115	139	0	0	0
Node 1: 19: SLEr V+	0	-196	43	0	0	0
Node 1: 20: SLEr V-	0	-193	29	0	0	0
Node 1: 21: SLEr DT+	0	-119	46	0	0	0
Node 1: 22: SLEr DT-	0	-114	22	0	0	0
Node 1: 23: SLEf V+	0	-40	42	0	0	0
Node 1: 24: SLEf V-	0	-37	30	0	0	0
Node 1: 25: SLEf DT+	0	-1	42	0	0	0
Node 1: 26: SLEf DT-	0	2	28	0	0	0
Node 1: 27: SLEqp	0	0	37	0	0	0
Node 2: 8: SLE full	0	0	144	0	0	0
Node 2: 9: SLEr T1+	0	0	150	0	0	0
Node 2: 10: SLEr T1-	0	0	135	0	0	0
Node 2: 11: SLEr T2+	0	0	121	0	0	0
Node 2: 12: SLEr T2-	0	0	106	0	0	0
Node 2: 13: SLEr T3+	0	0	64	0	0	0
Node 2: 14: SLEr T3-	0	0	48	0	0	0
Node 2: 15: SLEr T4+	0	0	82	0	0	0
Node 2: 16: SLEr T4-	0	0	66	0	0	0
Node 2: 17: SLEr T5+	0	0	155	0	0	0
Node 2: 18: SLEr T5-	0	0	140	0	0	0
Node 2: 19: SLEr V+	0	0	42	0	0	0
Node 2: 20: SLEr V-	0	0	27	0	0	0
Node 2: 21: SLEr DT+	0	0	46	0	0	0
Node 2: 22: SLEr DT-	0	0	21	0	0	0
Node 2: 23: SLEf V+	0	0	42	0	0	0
Node 2: 24: SLEf V-	0	0	29	0	0	0
Node 2: 25: SLEf DT+	0	0	42	0	0	0
Node 2: 26: SLEf DT-	0	0	28	0	0	0
Node 2: 27: SLEqp	0	0	37	0	0	0
Node 3: 8: SLE full	0	0	144	0	0	0

Node 3: 9: SLer T1+	0	0	142	0	0	0
Node 3: 10: SLer T1-	0	0	144	0	0	0
Node 3: 11: SLer T2+	0	0	64	0	0	0
Node 3: 12: SLer T2-	0	0	67	0	0	0
Node 3: 13: SLer T3+	0	0	57	0	0	0
Node 3: 14: SLer T3-	0	0	59	0	0	0
Node 3: 15: SLer T4+	0	0	104	0	0	0
Node 3: 16: SLer T4-	0	0	107	0	0	0
Node 3: 17: SLer T5+	0	0	32	0	0	0
Node 3: 18: SLer T5-	0	0	34	0	0	0
Node 3: 19: SLer V+	0	0	37	0	0	0
Node 3: 20: SLer V-	0	0	39	0	0	0
Node 3: 21: SLer DT+	0	0	36	0	0	0
Node 3: 22: SLer DT-	0	0	40	0	0	0
Node 3: 23: SLEf V+	0	0	36	0	0	0
Node 3: 24: SLEf V-	0	0	38	0	0	0
Node 3: 25: SLEf DT+	0	0	36	0	0	0
Node 3: 26: SLEf DT-	0	0	39	0	0	0
Node 3: 27: SLEqp	0	0	37	0	0	0
Node 108: 8: SLE full	0	0	144	0	0	0
Node 108: 9: SLer T1+	0	-82	144	0	0	0
Node 108: 10: SLer T1-	0	-91	146	0	0	0
Node 108: 11: SLer T2+	0	-80	115	0	0	0
Node 108: 12: SLer T2-	0	-90	117	0	0	0
Node 108: 13: SLer T3+	0	-81	57	0	0	0
Node 108: 14: SLer T3-	0	-91	59	0	0	0
Node 108: 15: SLer T4+	0	-80	75	0	0	0
Node 108: 16: SLer T4-	0	-90	78	0	0	0
Node 108: 17: SLer T5+	0	-83	31	0	0	0
Node 108: 18: SLer T5-	0	-93	34	0	0	0
Node 108: 19: SLer V+	0	-137	36	0	0	0
Node 108: 20: SLer V-	0	-147	38	0	0	0
Node 108: 21: SLer DT+	0	-79	35	0	0	0
Node 108: 22: SLer DT-	0	-95	40	0	0	0
Node 108: 23: SLEf V+	0	-25	36	0	0	0
Node 108: 24: SLEf V-	0	-33	38	0	0	0
Node 108: 25: SLEf DT+	0	3	36	0	0	0
Node 108: 26: SLEf DT-	0	-6	39	0	0	0
Node 108: 27: SLEqp	0	0	37	0	0	0
Node 117: 8: SLE full	354	0	-318	0	0	0
Node 117: 9: SLer T1+	362	-3	-326	0	0	0
Node 117: 10: SLer T1-	344	-3	-308	0	0	0
Node 117: 11: SLer T2+	205	-2	-181	0	0	0
Node 117: 12: SLer T2-	187	-2	-164	0	0	0
Node 117: 13: SLer T3+	305	-3	-273	0	0	0
Node 117: 14: SLer T3-	287	-3	-256	0	0	0
Node 117: 15: SLer T4+	226	-2	-200	0	0	0
Node 117: 16: SLer T4-	208	-2	-183	0	0	0
Node 117: 17: SLer T5+	153	-2	-133	0	0	0
Node 117: 18: SLer T5-	135	-2	-117	0	0	0
Node 117: 19: SLer V+	129	-3	-111	0	0	0
Node 117: 20: SLer V-	111	-3	-94	0	0	0
Node 117: 21: SLer DT+	132	-2	-113	0	0	0
Node 117: 22: SLer DT-	103	-2	-87	0	0	0
Node 117: 23: SLEf V+	126	-1	-108	0	0	0
Node 117: 24: SLEf V-	112	-1	-95	0	0	0
Node 117: 25: SLEf DT+	126	0	-108	0	0	0
Node 117: 26: SLEf DT-	109	0	-93	0	0	0
Node 117: 27: SLEqp	120	0	-103	0	0	0
Node 118: 8: SLE full	354	0	-318	0	0	0
Node 118: 9: SLer T1+	358	-4	-322	0	0	0
Node 118: 10: SLer T1-	340	-4	-305	0	0	0
Node 118: 11: SLer T2+	282	-3	-252	0	0	0
Node 118: 12: SLer T2-	264	-3	-235	0	0	0
Node 118: 13: SLer T3+	303	-4	-271	0	0	0

Node 118: 14: SLer T3-	285	-4	-254	0	0	0
Node 118: 15: SLer T4+	261	-3	-232	0	0	0
Node 118: 16: SLer T4-	243	-3	-216	0	0	0
Node 118: 17: SLer T5+	150	-3	-130	0	0	0
Node 118: 18: SLer T5-	132	-3	-113	0	0	0
Node 118: 19: SLer V+	124	-5	-106	0	0	0
Node 118: 20: SLer V-	107	-5	-90	0	0	0
Node 118: 21: SLer DT+	129	-3	-110	0	0	0
Node 118: 22: SLer DT-	100	-3	-84	0	0	0
Node 118: 23: SLEf V+	125	-1	-107	0	0	0
Node 118: 24: SLEf V-	111	-1	-94	0	0	0
Node 118: 25: SLEf DT+	126	0	-108	0	0	0
Node 118: 26: SLEf DT-	109	0	-92	0	0	0
Node 118: 27: SLEqp	120	0	-103	0	0	0
Node 123: 8: SLE full	-1	0	-21	0	0	0
Node 123: 9: SLer T1+	-161	22	-21	0	0	0
Node 123: 10: SLer T1-	-107	31	-22	0	0	0
Node 123: 11: SLer T2+	-156	20	-7	0	0	0
Node 123: 12: SLer T2-	-103	30	-8	0	0	0
Node 123: 13: SLer T3+	-160	21	9	0	0	0
Node 123: 14: SLer T3-	-107	31	8	0	0	0
Node 123: 15: SLer T4+	-154	20	-21	0	0	0
Node 123: 16: SLer T4-	-100	29	-21	0	0	0
Node 123: 17: SLer T5+	-32	23	1	0	0	0
Node 123: 18: SLer T5-	21	32	0	0	0	0
Node 123: 19: SLer V+	-251	38	-2	0	0	0
Node 123: 20: SLer V-	-200	47	-2	0	0	0
Node 123: 21: SLer DT+	-170	19	-1	0	0	0
Node 123: 22: SLer DT-	-85	34	-2	0	0	0
Node 123: 23: SLEf V+	-62	5	-1	0	0	0
Node 123: 24: SLEf V-	-19	13	-2	0	0	0
Node 123: 25: SLEf DT+	-18	-3	-1	0	0	0
Node 123: 26: SLEf DT-	33	6	-2	0	0	0
Node 123: 27: SLEqp	0	0	-1	0	0	0
Node 124: 8: SLE full	-1	0	-21	0	0	0
Node 124: 9: SLer T1+	137	0	-20	0	0	0
Node 124: 10: SLer T1-	146	0	-21	0	0	0
Node 124: 11: SLer T2+	132	0	-14	0	0	0
Node 124: 12: SLer T2-	142	0	-15	0	0	0
Node 124: 13: SLer T3+	136	0	10	0	0	0
Node 124: 14: SLer T3-	145	0	9	0	0	0
Node 124: 15: SLer T4+	130	0	-1	0	0	0
Node 124: 16: SLer T4-	139	0	-2	0	0	0
Node 124: 17: SLer T5+	253	0	2	0	0	0
Node 124: 18: SLer T5-	262	0	1	0	0	0
Node 124: 19: SLer V+	230	0	-1	0	0	0
Node 124: 20: SLer V-	237	0	-2	0	0	0
Node 124: 21: SLer DT+	135	0	-1	0	0	0
Node 124: 22: SLer DT-	148	0	-2	0	0	0
Node 124: 23: SLEf V+	44	0	-1	0	0	0
Node 124: 24: SLEf V-	50	0	-2	0	0	0
Node 124: 25: SLEf DT+	-3	0	-1	0	0	0
Node 124: 26: SLEf DT-	4	0	-2	0	0	0
Node 124: 27: SLEqp	0	0	-1	0	0	0
Node 125: 8: SLE full	-122	0	488	0	0	0
Node 125: 9: SLer T1+	-115	-4	462	0	0	0
Node 125: 10: SLer T1-	-109	-4	438	0	0	0
Node 125: 11: SLer T2+	-90	-4	362	0	0	0
Node 125: 12: SLer T2-	-84	-4	338	0	0	0
Node 125: 13: SLer T3+	-97	-4	388	0	0	0
Node 125: 14: SLer T3-	-91	-4	365	0	0	0
Node 125: 15: SLer T4+	-83	-4	333	0	0	0
Node 125: 16: SLer T4-	-77	-4	309	0	0	0
Node 125: 17: SLer T5+	-46	-5	185	0	0	0
Node 125: 18: SLer T5-	-40	-5	161	0	0	0

Node 125: 19: SLer V+	-32	-8	130	0	0	0
Node 125: 20: SLer V-	-26	-8	107	0	0	0
Node 125: 21: SLer DT+	-39	-5	157	0	0	0
Node 125: 22: SLer DT-	-29	-5	120	0	0	0
Node 125: 23: SLEf V+	-42	-2	173	0	0	0
Node 125: 24: SLEf V-	-38	-2	154	0	0	0
Node 125: 25: SLEf DT+	-45	0	185	0	0	0
Node 125: 26: SLEf DT-	-40	0	162	0	0	0
Node 125: 27: SLEqp	-43	0	177	0	0	0
Node 126: 8: SLE full	-122	0	488	0	0	0
Node 126: 9: SLer T1+	-133	-3	532	0	0	0
Node 126: 10: SLer T1-	-126	-3	507	0	0	0
Node 126: 11: SLer T2+	-79	-4	321	0	0	0
Node 126: 12: SLer T2-	-73	-4	296	0	0	0
Node 126: 13: SLer T3+	-113	-3	455	0	0	0
Node 126: 14: SLer T3-	-107	-3	430	0	0	0
Node 126: 15: SLer T4+	-86	-4	349	0	0	0
Node 126: 16: SLer T4-	-80	-4	325	0	0	0
Node 126: 17: SLer T5+	-62	-4	252	0	0	0
Node 126: 18: SLer T5-	-56	-4	227	0	0	0
Node 126: 19: SLer V+	-59	-7	239	0	0	0
Node 126: 20: SLer V-	-53	-7	216	0	0	0
Node 126: 21: SLer DT+	-55	-4	223	0	0	0
Node 126: 22: SLer DT-	-45	-4	184	0	0	0
Node 126: 23: SLEf V+	-48	-1	194	0	0	0
Node 126: 24: SLEf V-	-43	-1	175	0	0	0
Node 126: 25: SLEf DT+	-45	0	185	0	0	0
Node 126: 26: SLEf DT-	-40	0	162	0	0	0
Node 126: 27: SLEqp	-43	0	177	0	0	0
Node 129: 8: SLE full	-352	0	-316	0	0	0
Node 129: 9: SLer T1+	-340	-4	-305	0	0	0
Node 129: 10: SLer T1-	-369	-4	-331	0	0	0
Node 129: 11: SLer T2+	-265	-3	-236	0	0	0
Node 129: 12: SLer T2-	-293	-4	-262	0	0	0
Node 129: 13: SLer T3+	-285	-4	-254	0	0	0
Node 129: 14: SLer T3-	-312	-4	-280	0	0	0
Node 129: 15: SLer T4+	-244	-3	-217	0	0	0
Node 129: 16: SLer T4-	-271	-3	-242	0	0	0
Node 129: 17: SLer T5+	-317	-4	-284	0	0	0
Node 129: 18: SLer T5-	-344	-4	-309	0	0	0
Node 129: 19: SLer V+	-108	-5	-92	0	0	0
Node 129: 20: SLer V-	-134	-5	-115	0	0	0
Node 129: 21: SLer DT+	-103	-3	-87	0	0	0
Node 129: 22: SLer DT-	-146	-3	-127	0	0	0
Node 129: 23: SLEf V+	-111	-1	-95	0	0	0
Node 129: 24: SLEf V-	-134	-1	-115	0	0	0
Node 129: 25: SLEf DT+	-110	0	-94	0	0	0
Node 129: 26: SLEf DT-	-137	0	-118	0	0	0
Node 129: 27: SLEqp	-120	0	-102	0	0	0
Node 130: 8: SLE full	-352	0	-316	0	0	0
Node 130: 9: SLer T1+	-344	-3	-308	0	0	0
Node 130: 10: SLer T1-	-374	-3	-336	0	0	0
Node 130: 11: SLer T2+	-187	-2	-164	0	0	0
Node 130: 12: SLer T2-	-216	-2	-191	0	0	0
Node 130: 13: SLer T3+	-286	-3	-256	0	0	0
Node 130: 14: SLer T3-	-316	-3	-283	0	0	0
Node 130: 15: SLer T4+	-208	-2	-184	0	0	0
Node 130: 16: SLer T4-	-237	-2	-211	0	0	0
Node 130: 17: SLer T5+	-319	-3	-286	0	0	0
Node 130: 18: SLer T5-	-349	-3	-313	0	0	0
Node 130: 19: SLer V+	-112	-3	-95	0	0	0
Node 130: 20: SLer V-	-141	-3	-121	0	0	0
Node 130: 21: SLer DT+	-105	-2	-89	0	0	0
Node 130: 22: SLer DT-	-151	-2	-131	0	0	0
Node 130: 23: SLEf V+	-112	-1	-95	0	0	0

Node 130: 24: SLEf V-	-135	-1	-116	0	0	0
Node 130: 25: SLEf DT+	-110	0	-93	0	0	0
Node 130: 26: SLEf DT-	-137	0	-118	0	0	0
Node 130: 27: SLEqp	-120	0	-102	0	0	0
Node 133: 8: SLE full	0	0	-21	0	0	0
Node 133: 9: SLEr T1+	0	0	-25	0	0	0
Node 133: 10: SLEr T1-	0	0	-15	0	0	0
Node 133: 11: SLEr T2+	0	0	-11	0	0	0
Node 133: 12: SLEr T2-	0	0	-2	0	0	0
Node 133: 13: SLEr T3+	0	0	5	0	0	0
Node 133: 14: SLEr T3-	0	0	14	0	0	0
Node 133: 15: SLEr T4+	0	0	-24	0	0	0
Node 133: 16: SLEr T4-	0	0	-15	0	0	0
Node 133: 17: SLEr T5+	0	0	-27	0	0	0
Node 133: 18: SLEr T5-	0	0	-18	0	0	0
Node 133: 19: SLEr V+	0	0	-5	0	0	0
Node 133: 20: SLEr V-	0	0	4	0	0	0
Node 133: 21: SLEr DT+	0	0	-7	0	0	0
Node 133: 22: SLEr DT-	0	0	8	0	0	0
Node 133: 23: SLEf V+	0	0	-4	0	0	0
Node 133: 24: SLEf V-	0	0	3	0	0	0
Node 133: 25: SLEf DT+	0	0	-5	0	0	0
Node 133: 26: SLEf DT-	0	0	4	0	0	0
Node 133: 27: SLEqp	0	0	-1	0	0	0
Node 134: 8: SLE full	0	0	-21	0	0	0
Node 134: 9: SLEr T1+	0	61	-24	0	0	0
Node 134: 10: SLEr T1-	0	58	-15	0	0	0
Node 134: 11: SLEr T2+	0	59	-18	0	0	0
Node 134: 12: SLEr T2-	0	56	-9	0	0	0
Node 134: 13: SLEr T3+	0	61	6	0	0	0
Node 134: 14: SLEr T3-	0	58	15	0	0	0
Node 134: 15: SLEr T4+	0	58	-5	0	0	0
Node 134: 16: SLEr T4-	0	55	4	0	0	0
Node 134: 17: SLEr T5+	0	60	-26	0	0	0
Node 134: 18: SLEr T5-	0	58	-17	0	0	0
Node 134: 19: SLEr V+	0	100	-4	0	0	0
Node 134: 20: SLEr V-	0	97	5	0	0	0
Node 134: 21: SLEr DT+	0	61	-7	0	0	0
Node 134: 22: SLEr DT-	0	56	9	0	0	0
Node 134: 23: SLEf V+	0	21	-4	0	0	0
Node 134: 24: SLEf V-	0	18	4	0	0	0
Node 134: 25: SLEf DT+	0	1	-5	0	0	0
Node 134: 26: SLEf DT-	0	-2	4	0	0	0
Node 134: 27: SLEqp	0	0	-1	0	0	0
Node 135: 8: SLE full	121	0	487	0	0	0
Node 135: 9: SLEr T1+	110	-4	439	0	0	0
Node 135: 10: SLEr T1-	119	-4	476	0	0	0
Node 135: 11: SLEr T2+	84	-4	339	0	0	0
Node 135: 12: SLEr T2-	93	-4	376	0	0	0
Node 135: 13: SLEr T3+	91	-4	365	0	0	0
Node 135: 14: SLEr T3-	100	-4	401	0	0	0
Node 135: 15: SLEr T4+	77	-4	311	0	0	0
Node 135: 16: SLEr T4-	86	-4	347	0	0	0
Node 135: 17: SLEr T5+	102	-4	408	0	0	0
Node 135: 18: SLEr T5-	111	-4	444	0	0	0
Node 135: 19: SLEr V+	27	-8	110	0	0	0
Node 135: 20: SLEr V-	35	-8	143	0	0	0
Node 135: 21: SLEr DT+	30	-5	123	0	0	0
Node 135: 22: SLEr DT-	44	-5	181	0	0	0
Node 135: 23: SLEf V+	38	-2	155	0	0	0
Node 135: 24: SLEf V-	45	-2	184	0	0	0
Node 135: 25: SLEf DT+	40	0	164	0	0	0
Node 135: 26: SLEf DT-	49	0	199	0	0	0
Node 135: 27: SLEqp	43	0	176	0	0	0
Node 136: 8: SLE full	121	0	487	0	0	0

Node 136: 9: SLer T1+	126	-3	507	0	0	0
Node 136: 10: SLer T1-	136	-3	547	0	0	0
Node 136: 11: SLer T2+	73	-4	297	0	0	0
Node 136: 12: SLer T2-	83	-4	336	0	0	0
Node 136: 13: SLer T3+	107	-4	430	0	0	0
Node 136: 14: SLer T3-	117	-3	469	0	0	0
Node 136: 15: SLer T4+	81	-4	326	0	0	0
Node 136: 16: SLer T4-	90	-4	364	0	0	0
Node 136: 17: SLer T5+	118	-3	474	0	0	0
Node 136: 18: SLer T5-	128	-3	513	0	0	0
Node 136: 19: SLer V+	53	-7	217	0	0	0
Node 136: 20: SLer V-	63	-7	255	0	0	0
Node 136: 21: SLer DT+	46	-4	187	0	0	0
Node 136: 22: SLer DT-	61	-4	249	0	0	0
Node 136: 23: SLEf V+	43	-1	177	0	0	0
Node 136: 24: SLEf V-	51	-1	207	0	0	0
Node 136: 25: SLEf DT+	40	0	164	0	0	0
Node 136: 26: SLEf DT-	49	0	199	0	0	0
Node 136: 27: SLEqp	43	0	176	0	0	0

4.1.4. Reazioni vincolari SLU

	FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Node 1: 28: SLU 1/6	0	0	79	0	0	0
Node 1: 29: SLU2/3/4/5	0	0	178	0	0	0
Node 1: 30: SLU2/3	0	0	185	0	0	0
Node 1: 31: SLU 4/5	0	-178	51	0	0	0
Node 1: 32: slu FULL_DX	0	2	95	0	0	0
Node 1: 33: SLU 1/6 DX	0	-2	151	0	0	0
Node 1: 34: SLU2/3/4/5 DX	0	2	106	0	0	0
Node 1: 35: SLU2/3	0	-10	88	0	0	0
Node 1: 36: SLU 4/5	0	10	147	0	0	0
Node 1: 37: slu Max mez	0	-178	85	0	0	0
Node 1: 38: slu Max tors	0	-173	148	0	0	0
Node 1: 39: slu Half	0	0	207	0	0	0
Node 1: 40: SLU Tf+v	0	-179	198	0	0	0
Node 1: 41: SLU V+tf	0	-294	113	0	0	0
Node 1: 42: SLU V+tmez	0	-294	68	0	0	0
Node 1: 43: SLU V+ttor	0	-292	93	0	0	0
Node 1: 44: SLU DT+tf	0	-3	127	0	0	0
Node 1: 45: SLU DT-tf	0	5	91	0	0	0
Node 2: 28: SLU 1/6	0	0	78	0	0	0
Node 2: 29: SLU2/3/4/5	0	0	178	0	0	0
Node 2: 30: SLU2/3	0	0	185	0	0	0
Node 2: 31: SLU 4/5	0	0	50	0	0	0
Node 2: 32: slu FULL_DX	0	0	162	0	0	0
Node 2: 33: SLU 1/6 DX	0	0	106	0	0	0
Node 2: 34: SLU2/3/4/5 DX	0	0	151	0	0	0
Node 2: 35: SLU2/3	0	0	147	0	0	0
Node 2: 36: SLU 4/5	0	0	88	0	0	0
Node 2: 37: slu Max mez	0	0	85	0	0	0
Node 2: 38: slu Max tors	0	0	110	0	0	0
Node 2: 39: slu Half	0	0	207	0	0	0
Node 2: 40: SLU Tf+v	0	0	203	0	0	0
Node 2: 41: SLU V+tf	0	0	116	0	0	0
Node 2: 42: SLU V+tmez	0	0	68	0	0	0
Node 2: 43: SLU V+ttor	0	0	78	0	0	0
Node 2: 44: SLU DT+tf	0	0	127	0	0	0
Node 2: 45: SLU DT-tf	0	0	91	0	0	0
Node 3: 28: SLU 1/6	0	0	78	0	0	0
Node 3: 29: SLU2/3/4/5	0	0	178	0	0	0
Node 3: 30: SLU2/3	0	0	50	0	0	0

Node 3: 31: SLU 4/5	0	0	183	0	0	0
Node 3: 32: slu FULL_DX	0	0	94	0	0	0
Node 3: 33: SLU 1/6 DX	0	0	151	0	0	0
Node 3: 34: SLU2/3/4/5 DX	0	0	105	0	0	0
Node 3: 35: SLU2/3	0	0	147	0	0	0
Node 3: 36: SLU 4/5	0	0	88	0	0	0
Node 3: 37: slu Max mez	0	0	84	0	0	0
Node 3: 38: slu Max tors	0	0	147	0	0	0
Node 3: 39: slu Half	0	0	50	0	0	0
Node 3: 40: SLU Tf+v	0	0	198	0	0	0
Node 3: 41: SLU V+tf	0	0	113	0	0	0
Node 3: 42: SLU V+tmez	0	0	68	0	0	0
Node 3: 43: SLU V+ttor	0	0	93	0	0	0
Node 3: 44: SLU DT+tf	0	0	111	0	0	0
Node 3: 45: SLU DT-tf	0	0	118	0	0	0
Node 108: 28: SLU 1/6	0	0	78	0	0	0
Node 108: 29: SLU2/3/4/5	0	0	178	0	0	0
Node 108: 30: SLU2/3	0	-3	50	0	0	0
Node 108: 31: SLU 4/5	0	-125	188	0	0	0
Node 108: 32: slu FULL_DX	0	1	162	0	0	0
Node 108: 33: SLU 1/6 DX	0	-1	105	0	0	0
Node 108: 34: SLU2/3/4/5 DX	0	1	151	0	0	0
Node 108: 35: SLU2/3	0	6	88	0	0	0
Node 108: 36: SLU 4/5	0	-6	147	0	0	0
Node 108: 37: slu Max mez	0	-128	84	0	0	0
Node 108: 38: slu Max tors	0	-126	109	0	0	0
Node 108: 39: slu Half	0	-3	50	0	0	0
Node 108: 40: SLU Tf+v	0	-128	202	0	0	0
Node 108: 41: SLU V+tf	0	-212	116	0	0	0
Node 108: 42: SLU V+tmez	0	-212	68	0	0	0
Node 108: 43: SLU V+ttor	0	-211	78	0	0	0
Node 108: 44: SLU DT+tf	0	9	111	0	0	0
Node 108: 45: SLU DT-tf	0	-16	118	0	0	0
Node 117: 28: SLU 1/6	165	0	-141	0	0	0
Node 117: 29: SLU2/3/4/5	481	0	-432	0	0	0
Node 117: 30: SLU2/3	199	0	-172	0	0	0
Node 117: 31: SLU 4/5	452	-5	-406	0	0	0
Node 117: 32: slu FULL_DX	269	0	-236	0	0	0
Node 117: 33: SLU 1/6 DX	378	0	-337	0	0	0
Node 117: 34: SLU2/3/4/5 DX	268	0	-236	0	0	0
Node 117: 35: SLU2/3	370	0	-329	0	0	0
Node 117: 36: SLU 4/5	278	0	-245	0	0	0
Node 117: 37: slu Max mez	406	-5	-363	0	0	0
Node 117: 38: slu Max tors	300	-4	-265	0	0	0
Node 117: 39: slu Half	199	0	-173	0	0	0
Node 117: 40: SLU Tf+v	484	-5	-434	0	0	0
Node 117: 41: SLU V+tf	296	-6	-262	0	0	0
Node 117: 42: SLU V+tmez	264	-6	-232	0	0	0
Node 117: 43: SLU V+ttor	222	-6	-194	0	0	0
Node 117: 44: SLU DT+tf	308	0	-273	0	0	0
Node 117: 45: SLU DT-tf	262	0	-231	0	0	0
Node 118: 28: SLU 1/6	165	0	-141	0	0	0
Node 118: 29: SLU2/3/4/5	481	0	-432	0	0	0
Node 118: 30: SLU2/3	199	0	-172	0	0	0
Node 118: 31: SLU 4/5	446	-6	-400	0	0	0
Node 118: 32: slu FULL_DX	378	0	-337	0	0	0
Node 118: 33: SLU 1/6 DX	268	0	-236	0	0	0
Node 118: 34: SLU2/3/4/5 DX	378	0	-337	0	0	0
Node 118: 35: SLU2/3	278	0	-245	0	0	0
Node 118: 36: SLU 4/5	370	0	-329	0	0	0
Node 118: 37: slu Max mez	403	-6	-360	0	0	0
Node 118: 38: slu Max tors	346	-6	-308	0	0	0
Node 118: 39: slu Half	199	0	-173	0	0	0
Node 118: 40: SLU Tf+v	476	-7	-427	0	0	0
Node 118: 41: SLU V+tf	286	-9	-253	0	0	0

Node 118: 42: SLU V+tmez	257	-9	-226	0	0	0
Node 118: 43: SLU V+ttor	234	-8	-205	0	0	0
Node 118: 44: SLU DT+tf	308	0	-273	0	0	0
Node 118: 45: SLU DT-tf	262	0	-230	0	0	0
Node 123: 28: SLU 1/6	0	0	14	0	0	0
Node 123: 29: SLU2/3/4/5	-1	0	-49	0	0	0
Node 123: 30: SLU2/3	172	3	-1	0	0	0
Node 123: 31: SLU 4/5	-387	35	-54	0	0	0
Node 123: 32: slu FULL_DX	3	-1	-12	0	0	0
Node 123: 33: SLU 1/6 DX	-4	1	-32	0	0	0
Node 123: 34: SLU2/3/4/5 DX	2	-1	-3	0	0	0
Node 123: 35: SLU2/3	11	-2	-37	0	0	0
Node 123: 36: SLU 4/5	-12	2	-17	0	0	0
Node 123: 37: slu Max mez	-213	37	9	0	0	0
Node 123: 38: slu Max tors	-202	35	-31	0	0	0
Node 123: 39: slu Half	171	3	-1	0	0	0
Node 123: 40: SLU Tf+v	-214	38	-31	0	0	0
Node 123: 41: SLU V+tf	-352	62	-16	0	0	0
Node 123: 42: SLU V+tmez	-351	62	0	0	0	0
Node 123: 43: SLU V+ttor	-348	61	-16	0	0	0
Node 123: 44: SLU DT+tf	-48	-8	-14	0	0	0
Node 123: 45: SLU DT-tf	86	15	-17	0	0	0
Node 124: 28: SLU 1/6	-1	0	14	0	0	0
Node 124: 29: SLU2/3/4/5	-1	0	-49	0	0	0
Node 124: 30: SLU2/3	157	0	-2	0	0	0
Node 124: 31: SLU 4/5	51	0	-53	0	0	0
Node 124: 32: slu FULL_DX	-5	0	-23	0	0	0
Node 124: 33: SLU 1/6 DX	2	0	-3	0	0	0
Node 124: 34: SLU2/3/4/5 DX	-4	0	-32	0	0	0
Node 124: 35: SLU2/3	-13	0	-17	0	0	0
Node 124: 36: SLU 4/5	11	0	-37	0	0	0
Node 124: 37: slu Max mez	210	0	10	0	0	0
Node 124: 38: slu Max tors	201	0	-5	0	0	0
Node 124: 39: slu Half	156	0	-2	0	0	0
Node 124: 40: SLU Tf+v	212	0	-31	0	0	0
Node 124: 41: SLU V+tf	351	0	-15	0	0	0
Node 124: 42: SLU V+tmez	350	0	1	0	0	0
Node 124: 43: SLU V+ttor	347	0	-4	0	0	0
Node 124: 44: SLU DT+tf	-9	0	-14	0	0	0
Node 124: 45: SLU DT-tf	15	0	-17	0	0	0
Node 125: 28: SLU 1/6	-59	0	242	0	0	0
Node 125: 29: SLU2/3/4/5	-166	0	664	0	0	0
Node 125: 30: SLU2/3	-71	0	287	0	0	0
Node 125: 31: SLU 4/5	-142	-5	568	0	0	0
Node 125: 32: slu FULL_DX	-131	0	526	0	0	0
Node 125: 33: SLU 1/6 DX	-94	0	379	0	0	0
Node 125: 34: SLU2/3/4/5 DX	-131	0	527	0	0	0
Node 125: 35: SLU2/3	-97	0	392	0	0	0
Node 125: 36: SLU 4/5	-128	0	515	0	0	0
Node 125: 37: slu Max mez	-127	-5	511	0	0	0
Node 125: 38: slu Max tors	-108	-6	436	0	0	0
Node 125: 39: slu Half	-71	0	288	0	0	0
Node 125: 40: SLU Tf+v	-152	-5	608	0	0	0
Node 125: 41: SLU V+tf	-81	-11	325	0	0	0
Node 125: 42: SLU V+tmez	-71	-11	286	0	0	0
Node 125: 43: SLU V+ttor	-63	-12	256	0	0	0
Node 125: 44: SLU DT+tf	-107	0	433	0	0	0
Node 125: 45: SLU DT-tf	-92	0	372	0	0	0
Node 126: 28: SLU 1/6	-59	0	242	0	0	0
Node 126: 29: SLU2/3/4/5	-166	0	664	0	0	0
Node 126: 30: SLU2/3	-71	0	287	0	0	0
Node 126: 31: SLU 4/5	-168	-4	674	0	0	0
Node 126: 32: slu FULL_DX	-94	0	380	0	0	0
Node 126: 33: SLU 1/6 DX	-131	0	527	0	0	0
Node 126: 34: SLU2/3/4/5 DX	-94	0	379	0	0	0

Node 126: 35: SLU2/3	-128	0	515	0	0	0
Node 126: 36: SLU 4/5	-97	0	392	0	0	0
Node 126: 37: slu Max mez	-152	-4	612	0	0	0
Node 126: 38: slu Max tors	-116	-5	470	0	0	0
Node 126: 39: slu Half	-71	0	288	0	0	0
Node 126: 40: SLU Tf+v	-179	-3	716	0	0	0
Node 126: 41: SLU V+tf	-123	-8	496	0	0	0
Node 126: 42: SLU V+tmez	-112	-8	453	0	0	0
Node 126: 43: SLU V+ttor	-98	-9	397	0	0	0
Node 126: 44: SLU DT+tf	-107	0	433	0	0	0
Node 126: 45: SLU DT-tf	-92	0	372	0	0	0
Node 129: 28: SLU 1/6	-164	0	-140	0	0	0
Node 129: 29: SLU2/3/4/5	-480	0	-431	0	0	0
Node 129: 30: SLU2/3	-447	0	-401	0	0	0
Node 129: 31: SLU 4/5	-193	-5	-167	0	0	0
Node 129: 32: slu FULL_DX	-376	0	-336	0	0	0
Node 129: 33: SLU 1/6 DX	-267	0	-235	0	0	0
Node 129: 34: SLU2/3/4/5 DX	-377	0	-336	0	0	0
Node 129: 35: SLU2/3	-368	0	-328	0	0	0
Node 129: 36: SLU 4/5	-276	0	-244	0	0	0
Node 129: 37: slu Max mez	-401	-6	-358	0	0	0
Node 129: 38: slu Max tors	-345	-6	-307	0	0	0
Node 129: 39: slu Half	-446	0	-400	0	0	0
Node 129: 40: SLU Tf+v	-475	-7	-427	0	0	0
Node 129: 41: SLU V+tf	-286	-9	-252	0	0	0
Node 129: 42: SLU V+tmez	-257	-9	-225	0	0	0
Node 129: 43: SLU V+ttor	-234	-8	-205	0	0	0
Node 129: 44: SLU DT+tf	-265	0	-233	0	0	0
Node 129: 45: SLU DT-tf	-337	0	-300	0	0	0
Node 130: 28: SLU 1/6	-164	0	-140	0	0	0
Node 130: 29: SLU2/3/4/5	-480	0	-431	0	0	0
Node 130: 30: SLU2/3	-447	0	-401	0	0	0
Node 130: 31: SLU 4/5	-200	-3	-173	0	0	0
Node 130: 32: slu FULL_DX	-267	0	-235	0	0	0
Node 130: 33: SLU 1/6 DX	-377	0	-336	0	0	0
Node 130: 34: SLU2/3/4/5 DX	-267	0	-235	0	0	0
Node 130: 35: SLU2/3	-276	0	-244	0	0	0
Node 130: 36: SLU 4/5	-368	0	-328	0	0	0
Node 130: 37: slu Max mez	-404	-5	-361	0	0	0
Node 130: 38: slu Max tors	-299	-4	-264	0	0	0
Node 130: 39: slu Half	-446	0	-399	0	0	0
Node 130: 40: SLU Tf+v	-482	-5	-433	0	0	0
Node 130: 41: SLU V+tf	-295	-6	-261	0	0	0
Node 130: 42: SLU V+tmez	-263	-6	-231	0	0	0
Node 130: 43: SLU V+ttor	-221	-6	-193	0	0	0
Node 130: 44: SLU DT+tf	-265	0	-233	0	0	0
Node 130: 45: SLU DT-tf	-337	0	-300	0	0	0
Node 133: 28: SLU 1/6	0	0	14	0	0	0
Node 133: 29: SLU2/3/4/5	0	0	-50	0	0	0
Node 133: 30: SLU2/3	0	0	-53	0	0	0
Node 133: 31: SLU 4/5	0	0	-2	0	0	0
Node 133: 32: slu FULL_DX	0	0	-13	0	0	0
Node 133: 33: SLU 1/6 DX	0	0	-33	0	0	0
Node 133: 34: SLU2/3/4/5 DX	0	0	-4	0	0	0
Node 133: 35: SLU2/3	0	0	-17	0	0	0
Node 133: 36: SLU 4/5	0	0	-38	0	0	0
Node 133: 37: slu Max mez	0	0	9	0	0	0
Node 133: 38: slu Max tors	0	0	-31	0	0	0
Node 133: 39: slu Half	0	0	-34	0	0	0
Node 133: 40: SLU Tf+v	0	0	-32	0	0	0
Node 133: 41: SLU V+tf	0	0	-16	0	0	0
Node 133: 42: SLU V+tmez	0	0	0	0	0	0
Node 133: 43: SLU V+ttor	0	0	-16	0	0	0
Node 133: 44: SLU DT+tf	0	0	-24	0	0	0
Node 133: 45: SLU DT-tf	0	0	-1	0	0	0

Node 134: 28: SLU 1/6	0	0	14	0	0	0
Node 134: 29: SLU2/3/4/5	0	0	-50	0	0	0
Node 134: 30: SLU2/3	0	0	-53	0	0	0
Node 134: 31: SLU 4/5	0	91	-1	0	0	0
Node 134: 32: slu FULL_DX	0	-2	-23	0	0	0
Node 134: 33: SLU 1/6 DX	0	2	-4	0	0	0
Node 134: 34: SLU2/3/4/5 DX	0	-2	-33	0	0	0
Node 134: 35: SLU2/3	0	6	-38	0	0	0
Node 134: 36: SLU 4/5	0	-6	-17	0	0	0
Node 134: 37: slu Max mez	0	90	9	0	0	0
Node 134: 38: slu Max tors	0	86	-5	0	0	0
Node 134: 39: slu Half	0	0	-34	0	0	0
Node 134: 40: SLU Tf+v	0	91	-31	0	0	0
Node 134: 41: SLU V+tf	0	150	-15	0	0	0
Node 134: 42: SLU V+tmez	0	149	1	0	0	0
Node 134: 43: SLU V+ttor	0	148	-4	0	0	0
Node 134: 44: SLU DT+tf	0	3	-23	0	0	0
Node 134: 45: SLU DT-tf	0	-4	-1	0	0	0
Node 135: 28: SLU 1/6	59	0	241	0	0	0
Node 135: 29: SLU2/3/4/5	165	0	662	0	0	0
Node 135: 30: SLU2/3	154	0	619	0	0	0
Node 135: 31: SLU 4/5	57	-7	233	0	0	0
Node 135: 32: slu FULL_DX	131	0	525	0	0	0
Node 135: 33: SLU 1/6 DX	94	0	378	0	0	0
Node 135: 34: SLU2/3/4/5 DX	131	0	525	0	0	0
Node 135: 35: SLU2/3	128	0	514	0	0	0
Node 135: 36: SLU 4/5	97	0	391	0	0	0
Node 135: 37: slu Max mez	127	-5	508	0	0	0
Node 135: 38: slu Max tors	108	-6	435	0	0	0
Node 135: 39: slu Half	154	0	617	0	0	0
Node 135: 40: SLU Tf+v	152	-5	607	0	0	0
Node 135: 41: SLU V+tf	80	-11	324	0	0	0
Node 135: 42: SLU V+tmez	71	-11	285	0	0	0
Node 135: 43: SLU V+ttor	63	-12	256	0	0	0
Node 135: 44: SLU DT+tf	93	0	377	0	0	0
Node 135: 45: SLU DT-tf	117	0	471	0	0	0
Node 136: 28: SLU 1/6	59	0	241	0	0	0
Node 136: 29: SLU2/3/4/5	165	0	662	0	0	0
Node 136: 30: SLU2/3	154	0	619	0	0	0
Node 136: 31: SLU 4/5	83	-6	335	0	0	0
Node 136: 32: slu FULL_DX	94	0	378	0	0	0
Node 136: 33: SLU 1/6 DX	131	0	525	0	0	0
Node 136: 34: SLU2/3/4/5 DX	93	0	378	0	0	0
Node 136: 35: SLU2/3	97	0	391	0	0	0
Node 136: 36: SLU 4/5	128	0	514	0	0	0
Node 136: 37: slu Max mez	152	-4	609	0	0	0
Node 136: 38: slu Max tors	116	-5	469	0	0	0
Node 136: 39: slu Half	154	0	617	0	0	0
Node 136: 40: SLU Tf+v	178	-3	715	0	0	0
Node 136: 41: SLU V+tf	123	-8	495	0	0	0
Node 136: 42: SLU V+tmez	112	-8	452	0	0	0
Node 136: 43: SLU V+ttor	98	-9	396	0	0	0
Node 136: 44: SLU DT+tf	93	0	377	0	0	0
Node 136: 45: SLU DT-tf	117	0	471	0	0	0

4.1.5. Reazioni vincolari Casi sismici

	FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Node 1: 46: SLV X+++	0	3	37	0	0	0
Node 1: 47: SLV X++	0	-1	37	0	0	0
Node 1: 48: SLV X+-	0	3	37	0	0	0
Node 1: 49: SLV X--	0	-1	37	0	0	0

Node 1: 50: SLV X++	0	1	38	0	0	0
Node 1: 51: SLV X--	0	-3	38	0	0	0
Node 1: 52: SLV X+-	0	1	38	0	0	0
Node 1: 53: SLV X---	0	-3	38	0	0	0
Node 1: 54: SLV Y+++	0	7	37	0	0	0
Node 1: 55: SLV Y++	0	7	37	0	0	0
Node 1: 56: SLV Y+-	0	7	37	0	0	0
Node 1: 57: SLV Y-+	0	7	37	0	0	0
Node 1: 58: SLV Y++	0	-7	37	0	0	0
Node 1: 59: SLV Y--	0	-8	38	0	0	0
Node 1: 60: SLV Y+-	0	-7	37	0	0	0
Node 1: 61: SLV Y---	0	-8	37	0	0	0
Node 1: 62: SLV Z+++	0	2	37	0	0	0
Node 1: 63: SLV Z++	0	2	38	0	0	0
Node 1: 64: SLV Z+-	0	-2	37	0	0	0
Node 1: 65: SLV Z--	0	-3	38	0	0	0
Node 1: 66: SLV Z++	0	2	37	0	0	0
Node 1: 67: SLV Z+-	0	2	37	0	0	0
Node 1: 68: SLV Z+-	0	-2	37	0	0	0
Node 1: 69: SLV Z---	0	-3	37	0	0	0
Node 2: 46: SLV X+++	0	0	37	0	0	0
Node 2: 47: SLV X++	0	0	37	0	0	0
Node 2: 48: SLV X+-	0	0	37	0	0	0
Node 2: 49: SLV X+-	0	0	37	0	0	0
Node 2: 50: SLV X++	0	0	38	0	0	0
Node 2: 51: SLV X--	0	0	38	0	0	0
Node 2: 52: SLV X+-	0	0	38	0	0	0
Node 2: 53: SLV X---	0	0	37	0	0	0
Node 2: 54: SLV Y+++	0	0	37	0	0	0
Node 2: 55: SLV Y++	0	0	37	0	0	0
Node 2: 56: SLV Y+-	0	0	37	0	0	0
Node 2: 57: SLV Y-+	0	0	37	0	0	0
Node 2: 58: SLV Y++	0	0	37	0	0	0
Node 2: 59: SLV Y--	0	0	37	0	0	0
Node 2: 60: SLV Y+-	0	0	37	0	0	0
Node 2: 61: SLV Y---	0	0	37	0	0	0
Node 2: 62: SLV Z+++	0	0	37	0	0	0
Node 2: 63: SLV Z++	0	0	37	0	0	0
Node 2: 64: SLV Z+-	0	0	37	0	0	0
Node 2: 65: SLV Z--	0	0	37	0	0	0
Node 2: 66: SLV Z++	0	0	37	0	0	0
Node 2: 67: SLV Z+-	0	0	37	0	0	0
Node 2: 68: SLV Z+-	0	0	37	0	0	0
Node 2: 69: SLV Z---	0	0	37	0	0	0
Node 3: 46: SLV X+++	0	0	37	0	0	0
Node 3: 47: SLV X++	0	0	37	0	0	0
Node 3: 48: SLV X+-	0	0	37	0	0	0
Node 3: 49: SLV X+-	0	0	37	0	0	0
Node 3: 50: SLV X++	0	0	37	0	0	0
Node 3: 51: SLV X--	0	0	37	0	0	0
Node 3: 52: SLV X+-	0	0	37	0	0	0
Node 3: 53: SLV X---	0	0	37	0	0	0
Node 3: 54: SLV Y+++	0	0	37	0	0	0
Node 3: 55: SLV Y++	0	0	37	0	0	0
Node 3: 56: SLV Y+-	0	0	37	0	0	0
Node 3: 57: SLV Y-+	0	0	37	0	0	0
Node 3: 58: SLV Y++	0	0	37	0	0	0
Node 3: 59: SLV Y--	0	0	37	0	0	0
Node 3: 60: SLV Y+-	0	0	37	0	0	0
Node 3: 61: SLV Y---	0	0	37	0	0	0
Node 3: 62: SLV Z+++	0	0	37	0	0	0
Node 3: 63: SLV Z++	0	0	37	0	0	0
Node 3: 64: SLV Z+-	0	0	37	0	0	0
Node 3: 65: SLV Z--	0	0	37	0	0	0
Node 3: 66: SLV Z++	0	0	37	0	0	0

Node 3: 67: SLV Z--	0	0	37	0	0	0
Node 3: 68: SLV Z+-	0	0	37	0	0	0
Node 3: 69: SLV Z---	0	0	37	0	0	0
Node 108: 46: SLV X+++	0	1	37	0	0	0
Node 108: 47: SLV X++	0	-2	37	0	0	0
Node 108: 48: SLV X++	0	1	37	0	0	0
Node 108: 49: SLV X+-	0	-2	37	0	0	0
Node 108: 50: SLV X++	0	2	37	0	0	0
Node 108: 51: SLV X--	0	-1	37	0	0	0
Node 108: 52: SLV X+-	0	2	37	0	0	0
Node 108: 53: SLV X---	0	-1	37	0	0	0
Node 108: 54: SLV Y+++	0	5	37	0	0	0
Node 108: 55: SLV Y++	0	5	37	0	0	0
Node 108: 56: SLV Y++	0	5	37	0	0	0
Node 108: 57: SLV Y+-	0	5	37	0	0	0
Node 108: 58: SLV Y++	0	-5	37	0	0	0
Node 108: 59: SLV Y--	0	-5	37	0	0	0
Node 108: 60: SLV Y+-	0	-5	37	0	0	0
Node 108: 61: SLV Y---	0	-5	37	0	0	0
Node 108: 62: SLV Z+++	0	1	37	0	0	0
Node 108: 63: SLV Z++	0	2	37	0	0	0
Node 108: 64: SLV Z++	0	-2	37	0	0	0
Node 108: 65: SLV Z--	0	-1	37	0	0	0
Node 108: 66: SLV Z++	0	1	37	0	0	0
Node 108: 67: SLV Z+-	0	2	37	0	0	0
Node 108: 68: SLV Z+-	0	-2	37	0	0	0
Node 108: 69: SLV Z---	0	-1	37	0	0	0
Node 117: 46: SLV X+++	120	0	-103	0	0	0
Node 117: 47: SLV X++	120	0	-103	0	0	0
Node 117: 48: SLV X++	120	0	-102	0	0	0
Node 117: 49: SLV X+-	120	0	-103	0	0	0
Node 117: 50: SLV X++	120	0	-103	0	0	0
Node 117: 51: SLV X--	121	0	-103	0	0	0
Node 117: 52: SLV X+-	120	0	-103	0	0	0
Node 117: 53: SLV X---	120	0	-103	0	0	0
Node 117: 54: SLV Y+++	120	0	-103	0	0	0
Node 117: 55: SLV Y++	120	0	-103	0	0	0
Node 117: 56: SLV Y++	120	0	-102	0	0	0
Node 117: 57: SLV Y+-	120	0	-102	0	0	0
Node 117: 58: SLV Y++	121	0	-103	0	0	0
Node 117: 59: SLV Y--	121	0	-103	0	0	0
Node 117: 60: SLV Y+-	120	0	-103	0	0	0
Node 117: 61: SLV Y---	120	0	-103	0	0	0
Node 117: 62: SLV Z+++	121	0	-103	0	0	0
Node 117: 63: SLV Z++	121	0	-103	0	0	0
Node 117: 64: SLV Z++	121	0	-103	0	0	0
Node 117: 65: SLV Z--	121	0	-103	0	0	0
Node 117: 66: SLV Z++	120	0	-102	0	0	0
Node 117: 67: SLV Z+-	120	0	-102	0	0	0
Node 117: 68: SLV Z+-	120	0	-102	0	0	0
Node 117: 69: SLV Z---	120	0	-103	0	0	0
Node 118: 46: SLV X+++	120	0	-103	0	0	0
Node 118: 47: SLV X++	120	0	-103	0	0	0
Node 118: 48: SLV X++	120	0	-103	0	0	0
Node 118: 49: SLV X+-	120	0	-102	0	0	0
Node 118: 50: SLV X++	121	0	-103	0	0	0
Node 118: 51: SLV X--	120	0	-103	0	0	0
Node 118: 52: SLV X+-	120	0	-103	0	0	0
Node 118: 53: SLV X---	120	0	-103	0	0	0
Node 118: 54: SLV Y+++	121	0	-103	0	0	0
Node 118: 55: SLV Y++	121	0	-103	0	0	0
Node 118: 56: SLV Y++	120	0	-103	0	0	0
Node 118: 57: SLV Y+-	120	0	-103	0	0	0
Node 118: 58: SLV Y++	120	0	-103	0	0	0
Node 118: 59: SLV Y--	120	0	-103	0	0	0

Node 118: 60: SLV Y++	120	0	-102	0	0	0
Node 118: 61: SLV Y--	120	0	-102	0	0	0
Node 118: 62: SLV Z+++	121	0	-103	0	0	0
Node 118: 63: SLV Z++	121	0	-103	0	0	0
Node 118: 64: SLV Z+-	121	0	-103	0	0	0
Node 118: 65: SLV Z--	121	0	-103	0	0	0
Node 118: 66: SLV Z++	120	0	-102	0	0	0
Node 118: 67: SLV Z+-	120	0	-102	0	0	0
Node 118: 68: SLV Z--	120	0	-102	0	0	0
Node 118: 69: SLV Z--	120	0	-102	0	0	0
Node 123: 46: SLV X+++	0	0	-1	0	0	0
Node 123: 47: SLV X++	-6	1	-1	0	0	0
Node 123: 48: SLV X++	0	0	-1	0	0	0
Node 123: 49: SLV X--	-6	1	-1	0	0	0
Node 123: 50: SLV X++	5	-1	-1	0	0	0
Node 123: 51: SLV X--	-1	0	-1	0	0	0
Node 123: 52: SLV X+-	5	-1	-1	0	0	0
Node 123: 53: SLV X--	-1	0	-1	0	0	0
Node 123: 54: SLV Y+++	9	-2	-1	0	0	0
Node 123: 55: SLV Y++	10	-2	-1	0	0	0
Node 123: 56: SLV Y++	9	-2	-1	0	0	0
Node 123: 57: SLV Y+-	10	-2	-1	0	0	0
Node 123: 58: SLV Y++	-11	2	-1	0	0	0
Node 123: 59: SLV Y--	-9	2	-1	0	0	0
Node 123: 60: SLV Y--	-11	2	-1	0	0	0
Node 123: 61: SLV Y--	-9	2	-1	0	0	0
Node 123: 62: SLV Z+++	2	-1	-1	0	0	0
Node 123: 63: SLV Z++	3	-1	-1	0	0	0
Node 123: 64: SLV Z+-	-4	1	-1	0	0	0
Node 123: 65: SLV Z--	-2	1	-1	0	0	0
Node 123: 66: SLV Z++	2	-1	-1	0	0	0
Node 123: 67: SLV Z+-	3	-1	-1	0	0	0
Node 123: 68: SLV Z--	-4	1	-1	0	0	0
Node 123: 69: SLV Z--	-2	1	-1	0	0	0
Node 124: 46: SLV X+++	-4	0	-1	0	0	0
Node 124: 47: SLV X++	2	0	-1	0	0	0
Node 124: 48: SLV X++	-4	0	-1	0	0	0
Node 124: 49: SLV X--	2	0	-1	0	0	0
Node 124: 50: SLV X++	-3	0	-1	0	0	0
Node 124: 51: SLV X--	3	0	-1	0	0	0
Node 124: 52: SLV X+-	-3	0	-1	0	0	0
Node 124: 53: SLV X--	3	0	-1	0	0	0
Node 124: 54: SLV Y+++	-10	0	-1	0	0	0
Node 124: 55: SLV Y++	-10	0	-1	0	0	0
Node 124: 56: SLV Y++	-10	0	-1	0	0	0
Node 124: 57: SLV Y+-	-10	0	-1	0	0	0
Node 124: 58: SLV Y++	9	0	-1	0	0	0
Node 124: 59: SLV Y--	9	0	-1	0	0	0
Node 124: 60: SLV Y--	9	0	-1	0	0	0
Node 124: 61: SLV Y--	9	0	-1	0	0	0
Node 124: 62: SLV Z+++	-4	0	-1	0	0	0
Node 124: 63: SLV Z++	-3	0	-1	0	0	0
Node 124: 64: SLV Z+-	2	0	-1	0	0	0
Node 124: 65: SLV Z--	3	0	-1	0	0	0
Node 124: 66: SLV Z++	-4	0	-1	0	0	0
Node 124: 67: SLV Z+-	-3	0	-1	0	0	0
Node 124: 68: SLV Z--	2	0	-1	0	0	0
Node 124: 69: SLV Z--	3	0	-1	0	0	0
Node 125: 46: SLV X+++	-43	0	176	0	0	0
Node 125: 47: SLV X++	-43	0	177	0	0	0
Node 125: 48: SLV X++	-43	0	176	0	0	0
Node 125: 49: SLV X--	-43	0	177	0	0	0
Node 125: 50: SLV X++	-43	0	177	0	0	0
Node 125: 51: SLV X--	-43	0	178	0	0	0
Node 125: 52: SLV X+-	-43	0	176	0	0	0

Node 125: 53: SLV X---	-43	0	177	0	0	0
Node 125: 54: SLV Y+++	-43	0	175	0	0	0
Node 125: 55: SLV Y++	-43	0	175	0	0	0
Node 125: 56: SLV Y++	-43	0	175	0	0	0
Node 125: 57: SLV Y+-	-43	0	175	0	0	0
Node 125: 58: SLV Y++	-44	0	178	0	0	0
Node 125: 59: SLV Y--	-44	0	179	0	0	0
Node 125: 60: SLV Y--	-44	0	178	0	0	0
Node 125: 61: SLV Y---	-44	0	178	0	0	0
Node 125: 62: SLV Z+++	-43	0	177	0	0	0
Node 125: 63: SLV Z++	-43	0	177	0	0	0
Node 125: 64: SLV Z++	-44	0	178	0	0	0
Node 125: 65: SLV Z--	-44	0	178	0	0	0
Node 125: 66: SLV Z++	-43	0	176	0	0	0
Node 125: 67: SLV Z+-	-43	0	176	0	0	0
Node 125: 68: SLV Z--	-43	0	177	0	0	0
Node 125: 69: SLV Z---	-43	0	177	0	0	0
Node 126: 46: SLV X+++	-44	0	177	0	0	0
Node 126: 47: SLV X++	-43	0	176	0	0	0
Node 126: 48: SLV X++	-43	0	177	0	0	0
Node 126: 49: SLV X--	-43	0	176	0	0	0
Node 126: 50: SLV X++	-43	0	177	0	0	0
Node 126: 51: SLV X--	-43	0	176	0	0	0
Node 126: 52: SLV X+-	-43	0	177	0	0	0
Node 126: 53: SLV X---	-43	0	176	0	0	0
Node 126: 54: SLV Y+++	-44	0	178	0	0	0
Node 126: 55: SLV Y++	-44	0	178	0	0	0
Node 126: 56: SLV Y++	-44	0	178	0	0	0
Node 126: 57: SLV Y+-	-44	0	178	0	0	0
Node 126: 58: SLV Y++	-43	0	175	0	0	0
Node 126: 59: SLV Y--	-43	0	175	0	0	0
Node 126: 60: SLV Y--	-43	0	175	0	0	0
Node 126: 61: SLV Y---	-43	0	175	0	0	0
Node 126: 62: SLV Z+++	-44	0	178	0	0	0
Node 126: 63: SLV Z++	-44	0	178	0	0	0
Node 126: 64: SLV Z++	-43	0	177	0	0	0
Node 126: 65: SLV Z--	-43	0	177	0	0	0
Node 126: 66: SLV Z++	-43	0	177	0	0	0
Node 126: 67: SLV Z+-	-43	0	177	0	0	0
Node 126: 68: SLV Z--	-43	0	176	0	0	0
Node 126: 69: SLV Z---	-43	0	176	0	0	0
Node 129: 46: SLV X+++	-120	0	-103	0	0	0
Node 129: 47: SLV X++	-120	0	-102	0	0	0
Node 129: 48: SLV X++	-120	0	-102	0	0	0
Node 129: 49: SLV X--	-120	0	-102	0	0	0
Node 129: 50: SLV X++	-120	0	-102	0	0	0
Node 129: 51: SLV X--	-120	0	-102	0	0	0
Node 129: 52: SLV X+-	-120	0	-102	0	0	0
Node 129: 53: SLV X---	-119	0	-102	0	0	0
Node 129: 54: SLV Y+++	-120	0	-103	0	0	0
Node 129: 55: SLV Y++	-120	0	-103	0	0	0
Node 129: 56: SLV Y++	-120	0	-102	0	0	0
Node 129: 57: SLV Y+-	-120	0	-102	0	0	0
Node 129: 58: SLV Y++	-120	0	-102	0	0	0
Node 129: 59: SLV Y--	-120	0	-102	0	0	0
Node 129: 60: SLV Y--	-120	0	-102	0	0	0
Node 129: 61: SLV Y---	-119	0	-102	0	0	0
Node 129: 62: SLV Z+++	-120	0	-103	0	0	0
Node 129: 63: SLV Z++	-120	0	-103	0	0	0
Node 129: 64: SLV Z++	-120	0	-103	0	0	0
Node 129: 65: SLV Z--	-120	0	-102	0	0	0
Node 129: 66: SLV Z++	-120	0	-102	0	0	0
Node 129: 67: SLV Z+-	-120	0	-102	0	0	0
Node 129: 68: SLV Z--	-119	0	-102	0	0	0
Node 129: 69: SLV Z---	-119	0	-102	0	0	0

Node 130: 46: SLV X+++	-120	0	-102	0	0	0
Node 130: 47: SLV X+++	-120	0	-102	0	0	0
Node 130: 48: SLV X++-	-120	0	-102	0	0	0
Node 130: 49: SLV X+--	-120	0	-102	0	0	0
Node 130: 50: SLV X+++	-120	0	-102	0	0	0
Node 130: 51: SLV X--+	-120	0	-102	0	0	0
Node 130: 52: SLV X+-	-120	0	-102	0	0	0
Node 130: 53: SLV X---	-120	0	-102	0	0	0
Node 130: 54: SLV Y+++	-120	0	-102	0	0	0
Node 130: 55: SLV Y++	-120	0	-102	0	0	0
Node 130: 56: SLV Y+-	-119	0	-102	0	0	0
Node 130: 57: SLV Y-+	-119	0	-102	0	0	0
Node 130: 58: SLV Y++	-120	0	-103	0	0	0
Node 130: 59: SLV Y--	-120	0	-103	0	0	0
Node 130: 60: SLV Y+-	-120	0	-102	0	0	0
Node 130: 61: SLV Y---	-120	0	-102	0	0	0
Node 130: 62: SLV Z+++	-120	0	-102	0	0	0
Node 130: 63: SLV Z++	-120	0	-102	0	0	0
Node 130: 64: SLV Z+-	-120	0	-103	0	0	0
Node 130: 65: SLV Z--	-120	0	-103	0	0	0
Node 130: 66: SLV Z++	-119	0	-102	0	0	0
Node 130: 67: SLV Z+-	-119	0	-102	0	0	0
Node 130: 68: SLV Z--	-120	0	-102	0	0	0
Node 130: 69: SLV Z---	-120	0	-102	0	0	0
Node 133: 46: SLV X+++	0	0	-1	0	0	0
Node 133: 47: SLV X++	0	0	-1	0	0	0
Node 133: 48: SLV X+-	0	0	-1	0	0	0
Node 133: 49: SLV X+--	0	0	-1	0	0	0
Node 133: 50: SLV X+++	0	0	-2	0	0	0
Node 133: 51: SLV X--+	0	0	-2	0	0	0
Node 133: 52: SLV X+-	0	0	-2	0	0	0
Node 133: 53: SLV X---	0	0	-2	0	0	0
Node 133: 54: SLV Y+++	0	0	-1	0	0	0
Node 133: 55: SLV Y++	0	0	-1	0	0	0
Node 133: 56: SLV Y+-	0	0	-1	0	0	0
Node 133: 57: SLV Y-+	0	0	-1	0	0	0
Node 133: 58: SLV Y++	0	0	-1	0	0	0
Node 133: 59: SLV Y--	0	0	-2	0	0	0
Node 133: 60: SLV Y+-	0	0	-1	0	0	0
Node 133: 61: SLV Y---	0	0	-2	0	0	0
Node 133: 62: SLV Z+++	0	0	-1	0	0	0
Node 133: 63: SLV Z++	0	0	-2	0	0	0
Node 133: 64: SLV Z+-	0	0	-1	0	0	0
Node 133: 65: SLV Z--	0	0	-2	0	0	0
Node 133: 66: SLV Z++	0	0	-1	0	0	0
Node 133: 67: SLV Z+-	0	0	-1	0	0	0
Node 133: 68: SLV Z--	0	0	-1	0	0	0
Node 133: 69: SLV Z---	0	0	-1	0	0	0
Node 134: 46: SLV X+++	0	-2	-1	0	0	0
Node 134: 47: SLV X++	0	1	-1	0	0	0
Node 134: 48: SLV X+-	0	-2	-1	0	0	0
Node 134: 49: SLV X+--	0	1	-1	0	0	0
Node 134: 50: SLV X+++	0	-1	-2	0	0	0
Node 134: 51: SLV X--+	0	2	-2	0	0	0
Node 134: 52: SLV X+-	0	-1	-2	0	0	0
Node 134: 53: SLV X---	0	2	-2	0	0	0
Node 134: 54: SLV Y+++	0	-5	-1	0	0	0
Node 134: 55: SLV Y++	0	-4	-2	0	0	0
Node 134: 56: SLV Y+-	0	-5	-1	0	0	0
Node 134: 57: SLV Y-+	0	-4	-1	0	0	0
Node 134: 58: SLV Y++	0	4	-1	0	0	0
Node 134: 59: SLV Y--	0	5	-1	0	0	0
Node 134: 60: SLV Y+-	0	4	-1	0	0	0
Node 134: 61: SLV Y---	0	5	-1	0	0	0
Node 134: 62: SLV Z+++	0	-1	-1	0	0	0

Node 134: 63: SLV Z++	0	-1	-2	0	0	0
Node 134: 64: SLV Z++	0	1	-1	0	0	0
Node 134: 65: SLV Z--	0	1	-1	0	0	0
Node 134: 66: SLV Z++	0	-1	-1	0	0	0
Node 134: 67: SLV Z+-	0	-1	-1	0	0	0
Node 134: 68: SLV Z--	0	1	-1	0	0	0
Node 134: 69: SLV Z--	0	1	-1	0	0	0
Node 135: 46: SLV X+++	43	0	177	0	0	0
Node 135: 47: SLV X++	44	0	178	0	0	0
Node 135: 48: SLV X++	43	0	176	0	0	0
Node 135: 49: SLV X--	43	0	177	0	0	0
Node 135: 50: SLV X++	43	0	175	0	0	0
Node 135: 51: SLV X--	43	0	176	0	0	0
Node 135: 52: SLV X+-	43	0	175	0	0	0
Node 135: 53: SLV X--	43	0	176	0	0	0
Node 135: 54: SLV Y+++	43	0	175	0	0	0
Node 135: 55: SLV Y++	43	0	175	0	0	0
Node 135: 56: SLV Y++	43	0	175	0	0	0
Node 135: 57: SLV Y+-	43	0	174	0	0	0
Node 135: 58: SLV Y++	44	0	178	0	0	0
Node 135: 59: SLV Y--	44	0	178	0	0	0
Node 135: 60: SLV Y--	44	0	178	0	0	0
Node 135: 61: SLV Y--	44	0	178	0	0	0
Node 135: 62: SLV Z+++	43	0	176	0	0	0
Node 135: 63: SLV Z++	43	0	176	0	0	0
Node 135: 64: SLV Z++	43	0	177	0	0	0
Node 135: 65: SLV Z--	43	0	177	0	0	0
Node 135: 66: SLV Z++	43	0	176	0	0	0
Node 135: 67: SLV Z+-	43	0	175	0	0	0
Node 135: 68: SLV Z--	43	0	177	0	0	0
Node 135: 69: SLV Z--	43	0	176	0	0	0
Node 136: 46: SLV X+++	43	0	176	0	0	0
Node 136: 47: SLV X++	43	0	175	0	0	0
Node 136: 48: SLV X++	43	0	176	0	0	0
Node 136: 49: SLV X--	43	0	175	0	0	0
Node 136: 50: SLV X++	44	0	177	0	0	0
Node 136: 51: SLV X--	43	0	176	0	0	0
Node 136: 52: SLV X+-	43	0	177	0	0	0
Node 136: 53: SLV X--	43	0	176	0	0	0
Node 136: 54: SLV Y+++	44	0	178	0	0	0
Node 136: 55: SLV Y++	44	0	178	0	0	0
Node 136: 56: SLV Y++	44	0	178	0	0	0
Node 136: 57: SLV Y+-	44	0	178	0	0	0
Node 136: 58: SLV Y++	43	0	175	0	0	0
Node 136: 59: SLV Y--	43	0	175	0	0	0
Node 136: 60: SLV Y--	43	0	174	0	0	0
Node 136: 61: SLV Y--	43	0	175	0	0	0
Node 136: 62: SLV Z+++	43	0	177	0	0	0
Node 136: 63: SLV Z++	43	0	177	0	0	0
Node 136: 64: SLV Z++	43	0	176	0	0	0
Node 136: 65: SLV Z--	43	0	176	0	0	0
Node 136: 66: SLV Z++	43	0	176	0	0	0
Node 136: 67: SLV Z+-	43	0	176	0	0	0
Node 136: 68: SLV Z--	43	0	175	0	0	0
Node 136: 69: SLV Z--	43	0	176	0	0	0

5. CONDIZIONI E CASI DI CARICO

Di seguito le condizioni di carico considerate dimensionanti per il calcolo delle fondazioni derivanti dal modello della sovrastruttura. A queste si aggiungono il peso proprio degli elementi di fondazione e il peso del terreno (5.8 m) sopra la fondazione inferiore avente la funzione di stabilizzare il sistema globale.

5.1. CARICHI APPLICATI

CARICHI	NODI	----- ----- ----- -----	num.=	312
Nome	Nodo	Direzione	Intensità	
1 reazioni_x_d_1	457	X	0.010	
2 reazioni_x_d_1	457	Y	0.010	
3 reazioni_x_d_1	457	Z	-199.860	
4 reazioni_x_d_2	453	X	0.010	
5 reazioni_x_d_2	453	Y	-0.030	
6 reazioni_x_d_2	453	Z	-199.930	
7 reazioni_x_d_3	798	X	-480.220	
8 reazioni_x_d_3	798	Y	0.010	
9 reazioni_x_d_3	798	Z	431.080	
10 reazioni_x_d_4	803	X	-480.190	
11 reazioni_x_d_4	803	Y	0.010	
12 reazioni_x_d_4	803	Z	431.050	
13 reazioni_x_d_5	826	X	0.650	
14 reazioni_x_d_5	826	Y	0.010	
15 reazioni_x_d_5	826	Z	30.780	
16 reazioni_x_d_6	827	X	1.430	
17 reazioni_x_d_6	827	Y	0.010	
18 reazioni_x_d_6	827	Z	30.840	
19 reazioni_x_d_7	802	X	165.390	
20 reazioni_x_d_7	802	Y	-0.020	
21 reazioni_x_d_7	802	Z	-662.550	
22 reazioni_x_d_8	800	X	165.400	
23 reazioni_x_d_8	800	Y	0.020	
24 reazioni_x_d_8	800	Z	-662.590	
25 reazioni_x_d_9	457	X	0.010	
26 reazioni_x_d_9	457	Y	0.010	
27 reazioni_x_d_9	457	Z	-182.530	
28 reazioni_x_d_10	453	X	0.010	
29 reazioni_x_d_10	453	Y	125.110	
30 reazioni_x_d_10	453	Z	-188.260	
31 reazioni_x_d_11	798	X	-452.480	
32 reazioni_x_d_11	798	Y	4.900	
33 reazioni_x_d_11	798	Z	405.550	
34 reazioni_x_d_12	803	X	-446.270	
35 reazioni_x_d_12	803	Y	6.420	
36 reazioni_x_d_12	803	Z	399.890	
37 reazioni_x_d_13	826	X	387.240	
38 reazioni_x_d_13	826	Y	-34.770	
39 reazioni_x_d_13	826	Z	53.950	
40 reazioni_x_d_14	827	X	-51.450	
41 reazioni_x_d_14	827	Y	0.010	
42 reazioni_x_d_14	827	Z	53.390	
43 reazioni_x_d_15	802	X	141.860	
44 reazioni_x_d_15	802	Y	5.090	
45 reazioni_x_d_15	802	Z	-568.480	
46 reazioni_x_d_16	800	X	168.160	
47 reazioni_x_d_16	800	Y	3.670	
48 reazioni_x_d_16	800	Z	-674.500	
49 reazioni_x_d_17	457	X	0.010	
50 reazioni_x_d_17	457	Y	0.010	
51 reazioni_x_d_17	457	Z	-94.300	
52 reazioni_x_d_18	453	X	0.010	
53 reazioni_x_d_18	453	Y	-0.960	
54 reazioni_x_d_18	453	Z	-161.920	
55 reazioni_x_d_19	798	X	-268.550	
56 reazioni_x_d_19	798	Y	-0.090	
57 reazioni_x_d_19	798	Z	236.400	
58 reazioni_x_d_20	803	X	-377.710	
59 reazioni_x_d_20	803	Y	-0.130	
60 reazioni_x_d_20	803	Z	336.840	
61 reazioni_x_d_21	826	X	-2.780	
62 reazioni_x_d_21	826	Y	0.870	
63 reazioni_x_d_21	826	Z	12.500	
64 reazioni_x_d_22	827	X	4.630	
65 reazioni_x_d_22	827	Y	0.010	
66 reazioni_x_d_22	827	Z	23.040	
67 reazioni_x_d_23	802	X	131.000	
68 reazioni_x_d_23	802	Y	0.140	
69 reazioni_x_d_23	802	Z	-526.260	
70 reazioni_x_d_24	800	X	93.960	
71 reazioni_x_d_24	800	Y	0.130	
72 reazioni_x_d_24	800	Z	-379.780	
73 reazioni_x_d_25	457	X	0.010	
74 reazioni_x_d_25	457	Y	0.010	
75 reazioni_x_d_25	457	Z	-83.850	
76 reazioni_x_d_26	453	X	0.010	
77 reazioni_x_d_26	453	Y	127.980	

78	reazioni_x_d_26	453	Z	-84.240
79	reazioni_x_d_27	798	X	-405.950
80	reazioni_x_d_27	798	Y	4.580
81	reazioni_x_d_27	798	Z	362.780
82	reazioni_x_d_28	803	X	-402.760
83	reazioni_x_d_28	803	Y	6.110
84	reazioni_x_d_28	803	Z	359.890
85	reazioni_x_d_29	826	X	213.310
86	reazioni_x_d_29	826	Y	-37.320
87	reazioni_x_d_29	826	Z	-9.120
88	reazioni_x_d_30	827	X	-210.270
89	reazioni_x_d_30	827	Y	0.010
90	reazioni_x_d_30	827	Z	-9.900
91	reazioni_x_d_31	802	X	127.290
92	reazioni_x_d_31	802	Y	5.450
93	reazioni_x_d_31	802	Z	-510.770
94	reazioni_x_d_32	800	X	152.330
95	reazioni_x_d_32	800	Y	4.110
96	reazioni_x_d_32	800	Z	-611.960
97	reazioni_x_d_33	457	X	0.010
98	reazioni_x_d_33	457	Y	0.010
99	reazioni_x_d_33	457	Z	-147.180
100	reazioni_x_d_34	453	X	0.010
101	reazioni_x_d_34	453	Y	125.560
102	reazioni_x_d_34	453	Z	-109.220
103	reazioni_x_d_35	798	X	-300.120
104	reazioni_x_d_35	798	Y	3.880
105	reazioni_x_d_35	798	Z	265.440
106	reazioni_x_d_36	803	X	-346.020
107	reazioni_x_d_36	803	Y	5.660
108	reazioni_x_d_36	803	Z	307.710
109	reazioni_x_d_37	826	X	202.190
110	reazioni_x_d_37	826	Y	-35.290
111	reazioni_x_d_37	826	Z	31.030
112	reazioni_x_d_38	827	X	-200.600
113	reazioni_x_d_38	827	Y	0.010
114	reazioni_x_d_38	827	Z	4.640
115	reazioni_x_d_39	802	X	108.450
116	reazioni_x_d_39	802	Y	5.840
117	reazioni_x_d_39	802	Z	-435.890
118	reazioni_x_d_40	800	X	116.450
119	reazioni_x_d_40	800	Y	5.160
120	reazioni_x_d_40	800	Z	-469.990
121	reazioni_x_d_41	457	X	0.010
122	reazioni_x_d_41	457	Y	0.010
123	reazioni_x_d_41	457	Z	-197.670
124	reazioni_x_d_42	453	X	0.010
125	reazioni_x_d_42	453	Y	128.490
126	reazioni_x_d_42	453	Z	-202.480
127	reazioni_x_d_43	798	X	-483.670
128	reazioni_x_d_43	798	Y	5.130
129	reazioni_x_d_43	798	Z	434.210
130	reazioni_x_d_44	803	X	-476.270
131	reazioni_x_d_44	803	Y	6.640
132	reazioni_x_d_44	803	Z	427.460
133	reazioni_x_d_45	826	X	213.850
134	reazioni_x_d_45	826	Y	-37.560
135	reazioni_x_d_45	826	Z	31.270
136	reazioni_x_d_46	827	X	-212.040
137	reazioni_x_d_46	827	Y	0.010
138	reazioni_x_d_46	827	Z	30.560
139	reazioni_x_d_47	802	X	151.890
140	reazioni_x_d_47	802	Y	4.830
141	reazioni_x_d_47	802	Z	-608.210
142	reazioni_x_d_48	800	X	178.740
143	reazioni_x_d_48	800	Y	3.360
144	reazioni_x_d_48	800	Z	-716.270
145	reazioni_x_d_49	457	X	0.010
146	reazioni_x_d_49	457	Y	0.010
147	reazioni_x_d_49	457	Z	-141.730
148	reazioni_x_d_50	453	X	0.010
149	reazioni_x_d_50	453	Y	81.648
150	reazioni_x_d_50	453	Z	-143.628
151	reazioni_x_d_51	798	X	-362.342
152	reazioni_x_d_51	798	Y	2.857
153	reazioni_x_d_51	798	Z	325.543
154	reazioni_x_d_52	803	X	-358.025
155	reazioni_x_d_52	803	Y	3.869
156	reazioni_x_d_52	803	Z	321.598
157	reazioni_x_d_53	826	X	160.823
158	reazioni_x_d_53	826	Y	-21.529
159	reazioni_x_d_53	826	Z	20.696
160	reazioni_x_d_54	827	X	-136.526
161	reazioni_x_d_54	827	Y	0.010
162	reazioni_x_d_54	827	Z	20.237
163	reazioni_x_d_55	802	X	115.311
164	reazioni_x_d_55	802	Y	3.769
165	reazioni_x_d_55	802	Z	-461.951
166	reazioni_x_d_56	800	X	132.513
167	reazioni_x_d_56	800	Y	3.106
168	reazioni_x_d_56	800	Z	-531.573
169	reazioni_x_d_57	457	X	0.010
170	reazioni_x_d_57	457	Y	0.010
171	reazioni_x_d_57	457	Z	-144.259
172	reazioni_x_d_58	453	X	0.010

173	reazioni_x_d_58	453	Y	91.346
174	reazioni_x_d_58	453	Z	-146.260
175	reazioni_x_d_59	798	X	-343.669
176	reazioni_x_d_59	798	Y	2.772
177	reazioni_x_d_59	798	Z	308.422
178	reazioni_x_d_60	803	X	-339.740
179	reazioni_x_d_60	803	Y	3.797
180	reazioni_x_d_60	803	Z	304.831
181	reazioni_x_d_61	826	X	107.092
182	reazioni_x_d_61	826	Y	-30.716
183	reazioni_x_d_61	826	Z	21.562
184	reazioni_x_d_62	827	X	-146.157
185	reazioni_x_d_62	827	Y	0.010
186	reazioni_x_d_62	827	Z	21.074
187	reazioni_x_d_63	802	X	109.018
188	reazioni_x_d_63	802	Y	3.880
189	reazioni_x_d_63	802	Z	-437.725
190	reazioni_x_d_64	800	X	126.005
191	reazioni_x_d_64	800	Y	3.195
192	reazioni_x_d_64	800	Z	-506.653
193	reazioni_x_d_65	457	X	0.010
194	reazioni_x_d_65	457	Y	0.010
195	reazioni_x_d_65	457	Z	-36.395
196	reazioni_x_d_66	453	X	0.010
197	reazioni_x_d_66	453	Y	25.264
198	reazioni_x_d_66	453	Z	-36.282
199	reazioni_x_d_67	798	X	-125.903
200	reazioni_x_d_67	798	Y	0.653
201	reazioni_x_d_67	798	Z	107.882
202	reazioni_x_d_68	803	X	-124.827
203	reazioni_x_d_68	803	Y	0.994
204	reazioni_x_d_68	803	Z	106.893
205	reazioni_x_d_69	826	X	61.998
206	reazioni_x_d_69	826	Y	-5.448
207	reazioni_x_d_69	826	Z	1.121
208	reazioni_x_d_70	827	X	-43.914
209	reazioni_x_d_70	827	Y	0.010
210	reazioni_x_d_70	827	Z	0.992
211	reazioni_x_d_71	802	X	42.358
212	reazioni_x_d_71	802	Y	1.557
213	reazioni_x_d_71	802	Z	-172.526
214	reazioni_x_d_72	800	X	47.723
215	reazioni_x_d_72	800	Y	1.472
216	reazioni_x_d_72	800	Z	-194.431
217	reazioni_x_d_73	457	X	0.010
218	reazioni_x_d_73	457	Y	0.010
219	reazioni_x_d_73	457	Z	-38.456
220	reazioni_x_d_74	453	X	0.010
221	reazioni_x_d_74	453	Y	33.293
222	reazioni_x_d_74	453	Z	-38.352
223	reazioni_x_d_75	798	X	-111.522
224	reazioni_x_d_75	798	Y	0.635
225	reazioni_x_d_75	798	Z	94.642
226	reazioni_x_d_76	803	X	-110.543
227	reazioni_x_d_76	803	Y	0.980
228	reazioni_x_d_76	803	Z	93.743
229	reazioni_x_d_77	826	X	19.285
230	reazioni_x_d_77	826	Y	-13.074
231	reazioni_x_d_77	826	Z	1.837
232	reazioni_x_d_78	827	X	-50.148
233	reazioni_x_d_78	827	Y	0.010
234	reazioni_x_d_78	827	Z	1.699
235	reazioni_x_d_79	802	X	37.535
236	reazioni_x_d_79	802	Y	1.599
237	reazioni_x_d_79	802	Z	-153.512
238	reazioni_x_d_80	800	X	42.846
239	reazioni_x_d_80	800	Y	1.470
240	reazioni_x_d_80	800	Z	-175.239
241	reazioni_x_d_81	457	X	0.010
242	reazioni_x_d_81	457	Y	0.010
243	reazioni_x_d_81	457	Z	-36.146
244	reazioni_x_d_82	453	X	0.010
245	reazioni_x_d_82	453	Y	-3.440
246	reazioni_x_d_82	453	Z	-36.214
247	reazioni_x_d_83	798	X	-126.405
248	reazioni_x_d_83	798	Y	0.001
249	reazioni_x_d_83	798	Z	108.345
250	reazioni_x_d_84	803	X	-126.387
251	reazioni_x_d_84	803	Y	-0.001
252	reazioni_x_d_84	803	Z	108.328
253	reazioni_x_d_85	826	X	18.489
254	reazioni_x_d_85	826	Y	3.266
255	reazioni_x_d_85	826	Z	0.972
256	reazioni_x_d_86	827	X	3.078
257	reazioni_x_d_86	827	Y	0.010
258	reazioni_x_d_86	827	Z	1.027
259	reazioni_x_d_87	802	X	45.387
260	reazioni_x_d_87	802	Y	-0.026
261	reazioni_x_d_87	802	Z	-184.841
262	reazioni_x_d_88	800	X	45.393
263	reazioni_x_d_88	800	Y	0.025
264	reazioni_x_d_88	800	Z	-184.864
265	reazioni_x_d_89	457	X	0.010
266	reazioni_x_d_89	457	Y	0.010
267	reazioni_x_d_89	457	Z	-38.641

268	reazioni_x_d_90	453	X	0.010
269	reazioni_x_d_90	453	Y	6.181
270	reazioni_x_d_90	453	Z	-38.672
271	reazioni_x_d_91	798	X	-109.205
272	reazioni_x_d_91	798	Y	-0.001
273	reazioni_x_d_91	798	Z	92.510
274	reazioni_x_d_92	803	X	-109.179
275	reazioni_x_d_92	803	Y	0.001
276	reazioni_x_d_92	803	Z	92.486
277	reazioni_x_d_93	826	X	-32.760
278	reazioni_x_d_93	826	Y	-5.886
279	reazioni_x_d_93	826	Z	1.836
280	reazioni_x_d_94	827	X	-4.442
281	reazioni_x_d_94	827	Y	0.010
282	reazioni_x_d_94	827	Z	1.866
283	reazioni_x_d_95	802	X	39.564
284	reazioni_x_d_95	802	Y	0.001
285	reazioni_x_d_95	802	Z	-161.905
286	reazioni_x_d_96	800	X	39.573
287	reazioni_x_d_96	800	Y	-0.001
288	reazioni_x_d_96	800	Z	-161.941
289	reazioni_x_d_97	457	X	0.010
290	reazioni_x_d_97	457	Y	0.010
291	reazioni_x_d_97	457	Z	-37.044
292	reazioni_x_d_98	453	X	0.010
293	reazioni_x_d_98	453	Y	-0.006
294	reazioni_x_d_98	453	Z	-37.100
295	reazioni_x_d_99	798	X	-120.300
296	reazioni_x_d_99	798	Y	0.010
297	reazioni_x_d_99	798	Z	102.725
298	reazioni_x_d_100	803	X	-120.282
299	reazioni_x_d_100	803	Y	0.010
300	reazioni_x_d_100	803	Z	102.708
301	reazioni_x_d_101	826	X	0.286
302	reazioni_x_d_101	826	Y	0.010
303	reazioni_x_d_101	826	Z	1.285
304	reazioni_x_d_102	827	X	0.487
305	reazioni_x_d_102	827	Y	0.010
306	reazioni_x_d_102	827	Z	1.332
307	reazioni_x_d_103	802	X	43.319
308	reazioni_x_d_103	802	Y	-0.016
309	reazioni_x_d_103	802	Z	-176.704
310	reazioni_x_d_104	800	X	43.325
311	reazioni_x_d_104	800	Y	0.016
312	reazioni_x_d_104	800	Z	-176.727

PESI PROPRI ASTE--|-----|-----|-----|-----|
Cond. Nome Carichi Aste
14 313-314 1-2

CARICHI DI LINEA |-----|-----|-----|-----|num.= 0
Numero coordinata Intensità
Nome inizio fine Cond. Direz. inizio fine Descrizione

CARICHI GUSCI-----|-----|-----|-----|-----|num.= 471
Nome Guscio Dir Tip RIF Intensità
315 pesoterra 443 Z FD glo -108.000
316 pesoterra 444 Z FD glo -108.000
317 pesoterra 460 Z FD glo -108.000
318 pesoterra 775 Z FD glo -108.000
319 pesoterra 445 Z FD glo -108.000
320 pesoterra 446 Z FD glo -108.000
321 pesoterra 476 Z FD glo -108.000
322 pesoterra 477 Z FD glo -108.000
323 pesoterra 480 Z FD glo -108.000
324 pesoterra 481 Z FD glo -108.000
325 pesoterra 779 Z FD glo -108.000
326 pesoterra 780 Z FD glo -108.000
327 pesoterra 472 Z FD glo -108.000
328 pesoterra 473 Z FD glo -108.000
329 pesoterra 778 Z FD glo -108.000
330 pesoterra 484 Z FD glo -108.000
331 pesoterra 485 Z FD glo -108.000
332 pesoterra 781 Z FD glo -108.000
333 pesoterra 482 Z FD glo -108.000
334 pesoterra 486 Z FD glo -108.000
335 pesoterra 474 Z FD glo -108.000
336 pesoterra 478 Z FD glo -108.000
337 pesoterra 455 Z FD glo -108.000
338 pesoterra 456 Z FD glo -108.000
339 pesoterra 463 Z FD glo -108.000
340 pesoterra 774 Z FD glo -108.000
341 pesoterra 457 Z FD glo -108.000
342 pesoterra 458 Z FD glo -108.000

PESI PROPRI GUSCI-|-----|-----|-----|-----|
Cond. Nome Carichi Gusci
14 343-785 169-212, 217-227, 229-272, 277-287, 349-356,
358, 365-369, 371-436, 443-458, 460-623, 644,
649, 653, 656, 671, 675-676, 680, 683-704, 729-759,

5.2. CONDIZIONI DI CARICO

CONDIZIONI DI CARICO-----|-----|-----|-----|num.= 15

Nome			
1	001	N. carichi:	24
	Lista carichi: 1-24		
2	002	N. carichi:	24
	Lista carichi: 25-48		
3	003	N. carichi:	24
	Lista carichi: 49-72		
4	004	N. carichi:	24
	Lista carichi: 73-96		
5	005	N. carichi:	24
	Lista carichi: 97-120		
6	006	N. carichi:	24
	Lista carichi: 121-144		
7	007	N. carichi:	24
	Lista carichi: 145-168		
8	008	N. carichi:	24
	Lista carichi: 169-192		
9	009	N. carichi:	24
	Lista carichi: 193-216		
10	010	N. carichi:	24
	Lista carichi: 217-240		
11	011	N. carichi:	24
	Lista carichi: 241-264		
12	012	N. carichi:	24
	Lista carichi: 265-288		
13	013	N. carichi:	24
	Lista carichi: 289-312		
14	peso proprio	N. carichi:	445
	Lista carichi: 313-314, 343-785		
15	permanente terra	N. carichi:	28
	Lista carichi: 315-342		

RISULTANTI DEI CARICHI (punto di applicazione nell'origine degli assi):

cond.	FX	FY	FZ	MX	MY	MZ
1	-6.275200E+02	2.000000E-02	-8.011800E+02	-7.159000E-02	2.538092E+03	1.725360E+00
2	-2.529200E+02	1.104400E+02	-7.009900E+02	-2.012819E+02	1.556222E+03	8.793691E+02
3	-4.194300E+02	-2.000000E-02	-5.534800E+02	1.128832E+02	2.025058E+03	-8.711466E+01
4	-5.260300E+02	1.109300E+02	-5.871700E+02	-2.023235E+02	1.325234E+03	8.833109E+02
5	-4.196300E+02	1.108300E+02	-5.534600E+02	-1.706820E+02	2.024702E+03	8.691437E+02
6	-6.274800E+02	1.109100E+02	-8.011300E+02	-2.035136E+02	2.540554E+03	8.910418E+02
7	-4.482260E+02	7.374000E+01	-5.908080E+02	-1.336467E+02	1.797274E+03	5.853387E+02
8	-4.874310E+02	7.429400E+01	-5.790080E+02	-1.317808E+02	1.922071E+03	5.941569E+02
9	-1.425450E+02	2.451200E+01	-2.227460E+02	-4.355582E+01	1.063442E+03	1.906293E+02
10	-1.725270E+02	2.492300E+01	-2.136380E+02	-4.244202E+01	1.161467E+03	1.980440E+02
11	-1.404250E+02	-1.550000E-01	-2.233930E+02	-4.356000E-01	1.056324E+03	-2.629892E+00
12	-1.764290E+02	3.150000E-01	-2.124610E+02	6.940230E-01	1.174021E+03	6.268392E+00
13	-1.531450E+02	4.400000E-02	-2.195250E+02	-7.285200E-02	1.098198E+03	1.261160E+00
14	0.000000E+00	0.000000E+00	-2.353952E+03	0.000000E+00	4.581163E+04	0.000000E+00
15	0.000000E+00	0.000000E+00	-9.074808E+02	4.408787E+00	1.463642E+04	0.000000E+00

5.3. DESCRIZIONE CASI DI CARICO

NOME	DESCRIZIONE	VERIFICA	TIPO	CONDIZ. INSERITE			CASI INSERITI	
				Num.	Coeff.	Segno	Num.	Coeff.
1	SLU FULL	S.L.U.	somma	1 14 15	1.000 1.300 0.800	+ + +		
2	SLU 4 5	S.L.U.	somma	2 14 15	1.000 1.300 0.800	+ + +		
3	SLU FULL DX	S.L.U.	somma	3 14 15	1.000 1.300 0.800	+ + +		
4	SLU MAX MEZ	S.L.U.	somma	4 14 15	1.000 1.300 0.800	+ + +		
5	SLU MAX TORS	S.L.U.	somma	5 14 15	1.000 1.300 0.800	+ + +		
6	SLU TF+V	S.L.U.	somma	6 14 15	1.000 1.300 0.800	+ + +		
7	SLU EQU 01	SLU_EQU	somma	1 14 15	1.000 0.900 0.800	+ + +		
8	SLU EQU 02	SLU_EQU	somma	5 14 15	1.000 0.900 0.800	+ + +		
9	SLU EQU 03	SLU_EQU	somma	6 14 15	1.000 0.900 0.800	+ + +		
10	SLE RARA 01	Rara	somma	7 14 15	1.000 1.000 1.000	+ + +		
11	SLE RARA 02	Rara	somma	8 14 15	1.000 1.000 1.000	+ + +		
12	SLE FREQ 01	Freq.	somma	9 14 15	1.000 1.000 1.000	+ + +		
13	SLE FREQ 02	Freq.	somma	10 14 15	1.000 1.000 1.000	+ + +		
14	SLE FREQ 02	Freq.	somma	11 14 15	1.000 1.000 1.000	+ + +		
15	SLE FREQ 02	Freq.	somma	12 14 15	1.000 1.000 1.000	+ + +		
16	SLE QPERM	QuasiPerm.	somma	13 14 15	1.000 1.000 1.000	+ + +		

6. VERIFICHE STRUTTURALI SLU E SLE

In questo paragrafo riportiamo le verifiche di resistenza e a fessurazione degli elementi a shell o beam in c.a.

- VERIFICHE A SLU

CASI DI CARICO: ->

Nome	Descrizione
1	SLU FULL
2	SLU 4 5
3	SLU FULL DX
4	SLU MAX MEZ
5	SLU MAX TORS
6	SLU TF+V
7	SLU EQU 01
8	SLU EQU 02
9	SLU EQU 03

DATI:

tensione di snervamento acciaio (fyk):	450	N/mm ²
coefficiente sicurezza acciaio	: 1.15	
deformazione ultima acciaio	: 67.5	per mille
deformazione ultima cls	: 3.5	per mille
rapporto rottura/snervamento (k):	1.15	
resistenza cilindrica cls (fck):	33.2	N/mm ²
coefficiente sicurezza cls	: 1.5	
coefficiente riduttivo (alfa):	0.85	
copriferro inferiore (asse armatura):	0.07	m
copriferro superiore (asse armatura):	0.07	m
moltiplicatore sollecitazioni	: 1	

LEGENDA:

spess	= spessore guscio. Verifica effettuata su sezione BxH, con B=0.01 m e H="spess" m
Af	= area disposta al lembo teso, in cm ² al metro
Afc	= area disposta al lembo compresso, in cm ² al metro
Mom	= momento flettente [kNm/m]
Nor	= sforzo normale [kN]
epsC	= deformazione cls [per mille]
epsF	= deformazione acciaio [per mille]

<-

L'armatura è sufficiente se le deformazioni dei materiali sono ovunque minori delle corrispondenti deformazioni ultime.

Per gli elementi non dissipativi la permanenza in campo elastico è ottenuta limitando la deformazione dell'acciaio alla deformazione di snervamento (67.5 per mille) e quella del calcestruzzo al 2 per mille.

- VERIFICHE A SLE

CASI DI CARICO: ->

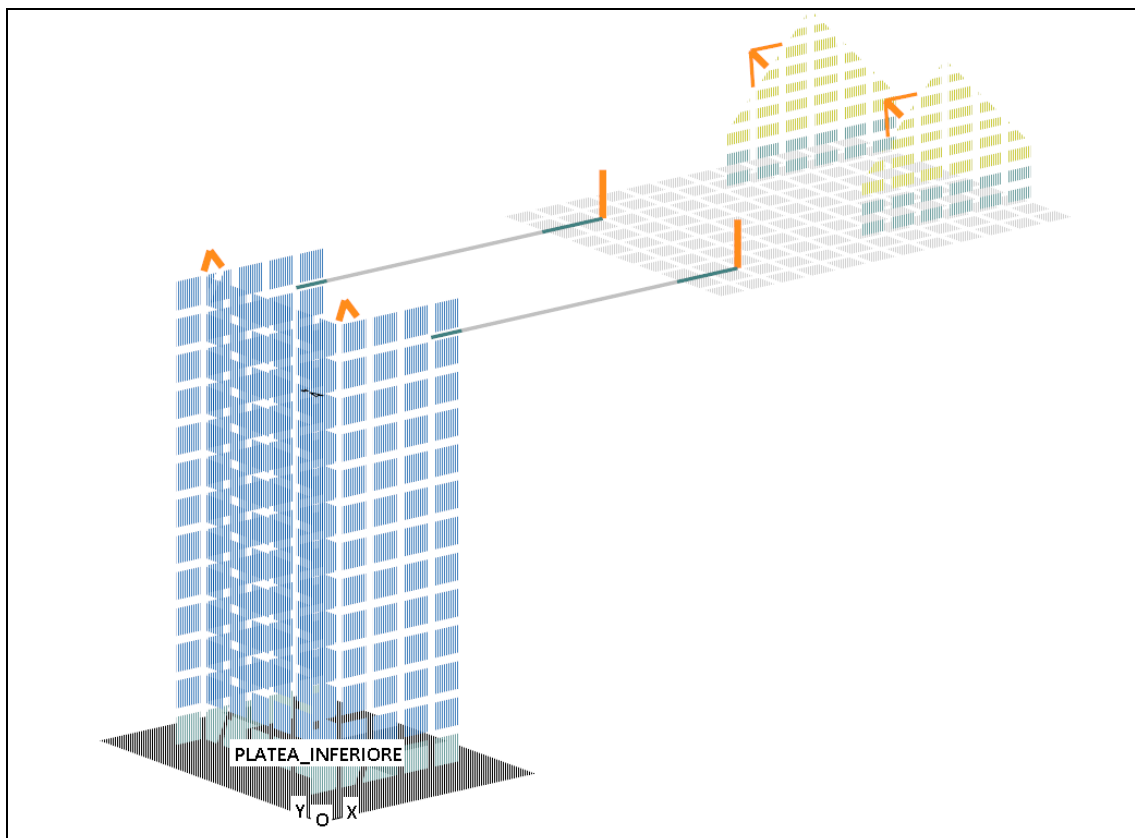
Nome	Descrizione
10	SLE RARA 01 (RARA)
11	SLE RARA 02 (RARA)
12	SLE FREQ 01 (FREQUENTE)
13	SLE FREQ 02 (FREQUENTE)
14	SLE FREQ 02 (FREQUENTE)
15	SLE FREQ 02 (FREQUENTE)
16	SLE QPERM (QUASI PERMANENTE)

DATI:

copriferro inferiore (asse armatura):	0.07	m
copriferro superiore (asse armatura):	0.07	m

Af	= area effettiva tesa (cm ² al metro)	
Afc	= area effettiva compressa (cm ² al metro)	
Mom	= momento flettente [kNm/m]	
Nor	= sforzo normale [kN]	
σc	= tensione calcestruzzo [N/mm ²]	
	valore max per combinazione rara	= 199 N/mm ²
	quasi permanente	= 149 N/mm ²
σf	= tensione acciaio [N/mm ²]	
	valore max per combinazione rara	= 3600 N/mm ²
wkF	= apertura caratteristica per combinazione frequente (mm)	- valore max = 0.4 mm
wkP	= apertura caratteristica per combinazione quasi permanente (mm)	- valore max = 0.3 mm

6.1. PLATEA INFERIORE



G466	G460	G446	G445	G444	G443	G775
G467	G461	G450	G449	G448	G447	G776
G493	G492	G471	G470	G469	G468	G777
G495	G494	G475	G474	G473	G472	G778
G497	G496	G479	G478	G477	G476	G779
G499	G498	G483	G482	G481	G480	G780
G501	G500	G487	G486	G485	G484	G781
G503	G502	G491	G490	G489	G488	G782
G464	G462	G454	G453	G452	G451	G773
G465	G463	G458	G457	G456	G455	G774

6.1.1. Verifica SLU

GUSCI	spess	INFERIORE ORIZZONTALE							INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF		Af	Afc	Mom	Nor	epsC	epsF	
443	1	15.71	15.71	45.	0.	0.00	0.22		15.71	15.71	48.	0.	0.03	0.17	
444	1	15.71	15.71	62.	0.	0.00	0.29		15.71	15.71	46.	0.	0.03	0.16	
445	1	15.71	15.71	91.	0.	0.00	0.38		15.71	15.71	46.	0.	0.03	0.16	

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
446	1	15.71	15.71	125.	0.	0.05	0.48	15.71	15.71	46.	0.	0.03	0.16	
447	1	15.71	15.71	42.	1.	0.00	0.23	15.71	15.71	98.	0.	0.06	0.35	
448	1	15.71	15.71	60.	0.	0.00	0.28	15.71	15.71	96.	0.	0.06	0.34	
449	1	15.71	15.71	93.	0.	0.01	0.38	15.71	15.71	96.	0.	0.06	0.34	
450	1	15.71	15.71	126.	0.	0.06	0.47	15.71	15.71	96.	0.	0.06	0.34	
451	1	15.71	15.71	18.	1.	0.00	0.20	15.71	15.71	58.	0.	0.04	0.20	
452	1	15.71	15.71	38.	1.	0.00	0.23	15.71	15.71	63.	0.	0.04	0.23	
453	1	15.71	15.71	78.	0.	0.00	0.34	15.71	15.71	63.	0.	0.04	0.23	
454	1	15.71	15.71	121.	0.	0.06	0.44	15.71	15.71	63.	0.	0.04	0.23	
455	1	15.71	15.71	14.	1.	0.00	0.19	15.71	15.71	27.	0.	0.02	0.09	
456	1	15.71	15.71	34.	1.	0.00	0.23	15.71	15.71	26.	0.	0.02	0.09	
457	1	15.71	15.71	76.	1.	0.00	0.34	15.71	15.71	26.	0.	0.02	0.09	
458	1	15.71	15.71	121.	0.	0.06	0.45	15.71	15.71	26.	0.	0.02	0.09	
460	1	15.71	15.71	134.	0.	0.08	0.48	15.71	15.71	46.	0.	0.03	0.16	
461	1	15.71	15.71	141.	0.	0.09	0.49	15.71	15.71	96.	0.	0.06	0.35	
462	1	15.71	15.71	148.	0.	0.10	0.50	15.71	15.71	68.	0.	0.04	0.24	
463	1	15.71	15.71	148.	0.	0.10	0.50	15.71	15.71	28.	0.	0.02	0.10	
464	1	15.71	15.71	62.	0.	0.04	0.21	15.71	15.71	79.	0.	0.05	0.28	
465	1	15.71	15.71	64.	0.	0.05	0.22	15.71	15.71	31.	0.	0.02	0.11	
466	1	15.71	15.71	46.	0.	0.00	0.20	15.71	15.71	46.	0.	0.03	0.16	
467	1	15.71	15.71	49.	0.	0.02	0.20	15.71	15.71	97.	0.	0.06	0.35	
468	1	15.71	15.71	39.	1.	0.00	0.25	15.71	15.71	111.	0.	0.04	0.43	
469	1	15.71	15.71	57.	1.	0.00	0.28	15.71	15.71	108.	0.	0.05	0.40	
470	1	15.71	15.71	92.	0.	0.02	0.37	15.71	15.71	108.	0.	0.05	0.40	
471	1	15.71	15.71	127.	0.	0.06	0.47	15.71	15.71	108.	0.	0.05	0.40	
472	1	15.71	15.71	34.	1.	0.00	0.24	15.71	15.71	72.	0.	0.02	0.29	
473	1	15.71	15.71	53.	1.	0.00	0.27	15.71	15.71	70.	0.	0.02	0.28	
474	1	15.71	15.71	88.	0.	0.01	0.36	15.71	15.71	70.	0.	0.02	0.28	
475	1	15.71	15.71	127.	0.	0.06	0.47	15.71	15.71	70.	0.	0.02	0.28	
476	1	15.71	15.71	29.	1.	0.00	0.21	15.71	15.71	55.	0.	0.00	0.25	
477	1	15.71	15.71	47.	1.	0.00	0.25	15.71	15.71	51.	0.	0.00	0.23	
478	1	15.71	15.71	81.	0.	0.01	0.34	15.71	15.71	51.	0.	0.00	0.23	
479	1	15.71	15.71	120.	0.	0.05	0.45	15.71	15.71	51.	0.	0.00	0.23	
480	1	15.71	15.71	28.	1.	0.00	0.21	15.71	15.71	51.	0.	0.00	0.23	
481	1	15.71	15.71	47.	1.	0.00	0.24	15.71	15.71	49.	0.	0.00	0.22	
482	1	15.71	15.71	81.	0.	0.01	0.33	15.71	15.71	49.	0.	0.00	0.22	
483	1	15.71	15.71	119.	0.	0.06	0.44	15.71	15.71	49.	0.	0.00	0.22	
484	1	15.71	15.71	25.	1.	0.00	0.21	15.71	15.71	48.	0.	0.00	0.23	
485	1	15.71	15.71	44.	1.	0.00	0.24	15.71	15.71	49.	0.	0.00	0.23	
486	1	15.71	15.71	80.	0.	0.01	0.33	15.71	15.71	49.	0.	0.00	0.23	
487	1	15.71	15.71	122.	0.	0.06	0.45	15.71	15.71	49.	0.	0.00	0.23	
488	1	15.71	15.71	21.	1.	0.00	0.20	15.71	15.71	52.	1.	0.00	0.37	
489	1	15.71	15.71	40.	1.	0.00	0.24	15.71	15.71	54.	1.	0.00	0.38	
490	1	15.71	15.71	78.	0.	0.00	0.33	15.71	15.71	54.	1.	0.00	0.38	
491	1	15.71	15.71	121.	0.	0.06	0.45	15.71	15.71	54.	1.	0.00	0.38	
492	1	15.71	15.71	143.	0.	0.10	0.49	15.71	15.71	108.	0.	0.05	0.41	
493	1	15.71	15.71	49.	0.	0.02	0.19	15.71	15.71	106.	0.	0.05	0.40	
494	1	15.71	15.71	144.	0.	0.10	0.49	15.71	15.71	69.	0.	0.02	0.27	
495	1	15.71	15.71	53.	0.	0.03	0.19	15.71	15.71	68.	0.	0.02	0.27	
496	1	15.71	15.71	136.	0.	0.09	0.47	15.71	15.71	51.	0.	0.00	0.23	
497	1	15.71	15.71	54.	0.	0.03	0.19	15.71	15.71	49.	0.	0.00	0.22	
498	1	15.71	15.71	136.	0.	0.09	0.47	15.71	15.71	51.	0.	0.00	0.24	
499	1	15.71	15.71	54.	0.	0.04	0.19	15.71	15.71	52.	0.	0.00	0.24	
500	1	15.71	15.71	143.	0.	0.10	0.49	15.71	15.71	55.	0.	0.00	0.26	
501	1	15.71	15.71	58.	0.	0.04	0.20	15.71	15.71	62.	1.	0.00	0.30	
502	1	15.71	15.71	147.	0.	0.10	0.50	15.71	15.71	67.	1.	0.00	0.41	
503	1	15.71	15.71	61.	0.	0.04	0.21	15.71	15.71	88.	1.	0.00	0.45	
773	1	15.71	15.71	18.	0.	0.01	0.06	15.71	15.71	52.	0.	0.04	0.18	
774	1	15.71	15.71	17.	0.	0.01	0.06	15.71	15.71	28.	0.	0.02	0.10	
775	1	15.71	15.71	35.	0.	0.01	0.13	15.71	15.71	52.	0.	0.03	0.18	
776	1	15.71	15.71	32.	0.	0.01	0.13	15.71	15.71	99.	0.	0.07	0.34	
777	1	15.71	15.71	30.	0.	0.02	0.10	15.71	15.71	115.	0.	0.05	0.44	
778	1	15.71	15.71	26.	0.	0.02	0.10	15.71	15.71	75.	0.	0.01	0.31	
779	1	15.71	15.71	22.	0.	0.01	0.08	15.71	15.71	58.	0.	0.00	0.25	
780	1	15.71	15.71	22.	0.	0.01	0.08	15.71	15.71	51.	0.	0.00	0.23	
781	1	15.71	15.71	20.	0.	0.01	0.08	15.71	15.71	43.	0.	0.00	0.21	
782	1	15.71	15.71	18.	0.	0.01	0.07	15.71	15.71	37.	1.	0.00	0.32	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
443	1	15.71	15.71	22.	0.	0.00	0.14	15.71	15.71	14.	0.	0.01	0.05	
444	1	15.71	15.71	14.	0.	0.00	0.13	15.71	15.71	14.	0.	0.01	0.05	
445	1	15.71	15.71	4.	0.	0.00	0.08	15.71	15.71	14.	0.	0.01	0.05	
446	1	15.71	15.71	0.	0.	0.00	0.05	15.71	15.71	14.	0.	0.01	0.05	
447	1	15.71	15.71	26.	1.	0.00	0.18	15.71	15.71	0.	0.	0.00	0.01	
448	1	15.71	15.71	21.	1.	0.00	0.15	15.71	15.71	0.	0.	0.00	0.01	
449	1	15.71	15.71	9.	0.	0.00	0.09	15.71	15.71	0.	0.	0.00	0.01	
450	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	0.	0.	0.00	0.01	
451	1	15.71	15.71	42.	1.	0.00	0.29	15.71	15.71	0.	0.	0.00	0.01	
452	1	15.71	15.71	35.	1.	0.00	0.23	15.71	15.71	0.	0.	0.00	0.01	
453	1	15.71	15.71	3.	0.	0.00	0.08	15.71	15.71	0.	0.	0.00	0.01	
454	1	15.71	15.71	0.	0.	0.00	0.03	15.71	15.71	0.	0.	0.00	0.01	
455	1	15.71	15.71	48.	1.	0.00	0.32	15.71	15.71	1.	0.	0.00	0.01	
456	1	15.71	15.71	41.	1.	0.00	0.25	15.71	15.71	0.	0.	0.00	0.01	
457	1	15.71	15.71	2.	1.	0.00	0.09	15.71	15.71	0.	0.	0.00	0.01	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
458	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	0.	0.	0.00	0.01	
460	1	15.71	15.71	0.	0.	0.00	0.02	15.71	15.71	15.	0.	0.01	0.05	
461	1	15.71	15.71	0.	0.	0.00	0.01	15.71	15.71	0.	0.	0.00	0.01	
462	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	0.	0.	0.00	0.01	
463	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	0.	0.	0.00	0.00	
464	1	15.71	15.71	16.	0.	0.01	0.05	15.71	15.71	0.	0.	0.00	0.00	
465	1	15.71	15.71	9.	0.	0.01	0.03	15.71	15.71	0.	0.	0.00	0.00	
466	1	15.71	15.71	22.	0.	0.00	0.11	15.71	15.71	15.	0.	0.01	0.05	
467	1	15.71	15.71	21.	0.	0.01	0.09	15.71	15.71	0.	0.	0.00	0.02	
468	1	15.71	15.71	30.	1.	0.00	0.23	15.71	15.71	0.	0.	0.00	0.05	
469	1	15.71	15.71	25.	1.	0.00	0.16	15.71	15.71	0.	0.	0.00	0.03	
470	1	15.71	15.71	9.	0.	0.00	0.09	15.71	15.71	0.	0.	0.00	0.03	
471	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	0.	0.	0.00	0.03	
472	1	15.71	15.71	32.	1.	0.00	0.24	15.71	15.71	16.	0.	0.00	0.09	
473	1	15.71	15.71	26.	1.	0.00	0.18	15.71	15.71	17.	0.	0.00	0.09	
474	1	15.71	15.71	5.	0.	0.00	0.07	15.71	15.71	17.	0.	0.00	0.09	
475	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	17.	0.	0.00	0.09	
476	1	15.71	15.71	32.	1.	0.00	0.23	15.71	15.71	42.	0.	0.00	0.20	
477	1	15.71	15.71	25.	1.	0.00	0.17	15.71	15.71	43.	0.	0.00	0.19	
478	1	15.71	15.71	0.	0.	0.00	0.06	15.71	15.71	43.	0.	0.00	0.19	
479	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	43.	0.	0.00	0.19	
480	1	15.71	15.71	33.	1.	0.00	0.23	15.71	15.71	47.	0.	0.00	0.22	
481	1	15.71	15.71	25.	1.	0.00	0.17	15.71	15.71	46.	0.	0.00	0.21	
482	1	15.71	15.71	0.	0.	0.00	0.06	15.71	15.71	46.	0.	0.00	0.21	
483	1	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	46.	0.	0.00	0.21	
484	1	15.71	15.71	36.	1.	0.00	0.26	15.71	15.71	41.	0.	0.00	0.20	
485	1	15.71	15.71	28.	1.	0.00	0.19	15.71	15.71	39.	0.	0.00	0.19	
486	1	15.71	15.71	0.	0.	0.00	0.06	15.71	15.71	39.	0.	0.00	0.19	
487	1	15.71	15.71	0.	0.	0.00	0.03	15.71	15.71	39.	0.	0.00	0.19	
488	1	15.71	15.71	39.	1.	0.00	0.27	15.71	15.71	16.	1.	0.00	0.26	
489	1	15.71	15.71	31.	1.	0.00	0.21	15.71	15.71	10.	1.	0.00	0.24	
490	1	15.71	15.71	0.	0.	0.00	0.06	15.71	15.71	10.	1.	0.00	0.24	
491	1	15.71	15.71	0.	0.	0.00	0.03	15.71	15.71	10.	1.	0.00	0.24	
492	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	0.	0.	0.00	0.03	
493	1	15.71	15.71	20.	0.	0.01	0.07	15.71	15.71	0.	0.	0.00	0.04	
494	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	20.	0.	0.00	0.10	
495	1	15.71	15.71	19.	0.	0.01	0.06	15.71	15.71	26.	0.	0.00	0.12	
496	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	44.	0.	0.00	0.20	
497	1	15.71	15.71	16.	0.	0.01	0.05	15.71	15.71	45.	0.	0.00	0.20	
498	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	46.	0.	0.00	0.22	
499	1	15.71	15.71	15.	0.	0.01	0.05	15.71	15.71	46.	0.	0.00	0.22	
500	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	38.	0.	0.00	0.19	
501	1	15.71	15.71	17.	0.	0.01	0.06	15.71	15.71	34.	0.	0.00	0.19	
502	1	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	3.	1.	0.00	0.21	
503	1	15.71	15.71	17.	0.	0.01	0.06	15.71	15.71	0.	1.	0.00	0.17	
773	1	15.71	15.71	33.	0.	0.02	0.12	15.71	15.71	0.	0.	0.00	0.01	
774	1	15.71	15.71	37.	0.	0.02	0.14	15.71	15.71	3.	0.	0.00	0.02	
775	1	15.71	15.71	18.	0.	0.00	0.08	15.71	15.71	15.	0.	0.00	0.06	
776	1	15.71	15.71	22.	0.	0.01	0.09	15.71	15.71	0.	0.	0.00	0.01	
777	1	15.71	15.71	22.	0.	0.02	0.08	15.71	15.71	0.	0.	0.00	0.05	
778	1	15.71	15.71	26.	0.	0.02	0.10	15.71	15.71	12.	0.	0.00	0.09	
779	1	15.71	15.71	26.	0.	0.02	0.10	15.71	15.71	43.	0.	0.00	0.20	
780	1	15.71	15.71	26.	0.	0.02	0.10	15.71	15.71	50.	0.	0.00	0.22	
781	1	15.71	15.71	28.	0.	0.02	0.11	15.71	15.71	49.	0.	0.00	0.23	
782	1	15.71	15.71	30.	0.	0.02	0.11	15.71	15.71	39.	1.	0.00	0.33	

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO ($R_d > E_d$)

6.1.2. Verifica SLE fessurazione

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP	
443	15.71	15.71	28.04	0.32	0.26	31.	13.46	0.10	0.016	4.12	0.14	0.00	0.011	
444	15.71	15.71	41.35	0.35	0.42	41.	20.44	0.12	0.023	10.05	0.15	0.08	0.015	
445	15.71	15.71	60.52	0.34	0.64	55.	25.77	0.12	0.027	17.03	0.12	0.18	0.020	
446	15.71	15.71	92.33	0.26	1.02	75.	36.66	0.08	0.034	30.14	0.06	0.33	0.028	
447	15.71	15.71	25.63	0.38	0.21	31.	12.74	0.12	0.016	3.79	0.15	0.00	0.011	
448	15.71	15.71	39.45	0.35	0.39	40.	19.90	0.13	0.022	9.83	0.14	0.08	0.015	
449	15.71	15.71	60.59	0.30	0.65	54.	26.00	0.11	0.027	17.16	0.10	0.18	0.019	
450	15.71	15.71	93.99	0.21	1.04	75.	37.39	0.06	0.034	30.19	0.06	0.34	0.028	
451	15.71	15.71	8.51	0.68	0.00	28.	7.55	0.22	0.018	3.85	0.18	0.00	0.013	
452	15.71	15.71	23.36	0.49	0.13	33.	15.34	0.17	0.021	10.18	0.16	0.08	0.016	
453	15.71	15.71	51.56	0.31	0.54	47.	23.12	0.12	0.025	17.92	0.13	0.19	0.021	
454	15.71	15.71	91.79	0.11	1.03	71.	37.46	0.06	0.034	30.90	0.08	0.34	0.030	
455	15.71	15.71	5.44	0.73	0.00	27.	6.63	0.24	0.018	3.88	0.18	0.00	0.013	
456	15.71	15.71	20.64	0.54	0.03	32.	14.50	0.18	0.021	10.02	0.17	0.08	0.017	
457	15.71	15.71	50.39	0.36	0.52	48.	22.74	0.14	0.025	17.85	0.14	0.18	0.022	
458	15.71	15.71	91.76	0.16	1.02	72.	37.71	0.06	0.035	30.88	0.10	0.34	0.030	
460	15.71	15.71	85.00	0.02	0.96	63.	32.08	-0.06	0.025	28.70	-0.09	0.33	0.021	
461	15.71	15.71	89.41	-0.01	1.01	65.	33.69	-0.06	0.026	28.62	-0.09	0.33	0.021	
462	15.71	15.71	99.61	-0.16	1.14	68.	37.08	-0.06	0.029	28.52	-0.08	0.33	0.021	
463	15.71	15.71	100.88	-0.14	1.15	70.	37.84	-0.04	0.030	28.04	-0.06	0.32	0.022	
464	15.71	15.71	38.67	-0.26	0.45	21.	13.22	-0.10	0.008	6.22	-0.15	0.06	0.001	

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
465	15.71	15.71	39.55	-0.25	0.46	22.	13.89	-0.09	0.009	6.40	-0.13	0.07	0.002
466	15.71	15.71	29.12	-0.05	0.33	20.	8.84	-0.12	0.004	6.85	-0.16	0.07	0.001
467	15.71	15.71	30.93	-0.15	0.36	18.	9.69	-0.14	0.004	6.66	-0.17	0.07	0.001
468	15.71	15.71	23.35	0.55	0.09	35.	12.08	0.17	0.018	3.64	0.17	0.00	0.012
469	15.71	15.71	37.60	0.38	0.36	39.	19.35	0.13	0.022	9.93	0.15	0.08	0.016
470	15.71	15.71	60.20	0.28	0.65	53.	25.96	0.11	0.027	17.26	0.12	0.18	0.020
471	15.71	15.71	94.72	0.19	1.05	75.	37.69	0.06	0.034	30.22	0.08	0.33	0.029
472	15.71	15.71	19.42	0.59	0.00	33.	10.85	0.19	0.018	3.63	0.17	0.00	0.012
473	15.71	15.71	33.79	0.42	0.31	38.	18.27	0.15	0.022	9.92	0.16	0.08	0.016
474	15.71	15.71	57.66	0.28	0.62	51.	25.01	0.11	0.026	17.11	0.12	0.18	0.020
475	15.71	15.71	93.76	0.20	1.04	75.	37.43	0.07	0.035	30.12	0.08	0.33	0.029
476	15.71	15.71	15.70	0.54	0.00	29.	9.72	0.18	0.017	3.77	0.16	0.00	0.012
477	15.71	15.71	30.11	0.40	0.27	35.	17.05	0.14	0.021	10.07	0.15	0.08	0.016
478	15.71	15.71	54.44	0.27	0.58	48.	23.76	0.11	0.025	17.38	0.12	0.18	0.020
479	15.71	15.71	90.63	0.19	1.01	72.	36.68	0.07	0.034	30.04	0.08	0.33	0.029
480	15.71	15.71	15.37	0.54	0.00	29.	9.63	0.18	0.017	3.79	0.16	0.00	0.012
481	15.71	15.71	29.77	0.40	0.26	34.	16.96	0.14	0.021	10.10	0.15	0.08	0.016
482	15.71	15.71	54.21	0.27	0.58	48.	23.68	0.11	0.025	17.42	0.12	0.18	0.020
483	15.71	15.71	90.58	0.19	1.01	72.	36.67	0.07	0.034	30.09	0.08	0.33	0.029
484	15.71	15.71	12.98	0.61	0.00	29.	9.02	0.20	0.017	3.94	0.18	0.00	0.013
485	15.71	15.71	27.45	0.44	0.22	34.	16.48	0.16	0.021	10.24	0.16	0.08	0.016
486	15.71	15.71	53.16	0.27	0.57	47.	23.47	0.11	0.025	17.78	0.13	0.18	0.021
487	15.71	15.71	92.31	0.16	1.03	73.	37.18	0.07	0.035	30.84	0.08	0.34	0.030
488	15.71	15.71	10.33	0.64	0.00	28.	8.14	0.21	0.018	3.97	0.17	0.00	0.012
489	15.71	15.71	25.04	0.47	0.17	33.	15.86	0.16	0.021	10.26	0.16	0.08	0.016
490	15.71	15.71	52.12	0.28	0.55	47.	23.27	0.12	0.025	17.97	0.12	0.19	0.021
491	15.71	15.71	91.59	0.14	1.02	71.	37.18	0.07	0.034	30.98	0.08	0.34	0.029
492	15.71	15.71	92.06	-0.06	1.05	66.	34.68	-0.07	0.027	28.78	-0.10	0.33	0.021
493	15.71	15.71	31.89	-0.26	0.37	16.	10.18	-0.17	0.003	6.76	-0.20	0.06	0.001
494	15.71	15.71	93.49	-0.09	1.06	66.	35.24	-0.08	0.027	28.73	-0.09	0.33	0.021
495	15.71	15.71	33.83	-0.25	0.39	17.	11.06	-0.15	0.004	6.68	-0.19	0.06	0.001
496	15.71	15.71	91.07	-0.09	1.04	64.	34.48	-0.07	0.027	28.18	-0.08	0.32	0.021
497	15.71	15.71	33.86	-0.23	0.39	18.	11.21	-0.14	0.005	6.57	-0.17	0.06	0.001
498	15.71	15.71	91.16	-0.09	1.04	64.	34.49	-0.07	0.027	28.22	-0.08	0.32	0.021
499	15.71	15.71	33.98	-0.23	0.39	18.	11.23	-0.14	0.005	6.59	-0.17	0.06	0.001
500	15.71	15.71	95.97	-0.14	1.10	66.	35.81	-0.08	0.027	29.13	-0.09	0.33	0.021
501	15.71	15.71	36.73	-0.29	0.42	18.	12.00	-0.16	0.005	6.48	-0.19	0.06	0.001
502	15.71	15.71	98.71	-0.18	1.13	67.	36.60	-0.08	0.028	28.93	-0.10	0.33	0.021
503	15.71	15.71	38.23	-0.23	0.44	21.	12.74	-0.10	0.007	6.34	-0.15	0.06	0.001
773	15.71	15.71	9.34	0.01	0.10	7.	3.74	0.00	0.003	0.00	0.00	0.00	0.000
774	15.71	15.71	7.94	0.04	0.09	7.	3.43	0.01	0.003	0.00	0.01	0.00	0.001
775	15.71	15.71	17.76	0.03	0.20	14.	6.15	0.01	0.006	0.23	0.01	0.00	0.001
776	15.71	15.71	16.80	0.06	0.18	14.	5.99	0.02	0.006	0.00	0.01	0.00	0.001
777	15.71	15.71	15.69	-0.01	0.18	11.	5.79	0.00	0.005	0.00	0.00	0.00	0.000
778	15.71	15.71	14.06	0.01	0.16	11.	5.33	0.00	0.005	0.00	0.00	0.00	0.000
779	15.71	15.71	11.88	0.01	0.13	9.	4.56	0.00	0.004	0.00	0.00	0.00	0.000
780	15.71	15.71	11.71	0.01	0.13	9.	4.50	0.00	0.004	0.00	0.00	0.00	0.000
781	15.71	15.71	11.13	0.00	0.13	8.	4.33	0.00	0.004	0.00	0.00	0.00	0.000
782	15.71	15.71	9.99	0.02	0.11	8.	3.89	0.01	0.004	0.00	0.01	0.00	0.001

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
443	15.71	15.71	25.10	-0.01	0.28	18.	4.93	0.01	0.004	1.41	0.00	0.02	0.001
444	15.71	15.71	24.06	0.00	0.27	18.	4.80	0.01	0.004	1.51	0.00	0.02	0.001
445	15.71	15.71	24.06	0.00	0.27	18.	4.80	0.01	0.004	1.51	0.00	0.02	0.001
446	15.71	15.71	24.06	0.00	0.27	18.	4.80	0.01	0.004	1.51	0.00	0.02	0.001
447	15.71	15.71	60.00	-0.02	0.68	43.	16.40	0.03	0.015	8.78	0.02	0.10	0.008
448	15.71	15.71	58.23	0.00	0.66	43.	16.09	0.01	0.014	8.95	0.00	0.10	0.008
449	15.71	15.71	58.23	0.00	0.66	43.	16.09	0.01	0.014	8.95	0.00	0.10	0.008
450	15.71	15.71	58.23	0.00	0.66	43.	16.09	0.01	0.014	8.95	0.00	0.10	0.008
451	15.71	15.71	31.51	0.04	0.35	24.	8.19	0.01	0.007	9.02	0.00	0.10	0.008
452	15.71	15.71	35.43	0.00	0.40	26.	9.53	0.02	0.009	9.16	0.00	0.10	0.008
453	15.71	15.71	35.43	0.00	0.40	26.	9.53	0.02	0.009	9.16	0.00	0.10	0.008
454	15.71	15.71	35.43	0.00	0.40	26.	9.53	0.02	0.009	9.16	0.00	0.10	0.008
455	15.71	15.71	3.73	0.00	0.04	3.	0.00	0.01	0.000	1.53	0.00	0.02	0.001
456	15.71	15.71	5.78	0.00	0.07	4.	0.00	0.01	0.000	1.62	0.00	0.02	0.001
457	15.71	15.71	5.78	0.00	0.07	4.	0.00	0.01	0.000	1.62	0.00	0.02	0.001
458	15.71	15.71	5.78	0.00	0.07	4.	0.00	0.01	0.000	1.62	0.00	0.02	0.001
460	15.71	15.71	24.35	0.00	0.28	18.	4.80	0.01	0.004	1.80	0.00	0.02	0.002
461	15.71	15.71	59.11	0.00	0.67	43.	16.33	0.01	0.014	10.01	0.00	0.11	0.008
462	15.71	15.71	40.20	0.02	0.45	30.	11.20	0.01	0.010	10.19	0.00	0.12	0.009
463	15.71	15.71	6.96	0.00	0.08	5.	0.67	0.01	0.001	1.90	0.00	0.02	0.002
464	15.71	15.71	50.11	0.02	0.57	37.	14.42	0.00	0.012	12.32	0.01	0.14	0.011
465	15.71	15.71	8.90	0.00	0.10	6.	2.09	0.00	0.002	2.52	0.00	0.03	0.002
466	15.71	15.71	24.92	0.00	0.28	18.	4.91	0.01	0.004	2.44	0.00	0.03	0.002
467	15.71	15.71	62.20	0.03	0.70	47.	16.99	0.01	0.015	12.20	0.01	0.14	0.011
468	15.71	15.71	68.28	0.22	0.75	57.	20.04	0.07	0.020	8.66	0.08	0.09	0.011
469	15.71	15.71	66.51	0.09	0.74	52.	19.59	0.04	0.018	9.10	0.05	0.10	0.010
470	15.71	15.71	66.51	0.09	0.74	52.	19.59	0.04	0.018	9.10	0.05	0.10	0.010
471	15.71	15.71	66.51	0.09	0.74	52.	19.59	0.04	0.018	9.10	0.05	0.10	0.010
472	15.71	15.71	43.92	0.19	0.47	38.	10.15	0.06	0.011	3.70	0.09	0.01	0.007
473	15.71	15.71	42.46	0.19	0.46	37.	9.61	0.06	0.011	3.59	0.09	0.01	0.007
474	15.71	15.71	42.46	0.19	0.46	37.	9.61	0.06	0.011	3.59	0.09	0.01	0.007
475	15.71	15.71	42.46	0.19	0.46	37.	9.61	0.06	0.011	3.59	0.09	0.01	0.007
476	15.71	15.71	36.91	0.27	0.38	35.	10.71	0.08	0.013	2.44	0.06	0.00	0.005

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
477	15.71	15.71	35.12	0.23	0.37	33.	9.87	0.07	0.011	1.80	0.06	0.00	0.005
478	15.71	15.71	35.12	0.23	0.37	33.	9.87	0.07	0.011	1.80	0.06	0.00	0.005
479	15.71	15.71	35.12	0.23	0.37	33.	9.87	0.07	0.011	1.80	0.06	0.00	0.005
480	15.71	15.71	35.44	0.23	0.37	33.	10.85	0.06	0.012	2.14	0.05	0.01	0.004
481	15.71	15.71	34.53	0.25	0.36	33.	10.30	0.07	0.012	1.50	0.05	0.00	0.004
482	15.71	15.71	34.53	0.25	0.36	33.	10.30	0.07	0.012	1.50	0.05	0.00	0.004
483	15.71	15.71	34.53	0.25	0.36	33.	10.30	0.07	0.012	1.50	0.05	0.00	0.004
484	15.71	15.71	31.33	0.25	0.32	31.	8.37	0.07	0.010	3.59	0.06	0.03	0.006
485	15.71	15.71	32.88	0.24	0.34	32.	8.78	0.07	0.011	3.48	0.04	0.03	0.005
486	15.71	15.71	32.88	0.24	0.34	32.	8.78	0.07	0.011	3.48	0.04	0.03	0.005
487	15.71	15.71	32.88	0.24	0.34	32.	8.78	0.07	0.011	3.48	0.04	0.03	0.005
488	15.71	15.71	28.64	0.98	0.00	52.	8.56	0.29	0.022	8.92	0.19	0.05	0.017
489	15.71	15.71	32.98	0.94	0.00	54.	9.89	0.28	0.023	9.33	0.19	0.05	0.017
490	15.71	15.71	32.98	0.94	0.00	54.	9.89	0.28	0.023	9.33	0.19	0.05	0.017
491	15.71	15.71	32.98	0.94	0.00	54.	9.89	0.28	0.023	9.33	0.19	0.05	0.017
492	15.71	15.71	67.51	0.09	0.75	52.	20.03	0.04	0.019	9.98	0.05	0.11	0.011
493	15.71	15.71	68.03	0.13	0.76	54.	20.08	0.05	0.019	11.93	0.08	0.12	0.014
494	15.71	15.71	41.96	0.18	0.45	36.	9.37	0.06	0.011	3.70	0.09	0.02	0.007
495	15.71	15.71	41.07	0.19	0.44	36.	8.82	0.07	0.010	4.02	0.09	0.02	0.008
496	15.71	15.71	34.42	0.22	0.36	32.	9.54	0.06	0.011	1.46	0.06	0.00	0.004
497	15.71	15.71	33.30	0.18	0.35	30.	9.02	0.05	0.010	0.82	0.05	0.00	0.003
498	15.71	15.71	34.80	0.27	0.35	34.	10.26	0.08	0.012	1.14	0.06	0.00	0.004
499	15.71	15.71	35.42	0.28	0.36	35.	10.26	0.08	0.012	0.49	0.06	0.00	0.004
500	15.71	15.71	35.47	0.25	0.37	34.	9.57	0.07	0.011	3.57	0.04	0.03	0.005
501	15.71	15.71	41.07	0.38	0.41	42.	11.40	0.11	0.015	3.88	0.07	0.03	0.007
502	15.71	15.71	37.68	0.95	0.10	58.	11.51	0.29	0.024	10.18	0.19	0.07	0.018
503	15.71	15.71	50.77	0.76	0.42	61.	15.81	0.23	0.024	12.07	0.18	0.10	0.019
773	15.71	15.71	20.74	0.00	0.23	15.	4.65	0.01	0.004	7.88	0.00	0.09	0.007
774	15.71	15.71	1.71	0.00	0.02	1.	0.00	0.01	0.001	1.55	0.00	0.02	0.001
775	15.71	15.71	27.11	0.02	0.30	21.	5.52	0.01	0.005	1.39	0.00	0.02	0.001
776	15.71	15.71	59.90	0.01	0.68	44.	16.44	0.00	0.014	7.59	-0.01	0.09	0.006
777	15.71	15.71	70.33	0.17	0.78	57.	20.49	0.05	0.020	6.78	0.07	0.07	0.009
778	15.71	15.71	46.30	0.24	0.50	41.	11.44	0.07	0.013	3.61	0.09	0.01	0.008
779	15.71	15.71	39.75	0.24	0.42	37.	12.15	0.07	0.013	3.50	0.07	0.02	0.006
780	15.71	15.71	36.55	0.25	0.38	35.	11.66	0.07	0.013	3.21	0.06	0.02	0.006
781	15.71	15.71	27.12	0.25	0.27	28.	7.11	0.07	0.009	3.50	0.06	0.03	0.006
782	15.71	15.71	14.70	0.95	0.00	41.	4.07	0.28	0.019	7.08	0.16	0.03	0.014

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
443	15.71	15.71	7.54	0.32	0.00	16.	0.00	0.10	0.007	0.00	0.14	0.00	0.010
444	15.71	15.71	5.27	0.35	0.00	15.	0.00	0.12	0.009	0.00	0.15	0.00	0.010
445	15.71	15.71	0.00	0.34	0.00	11.	0.00	0.12	0.009	0.00	0.12	0.00	0.008
446	15.71	15.71	0.00	0.26	0.00	8.	0.00	0.08	0.005	0.00	0.06	0.00	0.005
447	15.71	15.71	13.14	0.38	0.00	22.	0.00	0.12	0.009	0.00	0.15	0.00	0.011
448	15.71	15.71	9.33	0.35	0.00	18.	0.00	0.13	0.009	0.00	0.14	0.00	0.010
449	15.71	15.71	0.00	0.30	0.00	10.	0.00	0.11	0.008	0.00	0.10	0.00	0.007
450	15.71	15.71	0.00	0.21	0.00	7.	0.00	0.06	0.005	0.00	0.06	0.00	0.005
451	15.71	15.71	25.94	0.68	0.04	41.	4.14	0.22	0.016	0.00	0.18	0.00	0.013
452	15.71	15.71	17.20	0.49	0.00	28.	0.00	0.17	0.012	0.00	0.16	0.00	0.012
453	15.71	15.71	0.00	0.31	0.00	10.	0.00	0.12	0.009	0.00	0.13	0.00	0.009
454	15.71	15.71	0.00	0.11	0.00	4.	0.00	0.06	0.004	0.00	0.08	0.00	0.006
455	15.71	15.71	29.11	0.73	0.08	45.	5.20	0.24	0.017	0.00	0.18	0.00	0.013
456	15.71	15.71	19.33	0.54	0.00	31.	0.00	0.18	0.013	0.00	0.17	0.00	0.012
457	15.71	15.71	0.00	0.36	0.00	11.	0.00	0.14	0.010	0.00	0.14	0.00	0.010
458	15.71	15.71	0.00	0.16	0.00	5.	0.00	0.06	0.005	0.00	0.10	0.00	0.007
460	15.71	15.71	0.00	0.02	0.00	1.	0.00	-0.06	0.000	0.00	-0.09	0.01	0.000
461	15.71	15.71	0.00	-0.01	0.00	0.	0.00	-0.06	0.000	0.00	-0.09	0.01	0.000
462	15.71	15.71	0.00	-0.16	0.02	0.	0.00	-0.06	0.000	0.00	-0.08	0.01	0.000
463	15.71	15.71	0.00	-0.14	0.01	0.	0.00	-0.04	0.000	0.00	-0.06	0.01	0.000
464	15.71	15.71	0.00	-0.26	0.02	0.	0.00	-0.10	0.000	0.00	-0.15	0.01	0.000
465	15.71	15.71	0.00	-0.25	0.02	0.	0.00	-0.09	0.000	0.00	-0.13	0.01	0.000
466	15.71	15.71	3.07	-0.05	0.03	1.	0.00	-0.12	0.000	0.00	-0.16	0.01	0.000
467	15.71	15.71	2.37	-0.15	0.00	0.	0.00	-0.14	0.000	0.00	-0.17	0.02	0.000
468	15.71	15.71	15.93	0.55	0.00	29.	0.88	0.17	0.011	0.00	0.17	0.00	0.012
469	15.71	15.71	11.54	0.38	0.00	21.	0.00	0.13	0.009	0.00	0.15	0.00	0.011
470	15.71	15.71	0.00	0.28	0.00	9.	0.00	0.11	0.008	0.00	0.12	0.00	0.008
471	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.06	0.004	0.00	0.08	0.00	0.006
472	15.71	15.71	18.17	0.59	0.00	32.	1.67	0.19	0.013	0.00	0.17	0.00	0.012
473	15.71	15.71	11.62	0.42	0.00	22.	0.00	0.15	0.010	0.00	0.16	0.00	0.011
474	15.71	15.71	0.00	0.28	0.00	9.	0.00	0.11	0.008	0.00	0.12	0.00	0.009
475	15.71	15.71	0.00	0.20	0.00	6.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
476	15.71	15.71	18.26	0.54	0.00	31.	1.40	0.18	0.012	0.00	0.16	0.00	0.011
477	15.71	15.71	10.21	0.40	0.00	20.	0.00	0.14	0.010	0.00	0.15	0.00	0.011
478	15.71	15.71	0.00	0.27	0.00	9.	0.00	0.11	0.008	0.00	0.12	0.00	0.009
479	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
480	15.71	15.71	18.40	0.54	0.00	31.	1.40	0.18	0.012	0.00	0.16	0.00	0.011
481	15.71	15.71	10.23	0.40	0.00	20.	0.00	0.14	0.010	0.00	0.15	0.00	0.011
482	15.71	15.71	0.00	0.27	0.00	8.	0.00	0.11	0.008	0.00	0.12	0.00	0.009
483	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
484	15.71	15.71	20.97	0.61	0.00	35.	2.28	0.20	0.013	0.00	0.18	0.00	0.013
485	15.71	15.71	12.48	0.44	0.00	23.	0.00	0.16	0.011	0.00	0.16	0.00	0.012
486	15.71	15.71	0.00	0.27	0.00	9.	0.00	0.11	0.008	0.00	0.13	0.00	0.009
487	15.71	15.71	0.00	0.16	0.00	5.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
488	15.71	15.71	23.66	0.64	0.00	38.	3.32	0.21	0.015	0.00	0.17	0.00	0.012

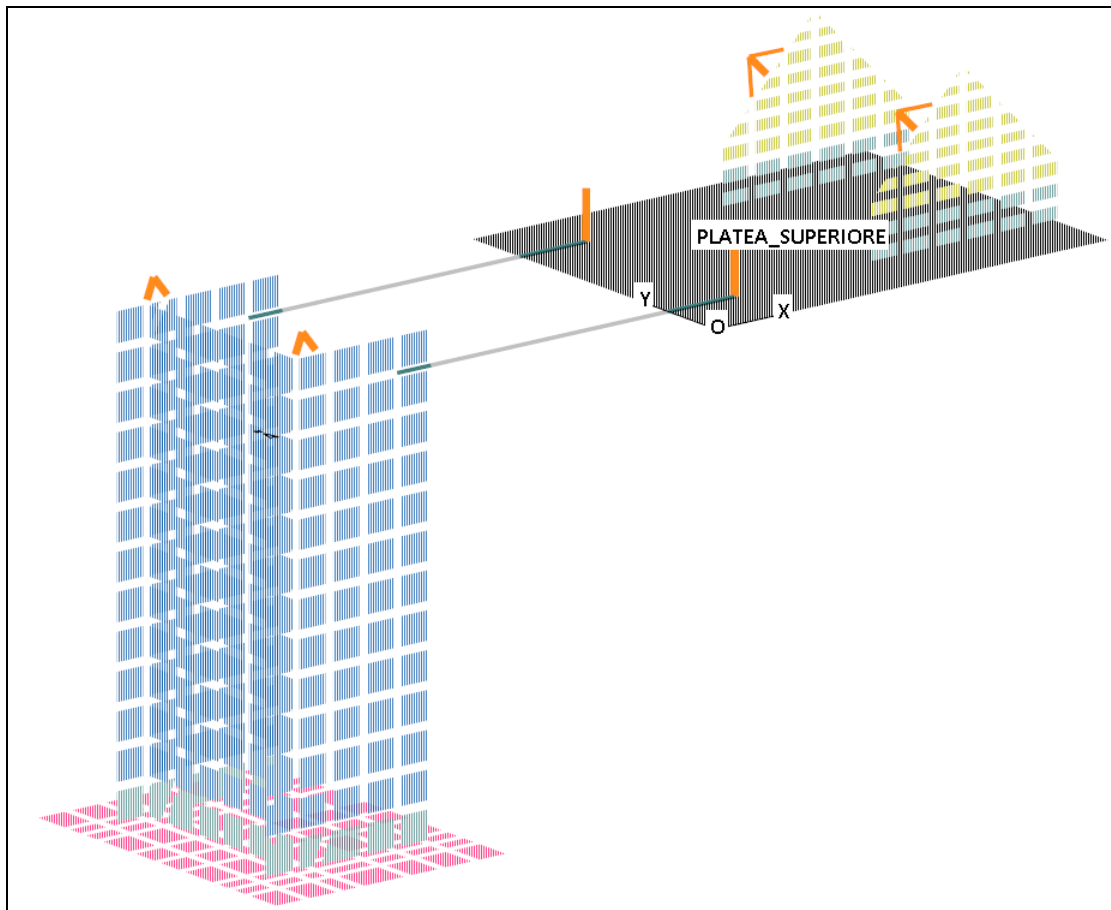
GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
489	15.71	15.71	15.32	0.47	0.00	26.	0.00	0.16	0.012	0.00	0.16	0.00	0.011
490	15.71	15.71	0.00	0.28	0.00	9.	0.00	0.12	0.008	0.00	0.12	0.00	0.009
491	15.71	15.71	0.00	0.14	0.00	4.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
492	15.71	15.71	0.00	-0.06	0.01	0.	0.00	-0.07	0.000	0.00	-0.10	0.01	0.000
493	15.71	15.71	0.98	-0.26	0.02	0.	0.00	-0.17	0.000	0.00	-0.20	0.02	0.000
494	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.08	0.000	0.00	-0.09	0.01	0.000
495	15.71	15.71	0.00	-0.25	0.02	0.	0.00	-0.15	0.000	0.00	-0.19	0.02	0.000
496	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.07	0.000	0.00	-0.08	0.01	0.000
497	15.71	15.71	0.00	-0.23	0.02	0.	0.00	-0.14	0.000	0.00	-0.17	0.02	0.000
498	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.07	0.000	0.00	-0.08	0.01	0.000
499	15.71	15.71	0.00	-0.23	0.02	0.	0.00	-0.14	0.000	0.00	-0.17	0.02	0.000
500	15.71	15.71	0.00	-0.14	0.01	0.	0.00	-0.08	0.000	0.00	-0.09	0.01	0.000
501	15.71	15.71	0.00	-0.29	0.03	0.	0.00	-0.16	0.000	0.00	-0.19	0.02	0.000
502	15.71	15.71	0.00	-0.18	0.02	0.	0.00	-0.08	0.000	0.00	-0.10	0.01	0.000
503	15.71	15.71	0.00	-0.23	0.02	0.	0.00	-0.10	0.000	0.00	-0.15	0.01	0.000
773	15.71	15.71	21.05	0.01	0.24	16.	6.70	0.00	0.006	0.34	0.00	0.00	0.000
774	15.71	15.71	22.57	0.04	0.25	18.	7.35	0.01	0.007	0.40	0.01	0.00	0.001
775	15.71	15.71	7.86	0.03	0.09	7.	2.19	0.01	0.002	0.91	0.01	0.01	0.001
776	15.71	15.71	13.53	0.06	0.15	12.	4.13	0.02	0.004	0.49	0.01	0.00	0.001
777	15.71	15.71	15.63	-0.01	0.18	11.	4.62	0.00	0.004	0.41	0.00	0.00	0.000
778	15.71	15.71	17.08	0.01	0.19	13.	5.08	0.00	0.004	0.42	0.00	0.00	0.000
779	15.71	15.71	17.01	0.01	0.19	13.	5.11	0.00	0.004	0.52	0.00	0.01	0.000
780	15.71	15.71	17.11	0.01	0.19	13.	5.15	0.00	0.004	0.53	0.00	0.01	0.000
781	15.71	15.71	18.86	0.00	0.21	14.	5.71	0.00	0.005	0.59	0.00	0.01	0.000
782	15.71	15.71	19.98	0.02	0.22	15.	6.19	0.01	0.006	0.42	0.01	0.00	0.001

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
443	15.71	15.71	2.00	-0.01	0.02	1.	0.24	0.01	0.000	0.71	0.00	0.01	0.001
444	15.71	15.71	1.57	0.00	0.02	1.	0.00	0.01	0.000	0.37	0.00	0.00	0.000
445	15.71	15.71	1.57	0.00	0.02	1.	0.00	0.01	0.000	0.37	0.00	0.00	0.000
446	15.71	15.71	1.57	0.00	0.02	1.	0.00	0.01	0.000	0.37	0.00	0.00	0.000
447	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.03	0.002	0.00	0.02	0.00	0.002
448	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
449	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
450	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
451	15.71	15.71	0.00	0.04	0.00	1.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
452	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.02	0.001	0.00	0.00	0.00	0.000
453	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.02	0.001	0.00	0.00	0.00	0.000
454	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.02	0.001	0.00	0.00	0.00	0.000
455	15.71	15.71	0.00	0.00	0.00	0.	0.90	0.01	0.001	0.72	0.00	0.01	0.001
456	15.71	15.71	0.00	0.00	0.00	0.	0.35	0.01	0.001	0.39	0.00	0.00	0.000
457	15.71	15.71	0.00	0.00	0.00	0.	0.35	0.01	0.001	0.39	0.00	0.00	0.000
458	15.71	15.71	0.00	0.00	0.00	0.	0.35	0.01	0.001	0.39	0.00	0.00	0.000
460	15.71	15.71	1.82	0.00	0.02	1.	0.00	0.01	0.000	0.15	0.00	0.00	0.000
461	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
462	15.71	15.71	0.00	0.02	0.00	1.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
463	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.000	0.17	0.00	0.00	0.000
464	15.71	15.71	0.00	0.02	0.00	1.	0.00	0.00	0.000	0.00	0.01	0.00	0.000
465	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
466	15.71	15.71	1.51	0.00	0.02	1.	0.00	0.01	0.000	0.00	0.00	0.00	0.000
467	15.71	15.71	0.00	0.03	0.00	1.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
468	15.71	15.71	0.00	0.22	0.00	7.	0.00	0.07	0.005	0.00	0.08	0.00	0.006
469	15.71	15.71	0.00	0.09	0.00	3.	0.00	0.04	0.003	0.00	0.05	0.00	0.004
470	15.71	15.71	0.00	0.09	0.00	3.	0.00	0.04	0.003	0.00	0.05	0.00	0.004
471	15.71	15.71	0.00	0.09	0.00	3.	0.00	0.04	0.003	0.00	0.05	0.00	0.004
472	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.06	0.005	0.00	0.09	0.00	0.006
473	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.06	0.004	0.00	0.09	0.00	0.006
474	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.06	0.004	0.00	0.09	0.00	0.006
475	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.06	0.004	0.00	0.09	0.00	0.006
476	15.71	15.71	15.05	0.27	0.11	19.	3.52	0.08	0.007	0.00	0.06	0.00	0.005
477	15.71	15.71	16.47	0.23	0.14	19.	4.62	0.07	0.007	0.00	0.06	0.00	0.004
478	15.71	15.71	16.47	0.23	0.14	19.	4.62	0.07	0.007	0.00	0.06	0.00	0.004
479	15.71	15.71	16.47	0.23	0.14	19.	4.62	0.07	0.007	0.00	0.06	0.00	0.004
480	15.71	15.71	22.67	0.23	0.22	24.	7.20	0.06	0.009	0.00	0.05	0.00	0.003
481	15.71	15.71	23.02	0.25	0.22	25.	8.08	0.07	0.010	0.00	0.05	0.00	0.004
482	15.71	15.71	23.02	0.25	0.22	25.	8.08	0.07	0.010	0.00	0.05	0.00	0.004
483	15.71	15.71	23.02	0.25	0.22	25.	8.08	0.07	0.010	0.00	0.05	0.00	0.004
484	15.71	15.71	23.96	0.25	0.23	25.	9.98	0.07	0.012	0.00	0.06	0.00	0.004
485	15.71	15.71	21.33	0.24	0.20	23.	9.57	0.07	0.011	0.00	0.04	0.00	0.003
486	15.71	15.71	21.33	0.24	0.20	23.	9.57	0.07	0.011	0.00	0.04	0.00	0.003
487	15.71	15.71	21.33	0.24	0.20	23.	9.57	0.07	0.011	0.00	0.04	0.00	0.003
488	15.71	15.71	0.00	0.98	0.00	31.	0.00	0.29	0.021	0.00	0.19	0.00	0.013
489	15.71	15.71	0.00	0.94	0.00	30.	0.00	0.28	0.020	0.00	0.19	0.00	0.014
490	15.71	15.71	0.00	0.94	0.00	30.	0.00	0.28	0.020	0.00	0.19	0.00	0.014
491	15.71	15.71	0.00	0.94	0.00	30.	0.00	0.28	0.020	0.00	0.19	0.00	0.014
492	15.71	15.71	0.00	0.09	0.00	3.	0.00	0.04	0.003	0.00	0.05	0.00	0.004
493	15.71	15.71	0.00	0.13	0.00	4.	0.00	0.05	0.004	0.00	0.08	0.00	0.006
494	15.71	15.71	0.00	0.18	0.00	6.	0.00	0.06	0.004	0.00	0.09	0.00	0.006
495	15.71	15.71	0.00	0.19	0.00	6.	0.00	0.07	0.005	0.00	0.09	0.00	0.006
496	15.71	15.71	18.36	0.22	0.17	21.	5.09	0.06	0.007	0.00	0.06	0.00	0.004
497	15.71	15.71	19.18	0.18	0.19	20.	5.71	0.05	0.007	0.31	0.05	0.00	0.003
498	15.71	15.71	24.01	0.27	0.22	26.	8.11	0.08	0.011	0.00	0.06	0.00	0.004
499	15.71	15.71	26.01	0.28	0.25	28.	8.28	0.08	0.011	0.21	0.06	0.00	0.004
500	15.71	15.71	19.90	0.25	0.18	22.	8.53	0.07	0.010	0.00	0.04	0.00	0.003

501	15.71	15.71	13.92	0.38	0.00	22.	6.24	0.11	0.011	0.00	0.07	0.00	0.005
502	15.71	15.71	0.00	0.95	0.00	30.	0.00	0.29	0.020	0.00	0.19	0.00	0.014
503	15.71	15.71	0.00	0.76	0.00	24.	0.00	0.23	0.016	0.00	0.18	0.00	0.013
773	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.01	0.001	0.00	0.00	0.00	0.000
774	15.71	15.71	0.00	0.00	0.00	0.	1.75	0.01	0.002	1.29	0.00	0.01	0.001
775	15.71	15.71	4.01	0.02	0.04	4.	1.00	0.01	0.001	1.28	0.00	0.01	0.001
776	15.71	15.71	0.00	0.01	0.00	0.	0.00	0.00	0.000	0.00	-0.01	0.00	0.000
777	15.71	15.71	0.00	0.17	0.00	6.	0.00	0.05	0.004	0.00	0.07	0.00	0.005
778	15.71	15.71	0.00	0.24	0.00	8.	0.00	0.07	0.005	0.00	0.09	0.00	0.006
779	15.71	15.71	12.59	0.24	0.08	17.	2.13	0.07	0.005	0.00	0.07	0.00	0.005
780	15.71	15.71	22.23	0.25	0.21	24.	6.55	0.07	0.009	0.00	0.06	0.00	0.005
781	15.71	15.71	29.75	0.25	0.30	30.	12.42	0.07	0.014	0.00	0.06	0.00	0.004
782	15.71	15.71	17.03	0.95	0.00	43.	4.46	0.28	0.019	0.00	0.16	0.00	0.012

6.2. PLATEA SUPERIORE



G521	G520	G519	G518	G517	G516	G509	G508	G507	G506	G505	G504
G527	G526	G525	G524	G523	G522	G515	G514	G513	G512	G511	G510
G593	G592	G591	G590	G589	G588	G557	G556	G555	G554	G553	G552
G599	G598	G597	G596	G595	G594	G563	G562	G561	G560	G559	G558
G605	G604	G603	G602	G601	G600	G569	G568	G567	G566	G565	G564
G611	G610	G609	G608	G607	G606	G575	G574	G573	G572	G571	G570
G617	G616	G615	G614	G613	G612	G581	G580	G579	G578	G577	G576
G623	G622	G621	G620	G619	G618	G587	G586	G585	G584	G583	G582
G545	G544	G543	G542	G541	G540	G533	G532	G531	G530	G529	G528
G551	G550	G549	G548	G547	G546	G539	G538	G537	G536	G535	G534

6.2.1. Verifica SLU

GUSCI	spess	INFERIORE ORIZZONTALE				INFERIORE VERTICALE				
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	
504	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	5.
505	1.5	15.71	15.71	30.	0.	0.01	0.06	15.71	15.71	5.
506	1.5	15.71	15.71	68.	-1.	0.03	0.14	15.71	15.71	5.
507	1.5	15.71	15.71	123.	-1.	0.05	0.25	15.71	15.71	5.
508	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	7.
509	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	7.
510	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	1.
511	1.5	15.71	15.71	30.	0.	0.01	0.06	15.71	15.71	7.
512	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	6.
513	1.5	15.71	15.71	122.	-1.	0.05	0.25	15.71	15.71	5.
514	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	4.
515	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	4.
516	1.5	15.71	15.71	301.	-2.	0.11	0.58	15.71	15.71	7.
517	1.5	15.71	15.71	314.	-2.	0.12	0.60	15.71	15.71	7.
518	1.5	15.71	15.71	314.	-2.	0.12	0.60	15.71	15.71	8.
519	1.5	15.71	15.71	300.	-2.	0.11	0.57	15.71	15.71	9.
520	1.5	15.71	15.71	192.	-1.	0.07	0.38	15.71	15.71	9.
521	1.5	15.71	15.71	145.	-1.	0.05	0.29	15.71	15.71	10.
522	1.5	15.71	15.71	301.	-2.	0.11	0.57	15.71	15.71	4.
523	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	4.
524	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	8.
525	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	12.
526	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	17.
527	1.5	15.71	15.71	140.	-1.	0.05	0.29	15.71	15.71	22.
528	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	1.
529	1.5	15.71	15.71	30.	0.	0.01	0.06	15.71	15.71	3.
530	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	5.
531	1.5	15.71	15.71	122.	-1.	0.05	0.25	15.71	15.71	6.
532	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	4.
533	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	3.
534	1.5	15.71	15.71	9.	0.	0.00	0.02	15.71	15.71	5.
535	1.5	15.71	15.71	30.	0.	0.01	0.06	15.71	15.71	5.
536	1.5	15.71	15.71	68.	-1.	0.03	0.14	15.71	15.71	5.
537	1.5	15.71	15.71	123.	-1.	0.05	0.25	15.71	15.71	5.
538	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	8.
539	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	8.
540	1.5	15.71	15.71	301.	-2.	0.11	0.57	15.71	15.71	3.
541	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	3.
542	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	7.
543	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	11.
544	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	15.
545	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	19.
546	1.5	15.71	15.71	301.	-2.	0.11	0.57	15.71	15.71	8.
547	1.5	15.71	15.71	313.	-2.	0.12	0.60	15.71	15.71	8.
548	1.5	15.71	15.71	311.	-2.	0.12	0.59	15.71	15.71	9.
549	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	10.
550	1.5	15.71	15.71	194.	-1.	0.07	0.40	15.71	15.71	11.
551	1.5	15.71	15.71	142.	-1.	0.05	0.29	15.71	15.71	12.
552	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	14.
553	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	17.
554	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	17.
555	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	19.
556	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	23.
557	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	23.
558	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	21.
559	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	19.
560	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	23.
561	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	28.
562	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	33.
563	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	33.
564	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	30.
565	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	32.
566	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	33.
567	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	37.
568	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	41.
569	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	41.
570	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	33.
571	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	33.
572	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	35.
573	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	35.
574	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	36.
575	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	36.
576	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	27.
577	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	25.
578	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	23.
579	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	22.
580	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	28.
581	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	28.
582	1.5	15.71	15.71	8.	0.	0.00	0.02	15.71	15.71	13.
583	1.5	15.71	15.71	29.	0.	0.01	0.06	15.71	15.71	14.
584	1.5	15.71	15.71	66.	-1.	0.03	0.14	15.71	15.71	14.
585	1.5	15.71	15.71	121.	-1.	0.05	0.25	15.71	15.71	10.
586	1.5	15.71	15.71	194.	-1.	0.07	0.39	15.71	15.71	15.
587	1.5	15.71	15.71	263.	-2.	0.10	0.51	15.71	15.71	15.

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
588	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	23.	0.	0.00	0.06	
589	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	23.	0.	0.00	0.06	
590	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	27.	0.	0.01	0.07	
591	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	33.	0.	0.01	0.08	
592	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	40.	0.	0.01	0.10	
593	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	48.	0.	0.00	0.13	
594	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	33.	0.	0.01	0.07	
595	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	33.	0.	0.01	0.07	
596	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	35.	0.	0.01	0.08	
597	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	38.	0.	0.01	0.08	
598	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	41.	0.	0.01	0.09	
599	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	46.	0.	0.01	0.11	
600	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	41.	0.	0.01	0.09	
601	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	41.	0.	0.01	0.09	
602	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	41.	0.	0.01	0.09	
603	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	42.	0.	0.02	0.09	
604	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	43.	0.	0.02	0.10	
605	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	44.	0.	0.02	0.10	
606	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	36.	0.	0.01	0.08	
607	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	36.	0.	0.01	0.08	
608	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	35.	0.	0.01	0.08	
609	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	35.	0.	0.01	0.08	
610	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	35.	0.	0.01	0.08	
611	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	34.	0.	0.01	0.08	
612	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	28.	0.	0.01	0.07	
613	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	28.	0.	0.01	0.07	
614	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	30.	0.	0.01	0.07	
615	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	32.	0.	0.01	0.07	
616	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	35.	0.	0.01	0.08	
617	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	38.	0.	0.01	0.09	
618	1.5	15.71	15.71	302.	-2.	0.11	0.57	15.71	15.71	15.	0.	0.00	0.04	
619	1.5	15.71	15.71	315.	-2.	0.12	0.60	15.71	15.71	15.	0.	0.00	0.04	
620	1.5	15.71	15.71	314.	-2.	0.12	0.59	15.71	15.71	20.	0.	0.00	0.06	
621	1.5	15.71	15.71	299.	-2.	0.11	0.57	15.71	15.71	26.	0.	0.00	0.07	
622	1.5	15.71	15.71	195.	-1.	0.07	0.39	15.71	15.71	32.	0.	0.00	0.09	
623	1.5	15.71	15.71	139.	-1.	0.05	0.28	15.71	15.71	39.	0.	0.00	0.11	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
504	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	3.	0.	0.00	0.01	
505	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	3.	0.	0.00	0.01	
506	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	3.	0.	0.00	0.01	
507	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	4.	0.	0.00	0.02	
508	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	6.	0.	0.00	0.02	
509	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	6.	0.	0.00	0.02	
510	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	12.	0.	0.00	0.05	
511	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	11.	0.	0.00	0.05	
512	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	12.	0.	0.00	0.05	
513	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	17.	0.	0.00	0.05	
514	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	22.	0.	0.01	0.06	
515	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.01	0.06	
516	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	6.	0.	0.00	0.02	
517	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	6.	0.	0.00	0.02	
518	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	5.	0.	0.00	0.02	
519	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	5.	0.	0.00	0.02	
520	1.5	15.71	15.71	86.	-1.	0.03	0.17	15.71	15.71	4.	0.	0.00	0.02	
521	1.5	15.71	15.71	114.	-1.	0.04	0.23	15.71	15.71	4.	0.	0.00	0.02	
522	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.01	0.06	
523	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.01	0.06	
524	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	21.	0.	0.00	0.06	
525	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	18.	0.	0.00	0.06	
526	1.5	15.71	15.71	64.	-1.	0.03	0.13	15.71	15.71	16.	0.	0.00	0.06	
527	1.5	15.71	15.71	105.	-1.	0.04	0.21	15.71	15.71	14.	0.	0.00	0.06	
528	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	15.	0.	0.00	0.05	
529	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	13.	0.	0.00	0.05	
530	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	15.	0.	0.00	0.06	
531	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	17.	0.	0.00	0.07	
532	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	22.	0.	0.00	0.06	
533	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.00	0.06	
534	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	4.	0.	0.00	0.01	
535	1.5	15.71	15.71	0.	0.	0.00	0.00	15.71	15.71	3.	0.	0.00	0.01	
536	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	4.	0.	0.00	0.01	
537	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	5.	0.	0.00	0.02	
538	1.5	15.71	15.71	0.	-1.	0.00	0.00	15.71	15.71	5.	0.	0.00	0.01	
539	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	5.	0.	0.00	0.01	
540	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.00	0.06	
541	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	22.	0.	0.00	0.06	
542	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	20.	0.	0.00	0.07	
543	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	18.	0.	0.00	0.06	
544	1.5	15.71	15.71	58.	-1.	0.02	0.11	15.71	15.71	15.	0.	0.00	0.06	
545	1.5	15.71	15.71	103.	-1.	0.04	0.21	15.71	15.71	12.	0.	0.00	0.06	
546	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	5.	0.	0.00	0.01	
547	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	5.	0.	0.00	0.01	
548	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	4.	0.	0.00	0.01	
549	1.5	15.71	15.71	0.	-2.	0.01	-0.01	15.71	15.71	4.	0.	0.00	0.01	
550	1.5	15.71	15.71	53.	-1.	0.02	0.10	15.71	15.71	3.	0.	0.00	0.01	
551	1.5	15.71	15.71	101.	-1.	0.04	0.21	15.71	15.71	3.	0.	0.00	0.01	

GUSCI	spess	SUPERIORE ORIZZONTALE							SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF		Af	Afc	Mom	Nor	epsC	epsF	
552	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	11.	0.	0.00	0.06	
553	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	8.	0.	0.00	0.05	
554	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	5.	0.	0.00	0.03	
555	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	9.	0.	0.00	0.04	
556	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	15.	0.	0.00	0.04	
557	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	15.	0.	0.00	0.04	
558	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.01	
559	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.01	
560	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
561	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
562	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.01	
563	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
564	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
565	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
566	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
567	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
568	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
569	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
570	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
571	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
572	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
573	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
574	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
575	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
576	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.01	
577	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
578	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
579	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.00	
580	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	0.	0.	0.00	0.01	
581	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
582	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	13.	0.	0.00	0.06	
583	1.5	15.71	15.71	0.	0.	0.00	0.00		15.71	15.71	9.	0.	0.00	0.05	
584	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	11.	0.	0.00	0.05	
585	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	13.	0.	0.00	0.05	
586	1.5	15.71	15.71	0.	-1.	0.00	0.00		15.71	15.71	19.	0.	0.00	0.06	
587	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	19.	0.	0.00	0.06	
588	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	15.	0.	0.00	0.04	
589	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	15.	0.	0.00	0.04	
590	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	13.	0.	0.00	0.04	
591	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	11.	0.	0.00	0.04	
592	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	8.	0.	0.00	0.03	
593	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	5.	0.	0.00	0.03	
594	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
595	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
596	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
597	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
598	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	0.	0.	0.00	0.00	
599	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	0.	0.	0.00	0.01	
600	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
601	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
602	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
603	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
604	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	0.	0.	0.00	0.00	
605	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	0.	0.	0.00	0.00	
606	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
607	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
608	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
609	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.00	
610	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	0.	0.	0.00	0.00	
611	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	0.	0.	0.00	0.00	
612	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
613	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
614	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
615	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	0.	0.	0.00	0.01	
616	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	0.	0.	0.00	0.01	
617	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	0.	0.	0.00	0.01	
618	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	19.	0.	0.00	0.06	
619	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	19.	0.	0.00	0.06	
620	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	17.	0.	0.00	0.06	
621	1.5	15.71	15.71	0.	-2.	0.01	-0.01		15.71	15.71	15.	0.	0.00	0.06	
622	1.5	15.71	15.71	59.	-1.	0.03	0.12		15.71	15.71	12.	0.	0.00	0.06	
623	1.5	15.71	15.71	101.	-1.	0.04	0.21		15.71	15.71	10.	0.	0.00	0.06	

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO ($R_d > E_d$)

6.2.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
504	15.71	15.71	4.61	-0.08	0.02	0.	1.20	-0.03	0.000	1.17	-0.03	0.01	0.000
505	15.71	15.71	17.34	-0.24	0.09	2.	1.34	-0.11	0.000	1.11	-0.11	0.01	0.000

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
506	15.71	15.71	37.67	-0.47	0.20	5.	0.00	-0.19	0.000	0.00	-0.20	0.01	0.000
507	15.71	15.71	66.97	-0.73	0.36	11.	0.00	-0.28	0.000	0.00	-0.30	0.02	0.000
508	15.71	15.71	105.07	-0.99	0.59	21.	0.00	-0.37	0.000	0.00	-0.39	0.03	0.000
509	15.71	15.71	143.47	-1.27	0.81	32.	0.00	-0.42	0.000	0.00	-0.46	0.03	0.000
510	15.71	15.71	4.36	-0.10	0.02	0.	0.97	-0.04	0.000	0.93	-0.04	0.01	0.000
511	15.71	15.71	16.82	-0.28	0.08	1.	1.14	-0.12	0.000	0.87	-0.12	0.01	0.000
512	15.71	15.71	36.78	-0.51	0.19	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
513	15.71	15.71	66.08	-0.77	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
514	15.71	15.71	105.00	-1.03	0.58	21.	0.00	-0.38	0.000	0.00	-0.40	0.03	0.000
515	15.71	15.71	143.74	-1.30	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
516	15.71	15.71	159.80	-1.53	0.89	32.	0.00	-0.47	0.000	0.00	-0.51	0.03	0.000
517	15.71	15.71	155.75	-1.51	0.86	31.	0.00	-0.47	0.000	0.00	-0.51	0.03	0.000
518	15.71	15.71	143.35	-1.52	0.78	25.	0.00	-0.46	0.000	0.00	-0.51	0.03	0.000
519	15.71	15.71	121.45	-1.54	0.63	16.	0.00	-0.45	0.000	0.00	-0.51	0.03	0.000
520	15.71	15.71	65.43	-1.00	0.32	6.	0.00	-0.27	0.000	0.00	-0.34	0.02	0.000
521	15.71	15.71	33.65	-0.67	0.15	1.	0.00	-0.22	0.000	0.00	-0.27	0.02	0.000
522	15.71	15.71	160.46	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
523	15.71	15.71	155.85	-1.54	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
524	15.71	15.71	142.72	-1.54	0.77	25.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
525	15.71	15.71	120.31	-1.56	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000
526	15.71	15.71	67.56	-1.03	0.33	6.	0.00	-0.30	0.000	0.00	-0.37	0.02	0.000
527	15.71	15.71	30.72	-0.59	0.14	1.	0.00	-0.22	0.000	0.00	-0.27	0.02	0.000
528	15.71	15.71	4.35	-0.09	0.02	0.	1.05	-0.04	0.000	1.00	-0.04	0.01	0.000
529	15.71	15.71	16.78	-0.27	0.08	1.	1.18	-0.12	0.000	0.94	-0.12	0.01	0.000
530	15.71	15.71	36.73	-0.50	0.19	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
531	15.71	15.71	66.07	-0.77	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
532	15.71	15.71	105.07	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.40	0.03	0.000
533	15.71	15.71	143.69	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
534	15.71	15.71	4.57	-0.08	0.02	0.	1.29	-0.03	0.000	1.24	-0.03	0.01	0.000
535	15.71	15.71	17.17	-0.24	0.09	2.	1.39	-0.11	0.000	1.17	-0.10	0.01	0.000
536	15.71	15.71	37.40	-0.47	0.19	5.	0.00	-0.19	0.000	0.00	-0.20	0.01	0.000
537	15.71	15.71	66.67	-0.73	0.36	11.	0.00	-0.28	0.000	0.00	-0.30	0.02	0.000
538	15.71	15.71	104.84	-1.00	0.58	21.	0.00	-0.37	0.000	0.00	-0.39	0.03	0.000
539	15.71	15.71	142.95	-1.29	0.80	31.	0.00	-0.42	0.000	0.00	-0.46	0.03	0.000
540	15.71	15.71	160.34	-1.56	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
541	15.71	15.71	155.37	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
542	15.71	15.71	141.98	-1.55	0.77	24.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000
543	15.71	15.71	120.12	-1.57	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000
544	15.71	15.71	68.66	-1.02	0.34	7.	0.00	-0.31	0.000	0.00	-0.37	0.02	0.000
545	15.71	15.71	31.08	-0.58	0.14	2.	0.00	-0.22	0.000	0.00	-0.27	0.02	0.000
546	15.71	15.71	159.66	-1.56	0.88	31.	0.00	-0.47	0.000	0.00	-0.51	0.03	0.000
547	15.71	15.71	154.10	-1.53	0.85	30.	0.00	-0.46	0.000	0.00	-0.51	0.03	0.000
548	15.71	15.71	140.05	-1.51	0.76	24.	0.00	-0.46	0.000	0.00	-0.51	0.03	0.000
549	15.71	15.71	119.91	-1.54	0.62	15.	0.00	-0.45	0.000	0.00	-0.51	0.03	0.000
550	15.71	15.71	70.99	-0.96	0.36	8.	0.00	-0.32	0.000	0.00	-0.34	0.02	0.000
551	15.71	15.71	33.52	-0.60	0.15	2.	0.00	-0.25	0.000	0.00	-0.27	0.02	0.000
552	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
553	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
554	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
555	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
556	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
557	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
558	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
559	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
560	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
561	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
562	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
563	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
564	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
565	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
566	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
567	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
568	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
569	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
570	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
571	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
572	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
573	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
574	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
575	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
576	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
577	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
578	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
579	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
580	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
581	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
582	15.71	15.71	4.25	-0.09	0.02	0.	1.01	-0.04	0.000	0.96	-0.04	0.01	0.000
583	15.71	15.71	16.67	-0.28	0.08	1.	1.13	-0.12	0.000	0.88	-0.12	0.01	0.000
584	15.71	15.71	36.65	-0.51	0.18	4.	0.00	-0.20	0.000	0.00	-0.22	0.01	0.000
585	15.71	15.71	66.02	-0.78	0.35	10.	0.00	-0.30	0.000	0.00	-0.32	0.02	0.000
586	15.71	15.71	105.14	-1.04	0.58	20.	0.00	-0.38	0.000	0.00	-0.41	0.03	0.000
587	15.71	15.71	143.83	-1.31	0.81	31.	0.00	-0.43	0.000	0.00	-0.47	0.03	0.000
588	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
589	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
590	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000
591	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000
592	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000

			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP	
593	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	
594	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
595	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
596	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
597	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000	
598	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000	
599	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	
600	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
601	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
602	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
603	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000	
604	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000	
605	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	
606	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
607	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
608	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
609	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000	
610	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000	
611	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	
612	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
613	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
614	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
615	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000	
616	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000	
617	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	
618	15.71	15.71	160.60	-1.55	0.89	32.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
619	15.71	15.71	155.92	-1.55	0.86	30.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
620	15.71	15.71	142.53	-1.55	0.77	24.	0.00	-0.47	0.000	0.00	-0.52	0.03	0.000	
621	15.71	15.71	119.93	-1.55	0.62	15.	0.00	-0.46	0.000	0.00	-0.52	0.03	0.000	
622	15.71	15.71	68.10	-1.00	0.33	7.	0.00	-0.30	0.000	0.00	-0.36	0.02	0.000	
623	15.71	15.71	30.37	-0.57	0.14	2.	0.00	-0.21	0.000	0.00	-0.26	0.02	0.000	

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom		Nor	σc
504	15.71	15.71	2.37	0.02	0.01	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
505	15.71	15.71	2.47	0.01	0.01	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
506	15.71	15.71	2.16	0.01	0.01	1.	0.00	0.01	0.000	0.00	0.01	0.00	0.000
507	15.71	15.71	1.50	0.00	0.01	1.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
508	15.71	15.71	1.06	0.00	0.01	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
509	15.71	15.71	1.06	0.00	0.01	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
510	15.71	15.71	0.00	0.10	0.00	3.	0.00	0.02	0.002	0.00	0.03	0.00	0.002
511	15.71	15.71	0.70	0.10	0.00	3.	0.00	0.02	0.002	0.00	0.03	0.00	0.002
512	15.71	15.71	0.00	0.08	0.00	3.	0.00	0.03	0.002	0.00	0.03	0.00	0.002
513	15.71	15.71	0.00	0.05	0.00	2.	0.00	0.02	0.001	0.00	0.03	0.00	0.002
514	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
515	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
516	15.71	15.71	1.06	0.00	0.01	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
517	15.71	15.71	1.06	0.00	0.01	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
518	15.71	15.71	1.45	0.00	0.01	1.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
519	15.71	15.71	2.06	0.01	0.01	1.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
520	15.71	15.71	3.02	0.01	0.02	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
521	15.71	15.71	3.74	0.01	0.02	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
522	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
523	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
524	15.71	15.71	0.00	0.01	0.00	0.	0.00	0.01	0.000	0.00	0.01	0.00	0.001
525	15.71	15.71	0.00	0.02	0.00	1.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
526	15.71	15.71	0.32	0.03	0.00	1.	0.00	0.01	0.001	0.00	0.02	0.00	0.001
527	15.71	15.71	2.45	0.04	0.00	2.	0.00	0.01	0.001	0.00	0.02	0.00	0.001
528	15.71	15.71	0.00	0.08	0.00	3.	0.00	0.02	0.002	0.00	0.03	0.00	0.002
529	15.71	15.71	0.00	0.08	0.00	2.	0.00	0.02	0.002	0.00	0.03	0.00	0.002
530	15.71	15.71	0.00	0.09	0.00	3.	0.00	0.03	0.002	0.00	0.03	0.00	0.002
531	15.71	15.71	0.00	0.11	0.00	4.	0.00	0.02	0.001	0.00	0.03	0.00	0.002
532	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
533	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
534	15.71	15.71	4.09	0.01	0.02	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
535	15.71	15.71	4.26	0.01	0.02	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
536	15.71	15.71	4.01	0.02	0.02	3.	0.00	0.01	0.000	0.00	0.01	0.00	0.000
537	15.71	15.71	3.77	0.01	0.02	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
538	15.71	15.71	4.39	0.00	0.03	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
539	15.71	15.71	4.39	0.00	0.03	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
540	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
541	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
542	15.71	15.71	0.00	0.02	0.00	1.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
543	15.71	15.71	1.82	0.03	0.00	2.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
544	15.71	15.71	3.91	0.04	0.02	3.	0.00	0.01	0.001	0.00	0.02	0.00	0.001
545	15.71	15.71	5.84	0.05	0.03	4.	0.00	0.01	0.001	0.00	0.02	0.00	0.001
546	15.71	15.71	4.39	0.00	0.03	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
547	15.71	15.71	4.39	0.00	0.03	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
548	15.71	15.71	4.98	0.00	0.03	2.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
549	15.71	15.71	5.75	0.01	0.03	3.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
550	15.71	15.71	6.30	0.01	0.04	3.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
551	15.71	15.71	6.69	0.01	0.04	3.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
552	15.71	15.71	6.03	0.16	0.00	8.	0.00	0.04	0.003	0.00	0.05	0.00	0.003
553	15.71	15.71	7.02	0.13	0.00	7.	0.00	0.03	0.002	0.00	0.04	0.00	0.003
554	15.71	15.71	5.28	0.08	0.01	5.	0.00	0.01	0.001	0.00	0.03	0.00	0.002

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
555	15.71	15.71	5.33	0.08	0.01	5.	0.00	0.01	0.001	0.00	0.02	0.00	0.002
556	15.71	15.71	4.51	-0.02	0.03	2.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
557	15.71	15.71	4.51	-0.02	0.03	2.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
558	15.71	15.71	19.74	0.03	0.11	10.	5.33	0.01	0.003	5.48	0.01	0.03	0.003
559	15.71	15.71	18.32	-0.01	0.11	8.	4.80	0.00	0.002	4.89	0.00	0.03	0.003
560	15.71	15.71	16.33	-0.02	0.10	7.	4.42	-0.01	0.002	4.42	-0.01	0.03	0.002
561	15.71	15.71	17.29	-0.02	0.10	8.	4.51	0.00	0.002	4.22	0.00	0.02	0.002
562	15.71	15.71	19.04	-0.02	0.11	8.	3.10	-0.01	0.001	2.63	0.00	0.02	0.001
563	15.71	15.71	19.04	-0.02	0.11	8.	3.10	-0.01	0.001	2.63	0.00	0.02	0.001
564	15.71	15.71	23.87	-0.03	0.14	10.	8.97	-0.01	0.005	8.94	-0.01	0.05	0.004
565	15.71	15.71	22.63	-0.04	0.13	9.	9.03	-0.02	0.004	8.91	0.00	0.05	0.005
566	15.71	15.71	22.37	-0.07	0.13	8.	9.07	-0.01	0.005	8.89	-0.02	0.05	0.004
567	15.71	15.71	23.97	-0.03	0.14	10.	8.15	-0.01	0.004	7.99	-0.02	0.05	0.004
568	15.71	15.71	25.63	-0.02	0.15	12.	5.70	0.00	0.003	5.63	0.00	0.03	0.003
569	15.71	15.71	25.63	-0.02	0.15	12.	5.70	0.00	0.003	5.63	0.00	0.03	0.003
570	15.71	15.71	23.98	-0.03	0.14	10.	9.06	-0.01	0.005	8.94	-0.01	0.05	0.004
571	15.71	15.71	23.48	0.00	0.14	11.	9.09	-0.01	0.005	8.91	0.00	0.05	0.005
572	15.71	15.71	23.29	-0.04	0.14	10.	9.09	-0.02	0.004	8.89	-0.02	0.05	0.004
573	15.71	15.71	23.31	-0.04	0.14	10.	8.09	-0.01	0.004	7.98	-0.02	0.05	0.004
574	15.71	15.71	23.77	-0.02	0.14	11.	5.54	0.00	0.003	5.63	0.00	0.03	0.003
575	15.71	15.71	23.77	-0.02	0.14	11.	5.54	0.00	0.003	5.63	0.00	0.03	0.003
576	15.71	15.71	19.57	0.02	0.11	10.	5.65	0.01	0.003	5.49	0.01	0.03	0.003
577	15.71	15.71	19.00	-0.01	0.11	9.	5.05	0.00	0.003	4.89	0.00	0.03	0.003
578	15.71	15.71	18.06	-0.04	0.11	7.	4.54	0.00	0.002	4.42	-0.01	0.03	0.002
579	15.71	15.71	16.02	-0.01	0.09	7.	4.23	-0.01	0.002	4.21	0.00	0.02	0.002
580	15.71	15.71	15.19	-0.02	0.09	7.	2.41	0.00	0.001	2.62	0.00	0.02	0.001
581	15.71	15.71	15.19	-0.02	0.09	7.	2.41	0.00	0.001	2.62	0.00	0.02	0.001
582	15.71	15.71	6.20	0.14	0.00	7.	0.00	0.04	0.003	0.00	0.05	0.00	0.003
583	15.71	15.71	5.88	0.10	0.00	6.	0.00	0.03	0.002	0.00	0.04	0.00	0.003
584	15.71	15.71	5.11	0.06	0.02	4.	0.00	0.03	0.002	0.00	0.03	0.00	0.002
585	15.71	15.71	2.53	0.02	0.01	2.	0.00	0.02	0.002	0.00	0.02	0.00	0.002
586	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
587	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
588	15.71	15.71	4.51	-0.02	0.03	2.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
589	15.71	15.71	4.51	-0.02	0.03	2.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
590	15.71	15.71	6.79	0.00	0.04	3.	0.00	0.00	0.000	0.00	0.01	0.00	0.001
591	15.71	15.71	10.04	0.01	0.06	5.	0.00	-0.01	0.000	0.00	0.01	0.00	0.001
592	15.71	15.71	13.59	0.02	0.08	7.	0.00	-0.01	0.000	0.00	0.01	0.00	0.001
593	15.71	15.71	17.48	0.05	0.10	10.	0.00	0.00	0.000	0.00	0.02	0.00	0.002
594	15.71	15.71	19.04	-0.02	0.11	8.	3.10	-0.01	0.001	2.63	0.00	0.02	0.001
595	15.71	15.71	19.04	-0.02	0.11	8.	3.10	-0.01	0.001	2.63	0.00	0.02	0.001
596	15.71	15.71	19.86	-0.03	0.12	8.	2.52	-0.02	0.001	2.04	0.00	0.01	0.001
597	15.71	15.71	21.23	-0.03	0.12	9.	1.63	-0.01	0.001	1.11	-0.01	0.01	0.000
598	15.71	15.71	22.83	-0.03	0.13	10.	0.67	0.00	0.000	0.10	-0.01	0.00	0.000
599	15.71	15.71	24.86	-0.02	0.14	11.	0.00	-0.02	0.000	0.00	0.00	0.00	0.000
600	15.71	15.71	25.63	-0.02	0.15	12.	5.70	0.00	0.003	5.63	0.00	0.03	0.003
601	15.71	15.71	25.63	-0.02	0.15	12.	5.70	0.00	0.003	5.63	0.00	0.03	0.003
602	15.71	15.71	25.58	-0.04	0.15	11.	4.95	0.00	0.003	4.91	-0.01	0.03	0.002
603	15.71	15.71	25.68	-0.06	0.15	10.	3.84	-0.01	0.002	3.83	-0.01	0.02	0.002
604	15.71	15.71	25.94	-0.07	0.15	10.	2.78	-0.02	0.001	2.75	-0.01	0.02	0.001
605	15.71	15.71	26.51	-0.07	0.16	10.	1.82	-0.02	0.000	1.75	0.00	0.01	0.001
606	15.71	15.71	23.77	-0.02	0.14	11.	5.54	0.00	0.003	5.63	0.00	0.03	0.003
607	15.71	15.71	23.77	-0.02	0.14	11.	5.54	0.00	0.003	5.63	0.00	0.03	0.003
608	15.71	15.71	23.32	0.00	0.13	11.	4.79	0.00	0.003	4.91	-0.01	0.03	0.002
609	15.71	15.71	22.96	-0.03	0.13	10.	3.67	0.00	0.002	3.83	-0.01	0.02	0.002
610	15.71	15.71	22.87	-0.04	0.13	9.	2.57	-0.02	0.001	2.75	-0.01	0.02	0.001
611	15.71	15.71	23.02	-0.06	0.14	9.	1.58	-0.02	0.000	1.75	0.00	0.01	0.001
612	15.71	15.71	15.19	-0.02	0.09	7.	2.41	0.00	0.001	2.62	0.00	0.02	0.001
613	15.71	15.71	15.19	-0.02	0.09	7.	2.41	0.00	0.001	2.62	0.00	0.02	0.001
614	15.71	15.71	15.71	-0.03	0.09	6.	1.78	-0.01	0.001	2.03	0.00	0.01	0.001
615	15.71	15.71	16.57	-0.03	0.10	7.	0.81	-0.01	0.000	1.10	-0.01	0.01	0.000
616	15.71	15.71	17.55	-0.03	0.10	7.	0.00	-0.01	0.000	0.09	-0.01	0.00	0.000
617	15.71	15.71	18.87	-0.05	0.11	7.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
618	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
619	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
620	15.71	15.71	1.18	0.00	0.01	0.	0.00	0.00	0.000	0.00	0.01	0.00	0.001
621	15.71	15.71	3.69	0.00	0.02	2.	0.00	0.00	0.000	0.00	0.01	0.00	0.001
622	15.71	15.71	6.36	0.00	0.04	3.	0.00	0.00	0.000	0.00	0.01	0.00	0.001
623	15.71	15.71	9.21	0.01	0.05	5.	0.00	0.01	0.001	0.00	0.02	0.00	0.002

ARMATURA SUPERIORE ORIZZONTALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
504	15.71	15.71	0.00	-0.08	0.01	0.	0.00	-0.03	0.000	0.00	-0.03	0.00	0.000
505	15.71	15.71	0.00	-0.24	0.02	0.	0.00	-0.11	0.000	0.00	-0.11	0.01	0.000
506	15.71	15.71	0.00	-0.47	0.03	0.	5.62	-0.19	0.000	3.72	-0.20	0.00	0.000
507	15.71	15.71	0.00	-0.73	0.05	-1.	17.76	-0.28	0.002	14.02	-0.30	0.06	0.000
508	15.71	15.71	0.00	-0.99	0.06	-1.	37.99	-0.37	0.009	31.65	-0.39	0.17	0.005
509	15.71	15.71	0.00	-1.27	0.08	-1.	66.45	-0.42	0.022	57.10	-0.46	0.33	0.016
510	15.71	15.71	0.00	-0.10	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
511	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
512	15.71	15.71	0.00	-0.51	0.03	0.	5.46	-0.20	0.000	3.59	-0.22	0.01	0.000
513	15.71	15.71	0.00	-0.77	0.05	-1.	17.50	-0.30	0.001	13.81	-0.32	0.06	0.000
514	15.71	15.71	0.00	-1.03	0.07	-1.	37.65	-0.38	0.008	31.35	-0.40	0.16	0.005
515	15.71	15.71	0.00	-1.30	0.08	-1.	66.11	-0.43	0.021	56.79	-0.47	0.32	0.015
516	15.71	15.71	0.00	-1.53	0.10	-1.	98.21	-0.47	0.037	86.47	-0.51	0.50	0.029

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
517	15.71	15.71	0.00	-1.51	0.10	-1.	130.19	-0.47	0.054	116.66	-0.51	0.69	0.046
518	15.71	15.71	0.00	-1.52	0.10	-1.	161.83	-0.46	0.072	145.91	-0.51	0.86	0.061
519	15.71	15.71	0.00	-1.54	0.10	-1.	193.86	-0.45	0.089	175.93	-0.51	1.04	0.077
520	15.71	15.71	0.00	-1.00	0.06	-1.	165.48	-0.27	0.080	153.01	-0.34	0.90	0.071
521	15.71	15.71	0.00	-0.67	0.04	-1.	145.97	-0.22	0.071	138.12	-0.27	0.81	0.065
522	15.71	15.71	0.00	-1.55	0.10	-2.	98.01	-0.47	0.037	86.31	-0.52	0.50	0.029
523	15.71	15.71	0.00	-1.54	0.10	-1.	130.36	-0.47	0.054	116.84	-0.52	0.69	0.045
524	15.71	15.71	0.00	-1.54	0.10	-1.	161.92	-0.47	0.071	146.39	-0.52	0.86	0.061
525	15.71	15.71	0.00	-1.56	0.10	-2.	193.82	-0.46	0.089	176.29	-0.52	1.04	0.077
526	15.71	15.71	0.00	-1.03	0.07	-1.	167.64	-0.30	0.080	155.06	-0.37	0.91	0.071
527	15.71	15.71	0.00	-0.59	0.04	-1.	140.08	-0.22	0.068	130.63	-0.27	0.77	0.061
528	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
529	15.71	15.71	0.00	-0.27	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
530	15.71	15.71	0.00	-0.50	0.03	0.	5.46	-0.20	0.000	3.60	-0.22	0.00	0.000
531	15.71	15.71	0.00	-0.77	0.05	-1.	17.51	-0.30	0.001	13.82	-0.32	0.06	0.000
532	15.71	15.71	0.00	-1.04	0.07	-1.	37.67	-0.38	0.008	31.37	-0.40	0.16	0.005
533	15.71	15.71	0.00	-1.31	0.08	-1.	66.14	-0.43	0.021	56.82	-0.47	0.32	0.015
534	15.71	15.71	0.00	-0.08	0.00	0.	0.00	-0.03	0.000	0.00	-0.03	0.00	0.000
535	15.71	15.71	0.00	-0.24	0.02	0.	0.00	-0.11	0.000	0.00	-0.10	0.01	0.000
536	15.71	15.71	0.00	-0.47	0.03	0.	5.62	-0.19	0.000	3.73	-0.20	0.00	0.000
537	15.71	15.71	0.00	-0.73	0.05	-1.	17.78	-0.28	0.002	14.06	-0.30	0.06	0.001
538	15.71	15.71	0.00	-1.00	0.06	-1.	38.06	-0.37	0.009	31.74	-0.39	0.17	0.005
539	15.71	15.71	0.00	-1.29	0.08	-1.	66.53	-0.42	0.022	57.22	-0.46	0.33	0.016
540	15.71	15.71	0.00	-1.56	0.10	-2.	98.05	-0.47	0.037	86.34	-0.52	0.50	0.029
541	15.71	15.71	0.00	-1.55	0.10	-2.	130.40	-0.47	0.054	116.88	-0.52	0.69	0.045
542	15.71	15.71	0.00	-1.55	0.10	-2.	161.76	-0.46	0.071	146.39	-0.52	0.86	0.061
543	15.71	15.71	0.00	-1.57	0.10	-2.	193.78	-0.46	0.089	176.37	-0.52	1.04	0.077
544	15.71	15.71	0.00	-1.02	0.07	-1.	168.25	-0.31	0.080	155.77	-0.37	0.92	0.072
545	15.71	15.71	0.00	-0.58	0.04	-1.	141.69	-0.22	0.069	131.75	-0.27	0.77	0.062
546	15.71	15.71	0.00	-1.56	0.10	-2.	98.28	-0.47	0.037	86.59	-0.51	0.51	0.030
547	15.71	15.71	0.00	-1.53	0.10	-1.	130.15	-0.46	0.054	116.75	-0.51	0.69	0.046
548	15.71	15.71	0.00	-1.51	0.10	-1.	160.20	-0.46	0.071	145.67	-0.51	0.86	0.061
549	15.71	15.71	0.00	-1.54	0.10	-1.	192.54	-0.45	0.089	175.45	-0.51	1.03	0.077
550	15.71	15.71	0.00	-0.96	0.06	-1.	167.07	-0.32	0.079	154.94	-0.34	0.91	0.072
551	15.71	15.71	0.00	-0.60	0.04	-1.	153.89	-0.25	0.075	142.97	-0.27	0.84	0.068
552	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
553	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
554	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
555	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
556	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
557	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
558	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
559	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
560	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
561	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
562	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
563	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
564	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
565	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
566	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
567	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
568	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
569	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
570	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
571	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
572	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
573	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
574	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
575	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
576	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
577	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
578	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
579	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
580	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
581	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
582	15.71	15.71	0.00	-0.09	0.01	0.	0.00	-0.04	0.000	0.00	-0.04	0.00	0.000
583	15.71	15.71	0.00	-0.28	0.02	0.	0.00	-0.12	0.000	0.00	-0.12	0.01	0.000
584	15.71	15.71	0.00	-0.51	0.03	0.	5.37	-0.20	0.000	3.52	-0.22	0.01	0.000
585	15.71	15.71	0.00	-0.78	0.05	-1.	17.40	-0.30	0.001	13.72	-0.32	0.06	0.000
586	15.71	15.71	0.00	-1.04	0.07	-1.	37.57	-0.38	0.008	31.27	-0.41	0.16	0.005
587	15.71	15.71	0.00	-1.31	0.08	-1.	66.07	-0.43	0.021	56.76	-0.47	0.32	0.015
588	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
589	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
590	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
591	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077
592	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
593	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060
594	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
595	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
596	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
597	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077
598	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
599	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060
600	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
601	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
602	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
603	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077

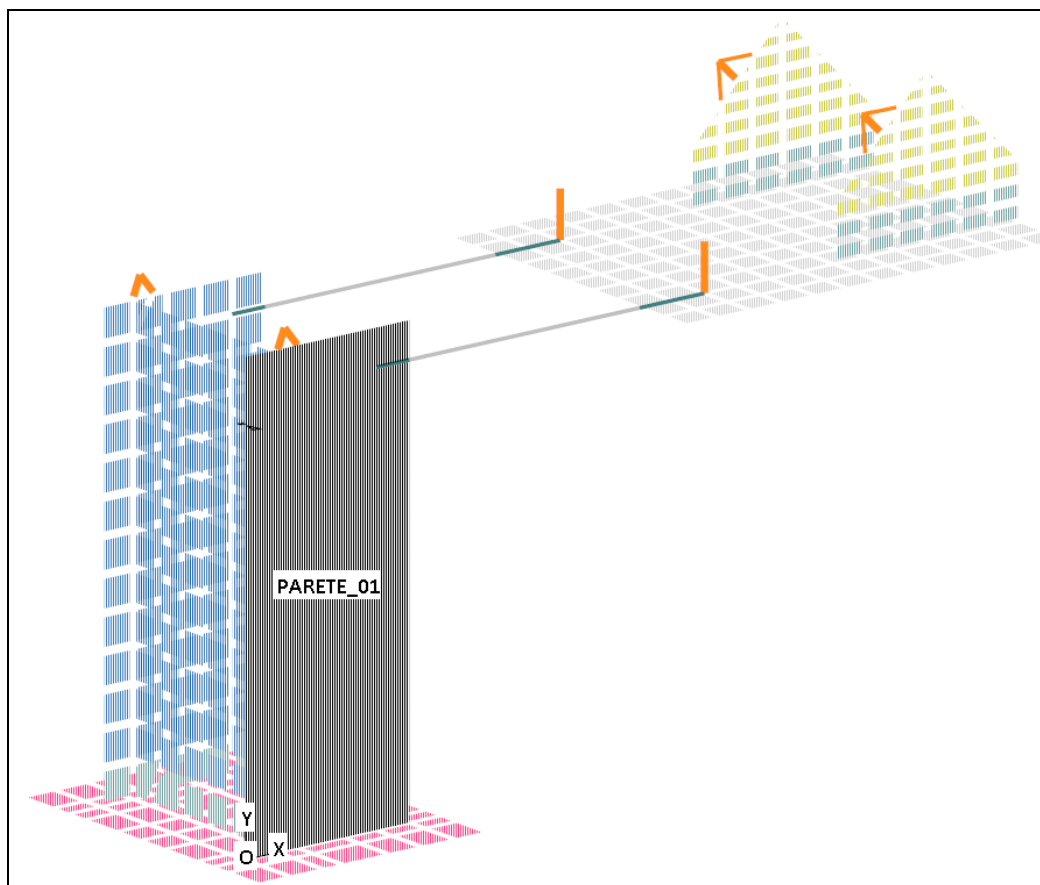
GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
604	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
605	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060
606	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
607	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
608	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
609	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077
610	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
611	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060
612	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
613	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
614	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
615	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077
616	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
617	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060
618	15.71	15.71	0.00	-1.55	0.10	-2.	98.06	-0.47	0.037	86.35	-0.52	0.50	0.029
619	15.71	15.71	0.00	-1.55	0.10	-2.	130.57	-0.47	0.054	117.03	-0.52	0.69	0.045
620	15.71	15.71	0.00	-1.55	0.10	-2.	162.19	-0.47	0.072	146.69	-0.52	0.86	0.061
621	15.71	15.71	0.00	-1.55	0.10	-2.	193.71	-0.46	0.089	176.31	-0.52	1.04	0.077
622	15.71	15.71	0.00	-1.00	0.06	-1.	167.98	-0.30	0.080	155.45	-0.36	0.91	0.071
623	15.71	15.71	0.00	-0.57	0.04	-1.	138.36	-0.21	0.067	128.84	-0.26	0.76	0.060

ARMATURA SUPERIORE VERTICALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
504	15.71	15.71	0.00	0.02	0.00	0.	6.23	0.00	0.003	5.85	0.00	0.03	0.003
505	15.71	15.71	0.00	0.01	0.00	0.	6.22	0.00	0.003	5.90	0.00	0.03	0.003
506	15.71	15.71	0.00	0.01	0.00	0.	6.51	0.01	0.004	6.14	0.01	0.04	0.004
507	15.71	15.71	0.00	0.00	0.00	0.	6.99	0.00	0.004	6.56	0.00	0.04	0.004
508	15.71	15.71	0.00	0.00	0.00	0.	10.03	0.00	0.005	9.35	0.00	0.05	0.005
509	15.71	15.71	0.00	0.00	0.00	0.	10.03	0.00	0.005	9.35	0.00	0.05	0.005
510	15.71	15.71	2.17	0.10	0.00	4.	6.36	0.02	0.004	5.80	0.03	0.03	0.004
511	15.71	15.71	0.06	0.10	0.00	3.	8.58	0.02	0.006	7.82	0.03	0.04	0.005
512	15.71	15.71	0.41	0.08	0.00	3.	12.45	0.03	0.008	11.18	0.03	0.06	0.007
513	15.71	15.71	3.29	0.05	0.01	3.	15.53	0.02	0.009	14.03	0.03	0.08	0.009
514	15.71	15.71	5.96	0.00	0.03	3.	22.21	0.00	0.012	20.27	0.00	0.12	0.011
515	15.71	15.71	5.96	0.00	0.03	3.	22.21	0.00	0.012	20.27	0.00	0.12	0.011
516	15.71	15.71	0.00	0.00	0.00	0.	10.03	0.00	0.005	9.35	0.00	0.05	0.005
517	15.71	15.71	0.00	0.00	0.00	0.	10.03	0.00	0.005	9.35	0.00	0.05	0.005
518	15.71	15.71	0.00	0.00	0.00	0.	10.55	0.00	0.006	9.82	0.00	0.06	0.005
519	15.71	15.71	0.00	0.01	0.00	0.	11.35	0.00	0.006	10.55	0.00	0.06	0.006
520	15.71	15.71	0.00	0.01	0.00	0.	12.20	0.00	0.007	11.33	0.00	0.07	0.006
521	15.71	15.71	0.00	0.01	0.00	0.	13.07	0.00	0.007	12.14	0.00	0.07	0.007
522	15.71	15.71	5.96	0.00	0.03	3.	22.21	0.00	0.012	20.27	0.00	0.12	0.011
523	15.71	15.71	5.96	0.00	0.03	3.	22.21	0.00	0.012	20.27	0.00	0.12	0.011
524	15.71	15.71	4.57	0.01	0.03	2.	23.04	0.01	0.013	21.01	0.01	0.12	0.012
525	15.71	15.71	2.59	0.02	0.01	2.	24.83	0.01	0.014	22.65	0.01	0.13	0.013
526	15.71	15.71	0.62	0.03	0.00	1.	27.30	0.01	0.015	24.83	0.02	0.14	0.014
527	15.71	15.71	0.00	0.04	0.00	1.	30.46	0.01	0.017	27.64	0.02	0.16	0.016
528	15.71	15.71	5.45	0.08	0.01	5.	6.50	0.02	0.005	5.80	0.03	0.03	0.004
529	15.71	15.71	4.50	0.08	0.00	5.	8.78	0.02	0.006	7.82	0.03	0.04	0.005
530	15.71	15.71	4.37	0.09	0.00	5.	12.62	0.03	0.008	11.17	0.03	0.06	0.007
531	15.71	15.71	5.02	0.11	0.00	6.	15.62	0.02	0.009	14.02	0.03	0.08	0.009
532	15.71	15.71	7.30	0.00	0.04	3.	22.20	0.00	0.012	20.25	0.00	0.12	0.011
533	15.71	15.71	7.30	0.00	0.04	3.	22.20	0.00	0.012	20.25	0.00	0.12	0.011
534	15.71	15.71	0.00	0.01	0.00	0.	6.54	0.00	0.004	5.85	0.00	0.03	0.003
535	15.71	15.71	0.00	0.01	0.00	0.	6.62	0.00	0.004	5.89	0.00	0.03	0.003
536	15.71	15.71	0.00	0.02	0.00	1.	6.91	0.01	0.004	6.13	0.01	0.03	0.004
537	15.71	15.71	0.00	0.01	0.00	0.	7.40	0.00	0.004	6.56	0.00	0.04	0.004
538	15.71	15.71	0.00	0.00	0.00	0.	10.34	0.00	0.006	9.34	0.00	0.05	0.005
539	15.71	15.71	0.00	0.00	0.00	0.	10.34	0.00	0.006	9.34	0.00	0.05	0.005
540	15.71	15.71	7.30	0.00	0.04	3.	22.20	0.00	0.012	20.25	0.00	0.12	0.011
541	15.71	15.71	7.30	0.00	0.04	3.	22.20	0.00	0.012	20.25	0.00	0.12	0.011
542	15.71	15.71	5.99	0.02	0.03	3.	23.01	0.01	0.013	20.99	0.01	0.12	0.012
543	15.71	15.71	4.08	0.03	0.02	3.	24.80	0.01	0.014	22.63	0.01	0.13	0.013
544	15.71	15.71	2.13	0.04	0.00	2.	27.26	0.01	0.015	24.81	0.02	0.14	0.014
545	15.71	15.71	0.42	0.05	0.00	2.	30.41	0.01	0.017	27.62	0.02	0.16	0.016
546	15.71	15.71	0.00	0.00	0.00	0.	10.34	0.00	0.006	9.34	0.00	0.05	0.005
547	15.71	15.71	0.00	0.00	0.00	0.	10.34	0.00	0.006	9.34	0.00	0.05	0.005
548	15.71	15.71	0.00	0.00	0.00	0.	10.88	0.00	0.006	9.81	0.00	0.06	0.005
549	15.71	15.71	0.00	0.01	0.00	0.	11.71	0.00	0.006	10.54	0.00	0.06	0.006
550	15.71	15.71	0.00	0.01	0.00	0.	12.59	0.00	0.007	11.32	0.00	0.07	0.006
551	15.71	15.71	0.00	0.01	0.00	0.	13.50	0.00	0.007	12.13	0.00	0.07	0.007
552	15.71	15.71	0.00	0.16	0.00	5.	2.94	0.04	0.003	2.43	0.05	0.00	0.004
553	15.71	15.71	0.00	0.13	0.00	4.	6.57	0.03	0.005	5.87	0.04	0.03	0.005
554	15.71	15.71	0.00	0.08	0.00	3.	7.57	0.01	0.005	7.25	0.03	0.04	0.005
555	15.71	15.71	0.00	0.08	0.00	3.	11.47	0.01	0.007	10.70	0.02	0.06	0.007
556	15.71	15.71	0.00	-0.02	0.00	0.	20.23	-0.01	0.011	19.01	0.00	0.11	0.010
557	15.71	15.71	0.00	-0.02	0.00	0.	20.23	-0.01	0.011	19.01	0.00	0.11	0.010
558	15.71	15.71	0.00	0.03	0.00	1.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
559	15.71	15.71	0.00	-0.01	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
560	15.71	15.71	0.00	-0.02	0.00	0.	0.00	-0.01	0.000	0.00	-0.01	0.00	0.000
561	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
562	15.71	15.71	0.00	-0.02	0.00	0.	4.64	-0.01	0.002	3.80	0.00	0.02	0.002
563	15.71	15.71	0.00	-0.02	0.00	0.	4.64	-0.01	0.002	3.80	0.00	0.02	0.002
564	15.71	15.71	0.00	-0.03	0.00	0.	0.00	-0.01	0.000	0.00	-0.01	0.00	0.000
565	15.71	15.71	0.00	-0.04	0.00	0.	0.00	-0.02	0.000	0.00	0.00	0.00	0.000

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
566	15.71	15.71	0.00	-0.07	0.00	0.	0.00	-0.01	0.000	0.00	-0.02	0.00	0.000
567	15.71	15.71	0.00	-0.03	0.00	0.	0.00	-0.01	0.000	0.00	-0.02	0.00	0.000
568	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
569	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
570	15.71	15.71	0.00	-0.03	0.00	0.	0.00	-0.01	0.000	0.00	-0.01	0.00	0.000
571	15.71	15.71	0.00	0.00	0.00	0.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
572	15.71	15.71	0.00	-0.04	0.00	0.	0.00	-0.02	0.000	0.00	-0.02	0.00	0.000
573	15.71	15.71	0.00	-0.04	0.00	0.	0.00	-0.01	0.000	0.00	-0.02	0.00	0.000
574	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
575	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
576	15.71	15.71	0.00	0.02	0.00	1.	0.00	0.01	0.001	0.00	0.01	0.00	0.001
577	15.71	15.71	0.00	-0.01	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
578	15.71	15.71	0.00	-0.04	0.00	0.	0.00	0.00	0.000	0.00	-0.01	0.00	0.000
579	15.71	15.71	0.00	-0.01	0.00	0.	0.00	-0.01	0.000	0.00	0.00	0.00	0.000
580	15.71	15.71	0.00	-0.02	0.00	0.	3.41	0.00	0.002	3.81	0.00	0.02	0.002
581	15.71	15.71	0.00	-0.02	0.00	0.	3.41	0.00	0.002	3.81	0.00	0.02	0.002
582	15.71	15.71	0.00	0.14	0.00	4.	2.87	0.04	0.004	2.42	0.05	0.00	0.004
583	15.71	15.71	0.00	0.10	0.00	3.	6.65	0.03	0.005	5.85	0.04	0.03	0.005
584	15.71	15.71	0.00	0.06	0.00	2.	7.96	0.03	0.005	7.24	0.03	0.04	0.005
585	15.71	15.71	0.00	0.02	0.00	1.	10.92	0.02	0.007	10.70	0.02	0.06	0.007
586	15.71	15.71	2.40	-0.02	0.01	1.	19.55	0.00	0.010	19.01	0.00	0.11	0.010
587	15.71	15.71	2.40	-0.02	0.01	1.	19.55	0.00	0.010	19.01	0.00	0.11	0.010
588	15.71	15.71	0.00	-0.02	0.00	0.	20.23	-0.01	0.011	19.01	0.00	0.11	0.010
589	15.71	15.71	0.00	-0.02	0.00	0.	20.23	-0.01	0.011	19.01	0.00	0.11	0.010
590	15.71	15.71	0.00	0.00	0.00	0.	21.15	0.00	0.011	19.86	0.01	0.11	0.011
591	15.71	15.71	0.00	0.01	0.00	0.	23.29	-0.01	0.012	21.75	0.01	0.12	0.012
592	15.71	15.71	0.00	0.02	0.00	1.	26.21	-0.01	0.014	24.37	0.01	0.14	0.014
593	15.71	15.71	0.00	0.05	0.00	2.	30.10	0.00	0.016	27.89	0.02	0.16	0.016
594	15.71	15.71	0.00	-0.02	0.00	0.	4.64	-0.01	0.002	3.80	0.00	0.02	0.002
595	15.71	15.71	0.00	-0.02	0.00	0.	4.64	-0.01	0.002	3.80	0.00	0.02	0.002
596	15.71	15.71	0.00	-0.03	0.00	0.	5.50	-0.02	0.002	4.59	0.00	0.03	0.002
597	15.71	15.71	0.00	-0.03	0.00	0.	6.94	-0.01	0.003	5.94	-0.01	0.03	0.003
598	15.71	15.71	0.00	-0.03	0.00	0.	8.67	0.00	0.005	7.53	-0.01	0.04	0.004
599	15.71	15.71	0.00	-0.02	0.00	0.	10.71	-0.02	0.005	9.39	0.00	0.05	0.005
600	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
601	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
602	15.71	15.71	0.00	-0.04	0.00	0.	0.00	0.00	0.000	0.00	-0.01	0.00	0.000
603	15.71	15.71	0.00	-0.06	0.00	0.	0.00	-0.01	0.000	0.00	-0.01	0.00	0.000
604	15.71	15.71	0.00	-0.07	0.00	0.	0.87	-0.02	0.000	0.00	-0.01	0.00	0.000
605	15.71	15.71	0.00	-0.07	0.00	0.	2.23	-0.02	0.000	0.89	0.00	0.01	0.000
606	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
607	15.71	15.71	0.00	-0.02	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
608	15.71	15.71	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	-0.01	0.00	0.000
609	15.71	15.71	0.00	-0.03	0.00	0.	0.00	0.00	0.000	0.00	-0.01	0.00	0.000
610	15.71	15.71	0.00	-0.04	0.00	0.	0.00	-0.02	0.000	0.00	-0.01	0.00	0.000
611	15.71	15.71	0.00	-0.06	0.00	0.	0.04	-0.02	0.000	0.89	0.00	0.01	0.000
612	15.71	15.71	0.00	-0.02	0.00	0.	3.41	0.00	0.002	3.81	0.00	0.02	0.002
613	15.71	15.71	0.00	-0.02	0.00	0.	3.41	0.00	0.002	3.81	0.00	0.02	0.002
614	15.71	15.71	0.00	-0.03	0.00	0.	4.22	-0.01	0.002	4.60	0.00	0.03	0.002
615	15.71	15.71	0.00	-0.03	0.00	0.	5.56	-0.01	0.003	5.95	-0.01	0.03	0.003
616	15.71	15.71	0.00	-0.03	0.00	0.	7.19	-0.01	0.004	7.54	-0.01	0.04	0.004
617	15.71	15.71	0.00	-0.05	0.00	0.	9.08	0.00	0.005	9.41	0.00	0.05	0.005
618	15.71	15.71	2.40	-0.02	0.01	1.	19.55	0.00	0.010	19.01	0.00	0.11	0.010
619	15.71	15.71	2.40	-0.02	0.01	1.	19.55	0.00	0.010	19.01	0.00	0.11	0.010
620	15.71	15.71	1.21	0.00	0.01	0.	20.43	0.00	0.011	19.86	0.01	0.11	0.011
621	15.71	15.71	0.00	0.00	0.00	0.	22.54	0.00	0.012	21.76	0.01	0.13	0.012
622	15.71	15.71	0.00	0.00	0.00	0.	25.44	0.00	0.014	24.38	0.01	0.14	0.014
623	15.71	15.71	0.00	0.01	0.00	0.	29.27	0.01	0.016	27.89	0.02	0.16	0.016

6.3. PARETE 01



G355	G759	G356	G355	G354
G217	G172	G171	G170	G169
G218	G176	G175	G174	G173
G219	G180	G179	G178	G177
G220	G184	G183	G182	G181
G221	G188	G187	G186	G185
G222	G192	G191	G190	G189
G223	G196	G195	G194	G193
G224	G200	G199	G198	G197
G225	G204	G203	G202	G201
G226	G208	G207	G206	G205
G227	G212	G211	G210	G209
G228	G216	G215	G214	G213

6.3.1. Verifica SLU

		INFERIORE ORIZZONTALE						INFERIORE VERTICALE							
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
229	0.6	16.38	16.38	2.	8.	0.00	1.23	16.34	16.34	4.	-2.	0.02	-0.01		
230	0.6	16.38	16.38	7.	-2.	0.03	0.04	16.34	16.34	6.	-2.	0.03	0.02		
231	0.6	16.38	16.38	3.	0.	0.01	0.07	16.34	16.34	7.	-2.	0.03	0.02		
232	0.6	10.21	10.21	1.	1.	0.00	0.28	16.34	16.34	8.	3.	0.01	0.51		
233	0.6	16.38	16.38	6.	6.	0.00	0.95	16.34	16.34	8.	-2.	0.03	0.03		
234	0.6	16.38	16.38	8.	-1.	0.03	0.04	16.34	16.34	9.	-2.	0.03	0.04		
235	0.6	16.38	16.38	7.	-1.	0.02	0.03	16.34	16.34	10.	-2.	0.03	0.04		

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
236	0.6	10.21	10.21	4.	0.	0.01	0.04	16.34	16.34	10.	-1.	0.02	0.06	
237	0.6	10.21	10.21	8.	5.	0.00	1.16	16.34	16.34	12.	-3.	0.04	0.04	
238	0.6	10.21	10.21	11.	-2.	0.03	0.07	16.34	16.34	12.	-2.	0.04	0.05	
239	0.6	10.21	10.21	9.	-1.	0.03	0.07	16.34	16.34	12.	-2.	0.04	0.05	
240	0.6	10.21	10.21	7.	0.	0.02	0.06	16.34	16.34	11.	-1.	0.03	0.06	
241	0.6	10.21	10.21	15.	1.	0.03	0.28	16.34	16.34	11.	-3.	0.04	0.05	
242	0.6	10.21	10.21	11.	-1.	0.03	0.13	16.34	16.34	14.	-2.	0.04	0.06	
243	0.6	10.21	10.21	10.	0.	0.03	0.12	16.34	16.34	15.	-2.	0.04	0.07	
244	0.6	10.21	10.21	9.	0.	0.02	0.14	16.34	16.34	13.	-1.	0.03	0.07	
245	0.6	10.21	10.21	17.	0.	0.03	0.18	16.34	16.34	16.	-2.	0.04	0.07	
246	0.6	10.21	10.21	16.	1.	0.00	0.32	16.34	16.34	16.	-1.	0.04	0.08	
247	0.6	10.21	10.21	15.	1.	0.00	0.39	16.34	16.34	17.	-1.	0.04	0.08	
248	0.6	10.21	10.21	12.	1.	0.00	0.36	16.34	16.34	17.	-1.	0.04	0.08	
249	0.6	10.21	10.21	18.	0.	0.02	0.22	16.34	16.34	12.	-2.	0.03	0.06	
250	0.6	10.21	10.21	18.	1.	0.00	0.44	16.34	16.34	14.	-1.	0.04	0.07	
251	0.6	10.21	10.21	16.	2.	0.00	0.54	16.34	16.34	15.	-2.	0.04	0.07	
252	0.6	10.21	10.21	14.	1.	0.00	0.48	16.34	16.34	14.	-1.	0.04	0.07	
253	0.6	10.21	10.21	19.	0.	0.00	0.27	16.34	16.34	17.	0.	0.03	0.11	
254	0.6	10.21	10.21	18.	2.	0.00	0.53	16.34	16.34	17.	-1.	0.04	0.10	
255	0.6	10.21	10.21	17.	2.	0.00	0.60	16.34	16.34	18.	-1.	0.04	0.10	
256	0.6	10.21	10.21	14.	2.	0.00	0.50	16.34	16.34	18.	-1.	0.04	0.10	
257	0.6	10.21	10.21	18.	1.	0.00	0.35	16.34	16.34	21.	0.	0.02	0.18	
258	0.6	10.21	10.21	18.	2.	0.00	0.61	16.34	16.34	20.	-1.	0.04	0.12	
259	0.6	10.21	10.21	17.	2.	0.00	0.63	16.34	16.34	20.	-1.	0.04	0.11	
260	0.6	10.21	10.21	13.	1.	0.00	0.46	16.34	16.34	20.	-1.	0.04	0.11	
261	0.6	10.21	10.21	17.	1.	0.00	0.41	16.34	16.34	24.	1.	0.00	0.28	
262	0.6	10.21	10.21	18.	2.	0.00	0.61	16.34	16.34	22.	-1.	0.04	0.16	
263	0.6	10.21	10.21	16.	2.	0.00	0.61	16.34	16.34	22.	-1.	0.04	0.12	
264	0.6	10.21	10.21	11.	1.	0.00	0.36	16.34	16.34	21.	-1.	0.05	0.11	
265	0.6	10.21	10.21	16.	1.	0.00	0.43	16.34	16.34	28.	1.	0.00	0.38	
266	0.6	10.21	10.21	17.	2.	0.00	0.60	16.34	16.34	26.	0.	0.04	0.23	
267	0.6	10.21	10.21	15.	2.	0.00	0.56	16.34	16.34	23.	-1.	0.05	0.13	
268	0.6	10.21	10.21	10.	1.	0.00	0.29	16.34	16.34	23.	-1.	0.05	0.13	
269	0.6	10.21	10.21	15.	1.	0.00	0.44	16.34	16.34	35.	2.	0.00	0.49	
270	0.6	10.21	10.21	17.	2.	0.00	0.59	16.34	16.34	31.	1.	0.05	0.29	
271	0.6	10.21	10.21	15.	2.	0.00	0.52	16.34	16.34	26.	-1.	0.05	0.16	
272	0.6	10.21	10.21	9.	1.	0.00	0.23	16.34	16.34	26.	-2.	0.06	0.15	
273	0.6	10.21	10.21	14.	1.	0.00	0.45	16.34	16.34	43.	2.	0.00	0.54	
274	0.6	10.21	10.21	16.	2.	0.00	0.57	16.34	16.34	38.	1.	0.06	0.31	
275	0.6	10.21	10.21	14.	1.	0.00	0.47	16.34	16.34	31.	-1.	0.06	0.18	
276	0.6	10.21	10.21	6.	0.	0.00	0.13	16.34	16.34	27.	-3.	0.07	0.15	
277	0.6	10.21	10.21	21.	0.	0.04	0.27	16.34	16.34	9.	3.	0.00	0.56	
278	0.6	10.21	10.21	21.	0.	0.04	0.26	16.34	16.34	12.	0.	0.02	0.08	
279	0.6	10.21	10.21	20.	0.	0.04	0.23	16.34	16.34	13.	0.	0.02	0.07	
280	0.6	10.21	10.21	19.	0.	0.04	0.22	16.34	16.34	15.	0.	0.03	0.09	
281	0.6	10.21	10.21	19.	0.	0.04	0.21	16.34	16.34	17.	-1.	0.03	0.09	
282	0.6	10.21	10.21	19.	0.	0.03	0.20	16.34	16.34	16.	-1.	0.04	0.09	
283	0.6	10.21	10.21	18.	0.	0.03	0.19	16.34	16.34	19.	-1.	0.04	0.10	
284	0.6	10.21	10.21	17.	0.	0.04	0.20	16.34	16.34	19.	-2.	0.05	0.10	
285	0.6	10.21	10.21	16.	0.	0.04	0.19	16.34	16.34	20.	-2.	0.05	0.10	
286	0.6	10.21	10.21	16.	0.	0.03	0.18	16.34	16.34	21.	-2.	0.05	0.10	
287	0.6	10.21	10.21	15.	0.	0.03	0.17	16.34	16.34	22.	-3.	0.06	0.11	
288	0.6	10.21	10.21	15.	0.	0.03	0.17	16.34	16.34	21.	-4.	0.07	0.10	
349	0.6	16.38	16.38	0.	11.	0.00	1.56	16.34	16.34	4.	1.	0.01	0.18	
350	0.6	16.38	16.38	5.	-1.	0.02	0.12	16.34	16.34	5.	1.	0.01	0.14	
351	0.6	16.38	16.38	1.	2.	0.00	0.23	16.34	16.34	5.	-1.	0.01	0.10	
352	0.6	10.21	10.21	0.	2.	0.00	0.56	16.34	16.34	8.	1.	0.01	0.23	
353	0.6	10.21	10.21	21.	0.	0.04	0.29	16.34	16.34	8.	3.	0.00	0.46	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
229	0.6	16.38	16.38	10.	8.	0.00	1.28	16.34	16.34	19.	-2.	0.05	0.10	
230	0.6	16.38	16.38	13.	-2.	0.04	0.07	16.34	16.34	18.	-2.	0.05	0.09	
231	0.6	16.38	16.38	12.	0.	0.02	0.12	16.34	16.34	17.	-2.	0.04	0.08	
232	0.6	10.21	10.21	21.	1.	0.00	0.43	16.34	16.34	12.	3.	0.03	0.53	
233	0.6	16.38	16.38	11.	6.	0.00	0.99	16.34	16.34	22.	-2.	0.05	0.11	
234	0.6	16.38	16.38	14.	-1.	0.04	0.07	16.34	16.34	21.	-2.	0.05	0.11	
235	0.6	16.38	16.38	16.	-1.	0.03	0.08	16.34	16.34	20.	-2.	0.05	0.10	
236	0.6	10.21	10.21	19.	0.	0.04	0.21	16.34	16.34	20.	-1.	0.04	0.11	
237	0.6	10.21	10.21	13.	5.	0.00	1.21	16.34	16.34	22.	-3.	0.06	0.10	
238	0.6	10.21	10.21	16.	-2.	0.05	0.11	16.34	16.34	22.	-2.	0.05	0.10	
239	0.6	10.21	10.21	17.	-1.	0.04	0.13	16.34	16.34	21.	-2.	0.05	0.10	
240	0.6	10.21	10.21	22.	0.	0.05	0.20	16.34	16.34	21.	-1.	0.05	0.12	
241	0.6	10.21	10.21	17.	1.	0.04	0.30	16.34	16.34	23.	-3.	0.06	0.10	
242	0.6	10.21	10.21	17.	-1.	0.04	0.17	16.34	16.34	22.	-2.	0.05	0.10	
243	0.6	10.21	10.21	18.	0.	0.04	0.18	16.34	16.34	21.	-2.	0.05	0.10	
244	0.6	10.21	10.21	22.	0.	0.04	0.26	16.34	16.34	22.	-1.	0.05	0.11	
245	0.6	10.21	10.21	18.	0.	0.04	0.19	16.34	16.34	19.	-2.	0.05	0.09	
246	0.6	10.21	10.21	20.	1.	0.01	0.36	16.34	16.34	19.	-1.	0.04	0.09	
247	0.6	10.21	10.21	21.	1.	0.00	0.45	16.34	16.34	17.	-1.	0.04	0.08	
248	0.6	10.21	10.21	24.	1.	0.00	0.47	16.34	16.34	17.	-1.	0.04	0.08	
249	0.6	10.21	10.21	19.	0.	0.02	0.22	16.34	16.34	20.	-1.	0.05	0.10	
250	0.6	10.21	10.21	20.	1.	0.00	0.47	16.34	16.34	20.	-1.	0.05	0.10	
251	0.6	10.21	10.21	23.	2.	0.00	0.61	16.34	16.34	20.	-2.	0.05	0.10	
252	0.6	10.21	10.21	25.	2.	0.00	0.59	16.34	16.34	20.	-1.	0.04	0.10	
253	0.6	10.21	10.21	18.	0.	0.00	0.26	16.34	16.34	19.	0.	0.03	0.11	
254	0.6	10.21	10.21	19.	2.	0.00	0.54	16.34	16.34	18.	-1.	0.04	0.10	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
255	0.6	10.21	10.21	22.	2.	0.00	0.66	16.34	16.34	19.	-1.	0.04	0.10
256	0.6	10.21	10.21	26.	1.	0.00	0.60	16.34	16.34	19.	-1.	0.04	0.10
257	0.6	10.21	10.21	17.	1.	0.00	0.33	16.34	16.34	17.	0.	0.02	0.16
258	0.6	10.21	10.21	18.	2.	0.00	0.59	16.34	16.34	16.	-1.	0.03	0.09
259	0.6	10.21	10.21	22.	2.	0.00	0.66	16.34	16.34	15.	-1.	0.03	0.08
260	0.6	10.21	10.21	26.	1.	0.00	0.58	16.34	16.34	16.	-1.	0.04	0.08
261	0.6	10.21	10.21	14.	1.	0.00	0.38	16.34	16.34	13.	1.	0.00	0.21
262	0.6	10.21	10.21	15.	2.	0.00	0.59	16.34	16.34	14.	-1.	0.03	0.11
263	0.6	10.21	10.21	19.	2.	0.00	0.61	16.34	16.34	16.	-1.	0.03	0.08
264	0.6	10.21	10.21	25.	1.	0.00	0.49	16.34	16.34	16.	-1.	0.04	0.08
265	0.6	10.21	10.21	8.	1.	0.00	0.36	16.34	16.34	2.	1.	0.00	0.23
266	0.6	10.21	10.21	13.	2.	0.00	0.57	16.34	16.34	9.	0.	0.02	0.10
267	0.6	10.21	10.21	16.	2.	0.00	0.55	16.34	16.34	10.	-1.	0.02	0.05
268	0.6	10.21	10.21	24.	1.	0.00	0.40	16.34	16.34	10.	-1.	0.03	0.04
269	0.6	10.21	10.21	5.	1.	0.00	0.34	16.34	16.34	0.	2.	0.00	0.28
270	0.6	10.21	10.21	8.	2.	0.00	0.52	16.34	16.34	0.	1.	0.00	0.11
271	0.6	10.21	10.21	14.	2.	0.00	0.51	16.34	16.34	0.	-1.	0.01	-0.01
272	0.6	10.21	10.21	24.	1.	0.00	0.36	16.34	16.34	2.	-2.	0.02	-0.01
273	0.6	10.21	10.21	1.	1.	0.00	0.33	16.34	16.34	0.	2.	0.00	0.28
274	0.6	10.21	10.21	3.	2.	0.00	0.46	16.34	16.34	0.	-1.	0.01	0.09
275	0.6	10.21	10.21	12.	1.	0.00	0.45	16.34	16.34	0.	-1.	0.01	-0.01
276	0.6	10.21	10.21	24.	0.	0.00	0.30	16.34	16.34	0.	-3.	0.02	-0.02
277	0.6	10.21	10.21	12.	0.	0.03	0.16	16.34	16.34	11.	3.	0.00	0.57
278	0.6	10.21	10.21	13.	0.	0.03	0.17	16.34	16.34	19.	0.	0.03	0.12
279	0.6	10.21	10.21	13.	0.	0.03	0.17	16.34	16.34	21.	0.	0.04	0.12
280	0.6	10.21	10.21	16.	0.	0.04	0.19	16.34	16.34	21.	-1.	0.04	0.12
281	0.6	10.21	10.21	18.	0.	0.04	0.19	16.34	16.34	16.	-1.	0.03	0.10
282	0.6	10.21	10.21	19.	0.	0.03	0.20	16.34	16.34	19.	-1.	0.04	0.10
283	0.6	10.21	10.21	19.	0.	0.03	0.19	16.34	16.34	20.	-1.	0.04	0.10
284	0.6	10.21	10.21	18.	0.	0.04	0.20	16.34	16.34	16.	-2.	0.04	0.08
285	0.6	10.21	10.21	17.	0.	0.04	0.20	16.34	16.34	17.	-2.	0.04	0.07
286	0.6	10.21	10.21	16.	0.	0.03	0.19	16.34	16.34	12.	-2.	0.04	0.04
287	0.6	10.21	10.21	15.	0.	0.03	0.18	16.34	16.34	4.	-3.	0.03	-0.02
288	0.6	10.21	10.21	13.	0.	0.03	0.18	16.34	16.34	0.	-4.	0.03	-0.03
349	0.6	16.38	16.38	7.	11.	0.00	1.60	16.34	16.34	9.	1.	0.02	0.21
350	0.6	16.38	16.38	11.	-1.	0.03	0.17	16.34	16.34	9.	1.	0.02	0.17
351	0.6	16.38	16.38	10.	2.	0.00	0.29	16.34	16.34	8.	-1.	0.02	0.11
352	0.6	10.21	10.21	20.	2.	0.00	0.69	16.34	16.34	9.	1.	0.02	0.24
353	0.6	10.21	10.21	10.	0.	0.02	0.17	16.34	16.34	9.	3.	0.00	0.47

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO (Rd > Ed)

6.3.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σF	Mom	Nor	wkF	Mom	Nor	σC	wkP
229	16.38	16.38	6.73	5.41	0.00	174.	2.76	3.76	0.158	0.07	3.35	0.00	0.141
230	16.38	16.38	3.97	-1.33	0.26	-2.	1.07	0.15	0.006	0.00	0.41	0.00	0.017
231	16.38	16.38	3.90	-0.39	0.12	0.	0.66	0.41	0.017	0.00	0.63	0.00	0.027
232	10.21	10.21	3.73	-0.04	0.13	5.	0.53	0.52	0.064	0.00	0.72	0.00	0.088
233	16.38	16.38	7.54	4.13	0.00	136.	2.89	3.13	0.132	0.05	2.79	0.00	0.117
234	16.38	16.38	5.08	-1.44	0.30	-2.	1.42	-0.02	0.001	0.00	0.21	0.00	0.009
235	16.38	16.38	4.84	-0.72	0.18	-1.	1.00	0.18	0.008	0.00	0.39	0.00	0.017
236	10.21	10.21	4.53	-0.06	0.15	6.	0.82	0.32	0.040	0.00	0.51	0.00	0.063
237	10.21	10.21	8.88	2.18	0.00	126.	3.26	2.08	0.252	0.02	1.76	0.00	0.214
238	10.21	10.21	6.68	-1.93	0.41	-3.	1.97	-0.92	0.000	0.00	-0.70	0.11	0.000
239	10.21	10.21	6.27	-1.19	0.28	-2.	1.53	-0.25	0.000	0.00	-0.05	0.01	0.000
240	10.21	10.21	6.03	-0.24	0.17	2.	1.42	0.16	0.020	0.00	0.39	0.00	0.048
241	10.21	10.21	10.85	-0.20	0.36	12.	3.81	-0.04	0.007	0.00	-0.10	0.02	0.000
242	10.21	10.21	8.86	-0.35	0.26	4.	2.79	-0.58	0.000	0.00	-0.61	0.10	0.000
243	10.21	10.21	8.07	-0.25	0.25	5.	2.21	-0.48	0.000	0.00	-0.49	0.08	0.000
244	10.21	10.21	7.41	-0.10	0.25	10.	1.94	-0.18	0.000	0.00	-0.05	0.01	0.000
245	10.21	10.21	11.75	-0.08	0.40	20.	3.98	-0.07	0.006	0.00	-0.10	0.02	0.000
246	10.21	10.21	10.27	0.28	0.28	35.	3.09	0.01	0.009	0.00	-0.18	0.03	0.000
247	10.21	10.21	9.27	0.35	0.21	36.	2.68	-0.02	0.006	0.00	-0.14	0.02	0.000
248	10.21	10.21	7.98	0.44	0.04	38.	2.21	-0.04	0.003	0.00	-0.04	0.01	0.000
249	10.21	10.21	12.17	0.08	0.41	28.	4.01	0.00	0.010	0.00	-0.03	0.00	0.000
250	10.21	10.21	11.27	0.70	0.00	58.	3.52	0.16	0.025	0.00	0.00	0.00	0.000
251	10.21	10.21	10.03	0.95	0.00	68.	3.02	0.20	0.028	0.00	0.00	0.00	0.000
252	10.21	10.21	8.20	0.83	0.00	58.	2.40	0.18	0.025	0.00	0.02	0.00	0.003
253	10.21	10.21	12.40	0.19	0.39	34.	4.06	0.03	0.013	0.00	0.00	0.00	0.000
254	10.21	10.21	11.95	0.96	0.00	72.	3.82	0.22	0.032	0.00	0.06	0.00	0.007
255	10.21	10.21	10.48	1.19	0.00	81.	3.26	0.30	0.040	0.00	0.10	0.00	0.013
256	10.21	10.21	7.89	0.96	0.00	64.	2.44	0.27	0.035	0.00	0.12	0.00	0.014
257	10.21	10.21	12.40	0.49	0.26	50.	4.12	0.05	0.015	0.00	0.00	0.00	0.000
258	10.21	10.21	12.26	1.23	0.00	87.	3.99	0.23	0.034	0.00	0.06	0.00	0.007
259	10.21	10.21	10.52	1.22	0.00	82.	3.35	0.30	0.040	0.00	0.11	0.00	0.014
260	10.21	10.21	6.94	0.86	0.00	57.	2.22	0.25	0.033	0.00	0.12	0.00	0.014
261	10.21	10.21	11.78	0.57	0.16	53.	3.96	0.08	0.017	0.04	0.00	0.00	0.000
262	10.21	10.21	11.98	1.24	0.00	86.	3.94	0.24	0.034	0.03	0.04	0.00	0.005
263	10.21	10.21	9.97	1.10	0.00	75.	3.22	0.24	0.034	0.00	0.07	0.00	0.009

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
264	10.21	10.21	5.58	0.55	0.00	39.	1.82	0.15	0.021	0.00	0.05	0.00	0.006
265	10.21	10.21	10.90	0.67	0.00	56.	3.68	0.15	0.024	0.08	0.00	0.00	0.000
266	10.21	10.21	11.51	1.23	0.00	85.	3.81	0.25	0.036	0.10	0.03	0.00	0.004
267	10.21	10.21	9.26	1.01	0.00	69.	3.00	0.21	0.030	0.00	0.05	0.00	0.006
268	10.21	10.21	4.79	0.39	0.00	29.	1.56	0.10	0.014	0.00	0.01	0.00	0.001
269	10.21	10.21	10.41	0.69	0.00	56.	3.51	0.16	0.025	0.09	0.00	0.00	0.000
270	10.21	10.21	11.31	1.19	0.00	83.	3.77	0.25	0.036	0.14	0.01	0.00	0.002
271	10.21	10.21	8.85	0.92	0.00	64.	2.88	0.17	0.025	0.00	0.02	0.00	0.002
272	10.21	10.21	3.89	0.24	0.00	20.	1.27	0.05	0.008	0.00	-0.04	0.01	0.000
273	10.21	10.21	9.65	0.73	0.00	56.	3.26	0.15	0.024	0.13	-0.01	0.00	0.000
274	10.21	10.21	10.78	1.14	0.00	79.	3.58	0.23	0.033	0.18	-0.01	0.00	0.000
275	10.21	10.21	7.85	0.74	0.00	53.	2.55	0.12	0.018	0.00	-0.02	0.00	0.000
276	10.21	10.21	2.55	0.15	0.00	13.	0.80	0.02	0.004	0.00	-0.06	0.01	0.000
277	10.21	10.21	12.43	-0.03	0.43	23.	4.02	0.01	0.011	0.19	0.00	0.01	0.001
278	10.21	10.21	12.58	-0.03	0.43	24.	4.11	-0.01	0.010	0.16	-0.01	0.00	0.000
279	10.21	10.21	12.41	-0.05	0.43	22.	4.03	0.00	0.010	0.00	-0.01	0.00	0.000
280	10.21	10.21	12.51	0.01	0.43	26.	4.08	-0.01	0.010	0.00	0.00	0.00	0.000
281	10.21	10.21	12.62	0.00	0.43	25.	4.20	-0.01	0.010	0.02	-0.02	0.00	0.000
282	10.21	10.21	12.43	0.02	0.42	26.	4.23	0.00	0.011	0.02	-0.01	0.00	0.000
283	10.21	10.21	12.02	0.03	0.41	25.	4.16	0.01	0.011	0.02	0.00	0.00	0.000
284	10.21	10.21	11.53	0.01	0.39	24.	4.06	0.01	0.011	0.05	0.00	0.00	0.000
285	10.21	10.21	10.88	-0.02	0.37	21.	3.88	-0.01	0.009	0.21	-0.01	0.01	0.000
286	10.21	10.21	9.84	-0.11	0.34	14.	3.54	-0.04	0.007	0.25	-0.03	0.01	0.000
287	10.21	10.21	9.38	-0.14	0.32	12.	3.41	-0.05	0.006	0.33	-0.04	0.01	0.000
288	10.21	10.21	8.90	-0.18	0.29	9.	3.28	-0.07	0.004	0.44	-0.05	0.01	0.000
349	16.38	16.38	5.54	7.47	0.00	236.	2.50	4.73	0.199	0.08	4.23	0.00	0.178
350	16.38	16.38	2.53	-0.84	0.17	-2.	0.64	0.59	0.025	0.00	0.89	0.00	0.038
351	16.38	16.38	2.71	0.29	0.00	12.	0.23	0.84	0.036	0.00	1.09	0.00	0.046
352	10.21	10.21	2.86	0.91	0.00	51.	0.26	0.82	0.100	0.00	1.04	0.00	0.126
353	10.21	10.21	12.26	-0.01	0.42	24.	3.94	0.03	0.013	0.24	0.02	0.00	0.003

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
229	16.34	16.34	1.33	-0.82	0.15	-2.	0.37	0.02	0.002	0.79	-0.03	0.02	0.000
230	16.34	16.34	3.78	-1.39	0.27	-3.	0.91	-0.05	0.000	0.86	-0.13	0.03	0.000
231	16.34	16.34	4.69	-1.16	0.25	-2.	1.20	-0.02	0.001	0.79	-0.10	0.03	0.000
232	16.34	16.34	6.45	1.99	0.00	70.	1.72	2.11	0.126	0.81	2.10	0.00	0.126
233	16.34	16.34	5.80	-1.42	0.30	-2.	2.01	-0.05	0.001	0.33	-0.10	0.02	0.000
234	16.34	16.34	6.80	-1.48	0.33	-2.	2.10	-0.17	0.000	0.35	-0.25	0.04	0.000
235	16.34	16.34	7.34	-1.31	0.31	-2.	2.24	-0.15	0.000	0.32	-0.23	0.04	0.000
236	16.34	16.34	7.83	-0.16	0.22	5.	2.31	0.29	0.018	0.33	0.23	0.00	0.014
237	16.34	16.34	7.69	-1.75	0.38	-3.	2.30	-0.37	0.000	0.00	-0.43	0.07	0.000
238	16.34	16.34	8.21	-1.53	0.36	-2.	2.45	-0.35	0.000	0.00	-0.42	0.06	0.000
239	16.34	16.34	8.61	-1.36	0.34	-2.	2.58	-0.29	0.000	0.00	-0.36	0.06	0.000
240	16.34	16.34	8.78	-0.81	0.25	0.	2.55	-0.02	0.003	0.00	-0.14	0.02	0.000
241	16.34	16.34	8.72	-1.69	0.39	-2.	2.64	-0.51	0.000	0.00	-0.64	0.10	0.000
242	16.34	16.34	9.31	-1.46	0.36	-2.	2.84	-0.42	0.000	0.00	-0.53	0.08	0.000
243	16.34	16.34	9.62	-1.31	0.34	-1.	2.96	-0.34	0.000	0.00	-0.45	0.07	0.000
244	16.34	16.34	9.88	-1.02	0.30	-1.	2.92	-0.19	0.000	0.00	-0.33	0.05	0.000
245	16.34	16.34	10.23	-1.46	0.37	-2.	3.07	-0.50	0.000	0.00	-0.70	0.11	0.000
246	16.34	16.34	10.68	-1.31	0.36	-1.	3.29	-0.42	0.000	0.00	-0.59	0.09	0.000
247	16.34	16.34	10.87	-1.25	0.35	-1.	3.38	-0.37	0.000	0.00	-0.52	0.08	0.000
248	16.34	16.34	11.06	-1.08	0.33	-1.	3.47	-0.29	0.000	0.00	-0.43	0.07	0.000
249	16.34	16.34	11.61	-1.08	0.34	-1.	3.67	-0.45	0.000	0.00	-0.69	0.11	0.000
250	16.34	16.34	11.84	-1.11	0.34	-1.	3.81	-0.42	0.000	0.00	-0.61	0.09	0.000
251	16.34	16.34	11.91	-1.16	0.35	-1.	3.86	-0.40	0.000	0.00	-0.56	0.09	0.000
252	16.34	16.34	12.02	-1.10	0.34	-1.	3.93	-0.35	0.000	0.00	-0.50	0.08	0.000
253	16.34	16.34	12.86	-0.66	0.32	2.	4.20	-0.37	0.000	0.00	-0.65	0.10	0.000
254	16.34	16.34	12.79	-0.88	0.33	0.	4.23	-0.39	0.000	0.00	-0.61	0.09	0.000
255	16.34	16.34	12.72	-1.05	0.35	0.	4.23	-0.42	0.000	0.00	-0.60	0.09	0.000
256	16.34	16.34	12.74	-1.10	0.35	0.	4.26	-0.41	0.000	0.00	-0.56	0.09	0.000
257	16.34	16.34	14.23	-0.23	0.40	12.	4.77	-0.28	0.000	0.00	-0.60	0.09	0.000
258	16.34	16.34	13.78	-0.66	0.35	2.	4.65	-0.37	0.000	0.00	-0.61	0.09	0.000
259	16.34	16.34	13.55	-0.95	0.35	0.	4.60	-0.44	0.000	0.00	-0.63	0.10	0.000
260	16.34	16.34	13.38	-1.09	0.36	0.	4.55	-0.46	0.000	0.00	-0.62	0.10	0.000
261	16.34	16.34	15.76	0.21	0.40	26.	5.23	-0.18	0.002	0.00	-0.55	0.09	0.000
262	16.34	16.34	14.86	-0.43	0.40	7.	4.97	-0.34	0.000	0.00	-0.61	0.09	0.000
263	16.34	16.34	14.49	-0.84	0.37	1.	4.88	-0.44	0.000	0.00	-0.67	0.10	0.000
264	16.34	16.34	14.11	-1.10	0.38	0.	4.78	-0.50	0.000	0.00	-0.68	0.10	0.000
265	16.34	16.34	18.31	0.54	0.37	40.	6.00	-0.13	0.004	0.00	-0.53	0.08	0.000
266	16.34	16.34	16.80	-0.27	0.47	14.	5.54	-0.33	0.000	0.00	-0.63	0.10	0.000
267	16.34	16.34	16.28	-0.81	0.41	3.	5.41	-0.48	0.000	0.00	-0.72	0.11	0.000
268	16.34	16.34	15.54	-1.18	0.41	0.	5.18	-0.57	0.000	0.00	-0.75	0.12	0.000
269	16.34	16.34	22.84	0.79	0.42	54.	7.30	-0.10	0.006	0.16	-0.53	0.08	0.000
270	16.34	16.34	20.37	-0.13	0.56	22.	6.48	-0.33	0.001	0.09	-0.65	0.10	0.000
271	16.34	16.34	19.55	-0.85	0.50	5.	6.22	-0.55	0.000	0.16	-0.79	0.12	0.000
272	16.34	16.34	18.20	-1.33	0.48	0.	5.76	-0.65	0.000	0.13	-0.84	0.13	0.000
273	16.34	16.34	29.92	0.82	0.64	64.	9.28	-0.12	0.008	1.43	-0.57	0.11	0.000
274	16.34	16.34	26.54	-0.07	0.73	32.	7.94	-0.33	0.002	1.45	-0.67	0.12	0.000
275	16.34	16.34	24.12	-1.01	0.62	6.	7.01	-0.63	0.000	1.46	-0.88	0.16	0.000
276	16.34	16.34	21.09	-1.78	0.58	-1.	5.87	-0.79	0.000	1.53	-0.94	0.17	0.000
277	16.34	16.34	8.69	1.08	0.00	45.	2.31	1.35	0.081	0.98	1.32	0.00	0.079
278	16.34	16.34	8.89	-0.42	0.22	2.	2.35	0.55	0.034	0.35	0.59	0.00	0.035
279	16.34	16.34	9.29	-0.29	0.25	4.	2.64	0.02	0.004	0.00	-0.04	0.01	0.000
280	16.34	16.34	10.38	-0.54	0.26	1.	3.12	0.01	0.004	0.00	-0.12	0.02	0.000

			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP	
281	16.34	16.34	11.44	-0.78	0.29	0.	3.64	-0.14	0.001	0.00	-0.26	0.04	0.000	
282	16.34	16.34	12.26	-0.99	0.33	0.	4.05	-0.27	0.000	0.00	-0.38	0.06	0.000	
283	16.34	16.34	12.75	-1.20	0.37	-1.	4.31	-0.39	0.000	0.00	-0.49	0.08	0.000	
284	16.34	16.34	13.04	-1.41	0.41	-1.	4.46	-0.51	0.000	0.00	-0.60	0.09	0.000	
285	16.34	16.34	13.38	-1.63	0.45	-2.	4.59	-0.62	0.000	0.00	-0.71	0.11	0.000	
286	16.34	16.34	14.14	-1.87	0.49	-2.	4.76	-0.73	0.000	0.00	-0.81	0.13	0.000	
287	16.34	16.34	15.70	-2.20	0.57	-2.	4.92	-0.86	0.000	0.07	-0.93	0.14	0.000	
288	16.34	16.34	17.22	-2.69	0.67	-3.	4.38	-1.01	0.000	1.67	-1.05	0.19	0.000	
349	16.34	16.34	0.81	-0.14	0.03	0.	0.00	-0.22	0.000	0.79	-0.10	0.03	0.000	
350	16.34	16.34	3.69	-0.71	0.16	-1.	1.14	-0.35	0.000	0.53	-0.28	0.05	0.000	
351	16.34	16.34	4.35	-0.48	0.14	0.	1.38	-0.26	0.000	0.54	-0.20	0.04	0.000	
352	16.34	16.34	4.93	-1.23	0.26	-2.	1.62	-0.74	0.000	0.56	-0.63	0.10	0.000	
353	16.34	16.34	6.56	1.89	0.00	67.	2.18	1.35	0.081	0.67	1.31	0.00	0.078	

ARMATURA SUPERIORE ORIZZONTALE

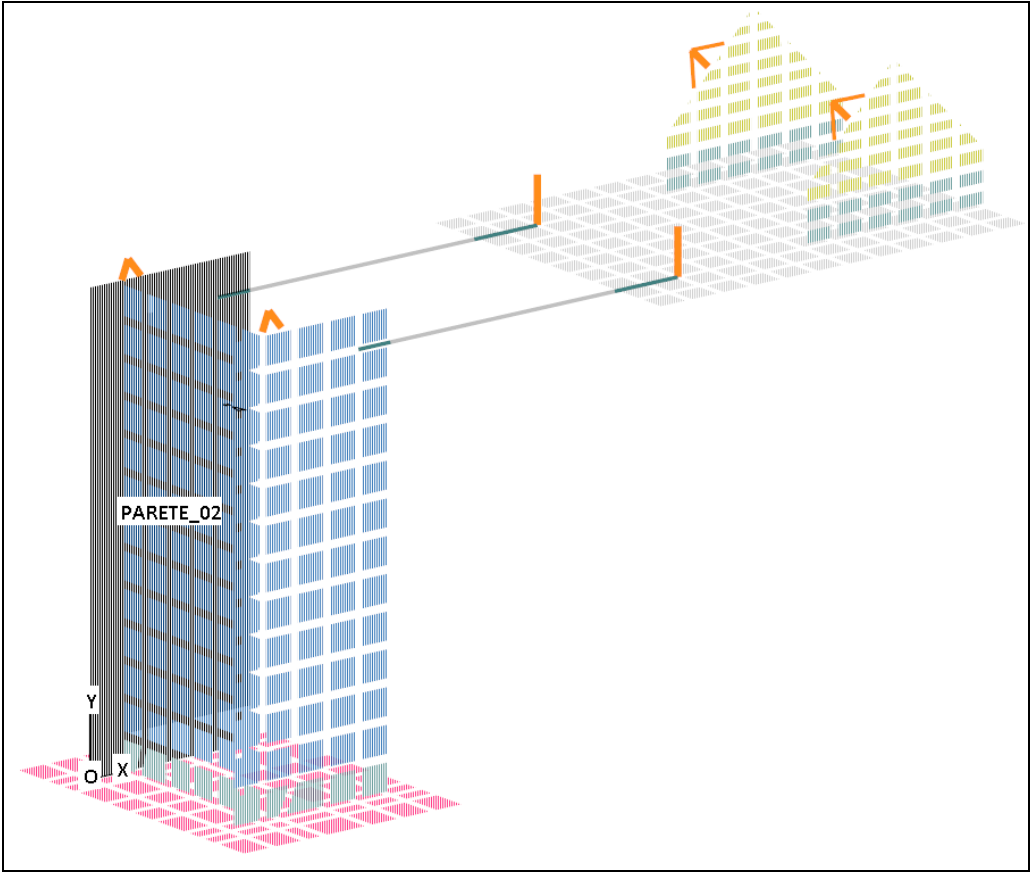
			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP	
229	16.38	16.38	9.37	5.41	0.00	178.	3.25	3.76	0.158	0.24	3.35	0.00	0.141	
230	16.38	16.38	12.06	-1.33	0.03	-5.	4.07	0.15	0.009	0.44	0.41	0.00	0.017	
231	16.38	16.38	13.94	-0.39	0.38	7.	5.00	0.41	0.019	0.40	0.63	0.00	0.027	
232	10.21	10.21	16.31	-0.04	0.56	31.	6.05	0.52	0.071	0.37	0.72	0.00	0.088	
233	16.38	16.38	9.98	4.13	0.00	139.	3.42	3.13	0.132	0.21	2.79	0.00	0.117	
234	16.38	16.38	12.45	-1.44	0.04	-5.	4.20	-0.02	0.003	0.41	0.21	0.00	0.009	
235	16.38	16.38	14.25	-0.72	0.36	2.	5.07	0.18	0.011	0.41	0.39	0.00	0.017	
236	10.21	10.21	16.49	-0.06	0.57	30.	6.07	0.32	0.049	0.42	0.51	0.00	0.063	
237	10.21	10.21	10.86	2.18	0.00	130.	3.69	2.08	0.252	0.19	1.76	0.00	0.214	
238	10.21	10.21	12.92	-1.93	0.11	-7.	4.34	-0.92	0.000	0.37	-0.70	0.11	0.000	
239	10.21	10.21	14.64	-1.19	0.04	-5.	5.16	-0.25	0.001	0.35	-0.05	0.00	0.000	
240	10.21	10.21	16.32	-0.24	0.55	21.	5.91	0.16	0.030	0.25	0.39	0.00	0.048	
241	10.21	10.21	12.38	-0.20	0.42	15.	4.20	-0.04	0.008	0.15	-0.10	0.01	0.000	
242	10.21	10.21	13.62	-0.35	0.44	12.	4.54	-0.58	0.000	0.25	-0.61	0.09	0.000	
243	10.21	10.21	15.26	-0.25	0.51	19.	5.32	-0.48	0.000	0.33	-0.49	0.07	0.000	
244	10.21	10.21	16.73	-0.10	0.57	28.	5.97	-0.18	0.005	0.32	-0.05	0.00	0.000	
245	10.21	10.21	12.78	-0.08	0.44	22.	4.29	-0.07	0.007	0.08	-0.10	0.01	0.000	
246	10.21	10.21	13.97	0.28	0.42	42.	4.72	0.01	0.013	0.21	-0.18	0.02	0.000	
247	10.21	10.21	15.63	0.35	0.47	49.	5.41	-0.02	0.013	0.36	-0.14	0.02	0.000	
248	10.21	10.21	17.21	0.44	0.49	56.	6.08	-0.04	0.013	0.51	-0.04	0.00	0.000	
249	10.21	10.21	12.69	0.08	0.43	29.	4.23	0.00	0.011	0.08	-0.03	0.00	0.000	
250	10.21	10.21	13.82	0.70	0.15	63.	4.67	0.16	0.028	0.23	0.00	0.01	0.001	
251	10.21	10.21	15.71	0.95	0.00	80.	5.43	0.20	0.033	0.42	0.00	0.01	0.001	
252	10.21	10.21	17.55	0.83	0.26	78.	6.15	0.18	0.033	0.60	0.02	0.01	0.004	
253	10.21	10.21	12.19	0.19	0.39	34.	4.09	0.03	0.013	0.09	0.00	0.00	0.000	
254	10.21	10.21	13.14	0.96	0.00	75.	4.49	0.22	0.034	0.25	0.06	0.00	0.007	
255	10.21	10.21	15.39	1.19	0.00	91.	5.34	0.30	0.044	0.49	0.10	0.00	0.013	
256	10.21	10.21	17.87	0.96	0.12	85.	6.22	0.27	0.043	0.75	0.12	0.00	0.015	
257	10.21	10.21	11.12	0.49	0.20	47.	3.77	0.05	0.014	0.07	0.00	0.00	0.001	
258	10.21	10.21	11.71	1.23	0.00	85.	4.05	0.23	0.035	0.21	0.06	0.00	0.007	
259	10.21	10.21	14.31	1.22	0.00	90.	5.03	0.30	0.044	0.51	0.11	0.00	0.014	
260	10.21	10.21	17.96	0.86	0.26	80.	6.25	0.25	0.041	0.97	0.12	0.00	0.015	
261	10.21	10.21	9.11	0.57	0.00	47.	3.13	0.08	0.015	0.01	0.00	0.00	0.000	
262	10.21	10.21	9.21	1.24	0.00	80.	3.23	0.24	0.033	0.11	0.04	0.00	0.005	
263	10.21	10.21	11.97	1.10	0.00	79.	4.27	0.24	0.036	0.44	0.07	0.00	0.009	
264	10.21	10.21	16.85	0.55	0.43	62.	5.90	0.15	0.030	1.10	0.05	0.02	0.007	
265	10.21	10.21	4.68	0.67	0.00	43.	1.80	0.15	0.020	0.00	0.00	0.00	0.000	
266	10.21	10.21	6.67	1.23	0.00	74.	2.55	0.25	0.033	0.04	0.03	0.00	0.004	
267	10.21	10.21	10.21	1.01	0.00	71.	3.68	0.21	0.031	0.42	0.05	0.00	0.006	
268	10.21	10.21	15.49	0.39	0.44	51.	5.46	0.10	0.023	1.15	0.01	0.04	0.004	
269	10.21	10.21	2.29	0.69	0.00	39.	0.96	0.16	0.020	0.00	0.00	0.00	0.000	
270	10.21	10.21	3.21	1.19	0.00	65.	1.45	0.25	0.032	0.00	0.01	0.00	0.001	
271	10.21	10.21	8.95	0.92	0.00	64.	3.28	0.17	0.026	0.39	0.02	0.01	0.003	
272	10.21	10.21	15.03	0.24	0.47	42.	5.34	0.05	0.018	1.29	-0.04	0.04	0.001	
273	10.21	10.21	0.14	0.73	0.00	36.	0.19	0.15	0.019	0.00	-0.01	0.00	0.000	
274	10.21	10.21	0.06	1.14	0.00	56.	0.32	0.23	0.028	0.00	-0.01	0.00	0.000	
275	10.21	10.21	6.42	0.74	0.00	50.	2.85	0.12	0.019	0.34	-0.02	0.01	0.000	
276	10.21	10.21	14.68	0.15	0.48	37.	5.26	0.02	0.015	1.52	-0.06	0.04	0.001	
277	10.21	10.21	6.51	-0.03	0.22	11.	2.13	0.01	0.006	0.10	0.00	0.00	0.001	
278	10.21	10.21	7.56	-0.03	0.26	14.	2.47	-0.01	0.006	0.08	-0.01	0.00	0.000	
279	10.21	10.21	9.37	-0.05	0.32	16.	3.09	0.00	0.008	0.13	-0.01	0.00	0.000	
280	10.21	10.21	11.03	0.01	0.38	23.	3.62	-0.01	0.009	0.10	0.00	0.00	0.000	
281	10.21	10.21	11.98	0.00	0.41	24.	3.92	-0.01	0.009	0.06	-0.02	0.00	0.000	
282	10.21	10.21	12.52	0.02	0.43	26.	4.14	0.00	0.011	0.03	-0.01	0.00	0.000	
283	10.21	10.21	12.67	0.03	0.43	27.	4.23	0.01	0.011	0.00	0.00	0.00	0.000	
284	10.21	10.21	12.43	0.01	0.42	26.	4.18	0.01	0.011	0.00	0.00	0.00	0.000	
285	10.21	10.21	11.52	-0.02	0.40	22.	3.90	-0.01	0.009	0.00	-0.01	0.00	0.000	
286	10.21	10.21	10.14	-0.11	0.35	15.	3.42	-0.04	0.006	0.00	-0.03	0.00	0.000	
287	10.21	10.21	9.49	-0.14	0.32	12.	3.21	-0.05	0.005	0.00	-0.04	0.01	0.000	
288	10.21	10.21	8.60	-0.18	0.28	9.	2.91	-0.07	0.004	0.00	-0.05	0.01	0.000	
349	16.38	16.38	8.46	7.47	0.00	239.	2.99	4.73	0.199	0.23	4.23	0.00	0.178	
350	16.38	16.38	11.52	-0.84	0.30	0.	3.91	0.59	0.026	0.49	0.89	0.00	0.038	
351	16.38	16.38	13.51	0.29	0.31	26.	4.89	0.84	0.037	0.42	1.09	0.00	0.046	
352	10.21	10.21	16.00	0.91	0.00	79.	5.97	0.82	0.105	0.26	1.04	0.00	0.126	
353	10.21	10.21	5.18	-0.01	0.18	10.	1.72	0.03	0.007	0.17	0.02	0.00	0.003	

ARMATURA SUPERIORE VERTICALE

	COMBINAZIONE RARA	COMB. FREQUENTE	COMB. QUASI PERMANENTE
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GUSCI	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	WkF	Mom	Nor	σC	WkP
229	16.34	16.34	13.38	-0.82	0.34	1.	4.73	0.02	0.007	0.00	-0.03	0.00	0.000
230	16.34	16.34	11.85	-1.39	0.04	-5.	3.79	-0.05	0.003	0.00	-0.13	0.02	0.000
231	16.34	16.34	11.01	-1.16	0.02	-5.	3.58	-0.02	0.004	0.00	-0.10	0.02	0.000
232	16.34	16.34	9.33	1.99	0.00	73.	2.87	2.11	0.126	0.00	2.10	0.00	0.126
233	16.34	16.34	14.88	-1.42	0.00	-6.	5.32	-0.05	0.005	0.00	-0.10	0.02	0.000
234	16.34	16.34	13.83	-1.48	0.03	-6.	4.97	-0.17	0.002	0.00	-0.25	0.04	0.000
235	16.34	16.34	13.25	-1.31	0.01	-5.	4.78	-0.15	0.002	0.00	-0.23	0.04	0.000
236	16.34	16.34	12.55	-0.16	0.35	11.	4.53	0.29	0.021	0.00	0.23	0.00	0.014
237	16.34	16.34	15.34	-1.75	0.05	-7.	5.32	-0.37	0.000	0.09	-0.43	0.07	0.000
238	16.34	16.34	14.81	-1.53	0.02	-6.	5.13	-0.35	0.000	0.17	-0.42	0.06	0.000
239	16.34	16.34	14.40	-1.36	0.00	-6.	4.99	-0.29	0.000	0.18	-0.36	0.05	0.000
240	16.34	16.34	14.10	-0.81	0.35	1.	4.88	-0.02	0.006	0.18	-0.14	0.02	0.000
241	16.34	16.34	15.17	-1.69	0.04	-6.	5.17	-0.51	0.000	0.32	-0.64	0.09	0.000
242	16.34	16.34	14.91	-1.46	0.01	-6.	5.08	-0.42	0.000	0.33	-0.53	0.08	0.000
243	16.34	16.34	14.67	-1.31	0.01	-5.	4.99	-0.34	0.000	0.31	-0.45	0.07	0.000
244	16.34	16.34	14.51	-1.02	0.38	0.	4.92	-0.19	0.001	0.31	-0.33	0.05	0.000
245	16.34	16.34	14.88	-1.46	0.01	-6.	5.02	-0.50	0.000	0.33	-0.70	0.10	0.000
246	16.34	16.34	14.71	-1.31	0.01	-6.	4.96	-0.42	0.000	0.29	-0.59	0.09	0.000
247	16.34	16.34	14.57	-1.25	0.02	-5.	4.90	-0.37	0.000	0.27	-0.52	0.08	0.000
248	16.34	16.34	14.46	-1.08	0.38	0.	4.86	-0.29	0.000	0.26	-0.43	0.06	0.000
249	16.34	16.34	14.44	-1.08	0.38	0.	4.85	-0.45	0.000	0.27	-0.69	0.10	0.000
250	16.34	16.34	14.31	-1.11	0.04	-5.	4.80	-0.42	0.000	0.24	-0.61	0.09	0.000
251	16.34	16.34	14.23	-1.16	0.03	-5.	4.76	-0.40	0.000	0.23	-0.56	0.08	0.000
252	16.34	16.34	14.17	-1.10	0.04	-5.	4.73	-0.35	0.000	0.22	-0.50	0.07	0.000
253	16.34	16.34	13.73	-0.66	0.35	2.	4.62	-0.37	0.000	0.35	-0.65	0.09	0.000
254	16.34	16.34	13.66	-0.88	0.35	1.	4.58	-0.39	0.000	0.29	-0.61	0.09	0.000
255	16.34	16.34	13.63	-1.05	0.04	-5.	4.56	-0.42	0.000	0.27	-0.60	0.09	0.000
256	16.34	16.34	13.65	-1.10	0.03	-5.	4.56	-0.41	0.000	0.25	-0.56	0.08	0.000
257	16.34	16.34	12.26	-0.23	0.34	9.	4.17	-0.28	0.000	0.47	-0.60	0.09	0.000
258	16.34	16.34	12.39	-0.66	0.31	2.	4.19	-0.37	0.000	0.39	-0.61	0.09	0.000
259	16.34	16.34	12.43	-0.95	0.04	-4.	4.19	-0.44	0.000	0.36	-0.63	0.09	0.000
260	16.34	16.34	12.62	-1.09	0.02	-5.	4.24	-0.46	0.000	0.34	-0.62	0.09	0.000
261	16.34	16.34	9.39	0.21	0.22	18.	3.36	-0.18	0.000	0.56	-0.55	0.08	0.000
262	16.34	16.34	9.93	-0.43	0.25	2.	3.50	-0.34	0.000	0.48	-0.61	0.09	0.000
263	16.34	16.34	10.12	-0.84	0.02	-4.	3.55	-0.44	0.000	0.44	-0.67	0.10	0.000
264	16.34	16.34	10.55	-1.10	0.02	-4.	3.67	-0.50	0.000	0.45	-0.68	0.10	0.000
265	16.34	16.34	3.61	0.54	0.00	21.	1.65	-0.13	0.000	0.45	-0.53	0.07	0.000
266	16.34	16.34	5.08	-0.27	0.13	1.	2.10	-0.33	0.000	0.46	-0.63	0.09	0.000
267	16.34	16.34	5.59	-0.81	0.04	-3.	2.25	-0.48	0.000	0.42	-0.72	0.10	0.000
268	16.34	16.34	6.41	-1.18	0.09	-4.	2.52	-0.57	0.000	0.46	-0.75	0.11	0.000
269	16.34	16.34	0.00	0.79	0.00	24.	0.00	-0.10	0.000	0.00	-0.53	0.08	0.000
270	16.34	16.34	0.00	-0.13	0.02	0.	0.00	-0.33	0.000	0.04	-0.65	0.10	0.000
271	16.34	16.34	0.00	-0.85	0.13	-2.	0.00	-0.55	0.000	0.03	-0.79	0.12	0.000
272	16.34	16.34	0.00	-1.33	0.20	-3.	0.37	-0.65	0.000	0.10	-0.84	0.13	0.000
273	16.34	16.34	0.00	0.82	0.00	25.	0.00	-0.12	0.000	0.00	-0.57	0.09	0.000
274	16.34	16.34	0.00	-0.07	0.01	0.	0.00	-0.33	0.000	0.00	-0.67	0.10	0.000
275	16.34	16.34	0.00	-1.01	0.15	-2.	0.00	-0.63	0.000	0.00	-0.88	0.14	0.000
276	16.34	16.34	0.00	-1.78	0.28	-4.	0.00	-0.79	0.000	0.00	-0.94	0.14	0.000
277	16.34	16.34	7.81	1.08	0.00	43.	2.22	1.35	0.081	0.00	1.32	0.00	0.079
278	16.34	16.34	11.47	-0.42	0.30	4.	4.06	0.55	0.035	0.00	0.59	0.00	0.035
279	16.34	16.34	13.56	-0.29	0.37	9.	4.68	0.02	0.007	0.21	-0.04	0.00	0.000
280	16.34	16.34	14.26	-0.54	0.37	4.	4.84	0.01	0.007	0.33	-0.12	0.01	0.000
281	16.34	16.34	14.30	-0.78	0.36	2.	4.79	-0.14	0.002	0.25	-0.26	0.04	0.000
282	16.34	16.34	14.08	-0.99	0.37	0.	4.68	-0.27	0.000	0.18	-0.38	0.06	0.000
283	16.34	16.34	13.69	-1.20	0.01	-5.	4.55	-0.39	0.000	0.21	-0.49	0.07	0.000
284	16.34	16.34	12.94	-1.41	0.03	-5.	4.33	-0.51	0.000	0.30	-0.60	0.09	0.000
285	16.34	16.34	11.35	-1.63	0.09	-6.	3.91	-0.62	0.000	0.44	-0.71	0.10	0.000
286	16.34	16.34	8.10	-1.87	0.17	-6.	3.06	-0.73	0.000	0.53	-0.81	0.12	0.000
287	16.34	16.34	2.01	-2.20	0.31	-5.	1.48	-0.86	0.000	0.25	-0.93	0.14	0.000
288	16.34	16.34	0.00	-2.69	0.41	-6.	0.00	-1.01	0.000	0.00	-1.05	0.16	0.000
349	16.34	16.34	5.55	-0.14	0.15	3.	1.93	-0.22	0.000	0.03	-0.10	0.01	0.000
350	16.34	16.34	6.09	-0.71	0.02	-3.	2.20	-0.35	0.000	0.00	-0.28	0.04	0.000
351	16.34	16.34	5.51	-0.48	0.01	-2.	2.02	-0.26	0.000	0.00	-0.20	0.03	0.000
352	16.34	16.34	5.75	-1.23	0.11	-4.	2.08	-0.74	0.000	0.00	-0.63	0.10	0.000
353	16.34	16.34	5.68	1.89	0.00	65.	2.05	1.35	0.081	0.00	1.31	0.00	0.079

6.4. PARETE 02



G353	G352	G351	G350	G349
G277	G232	G231	G230	G229
G278	G236	G235	G234	G233
G279	G240	G239	G238	G237
G280	G244	G243	G242	G241
G281	G248	G247	G246	G245
G282	G252	G251	G250	G249
G283	G256	G255	G254	G253
G284	G260	G259	G258	G257
G285	G264	G263	G262	G261
G286	G268	G267	G266	G265
G287	G272	G271	G270	G269
G288	G276	G275	G274	G273

6.4.1. Verifica SLU

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
169	0.6	16.38	16.38	0.	7.	0.00	1.08	16.34	16.34	0.	-1.	0.01	0.04
170	0.6	16.38	16.38	4.	1.	0.01	0.13	16.34	16.34	0.	-2.	0.01	-0.01
171	0.6	16.38	16.38	5.	2.	0.00	0.26	16.34	16.34	0.	-2.	0.01	-0.01
172	0.6	10.21	10.21	6.	1.	0.00	0.26	16.34	16.34	0.	3.	0.00	0.47
173	0.6	16.38	16.38	1.	5.	0.00	0.80	16.34	16.34	6.	-3.	0.03	-0.01
174	0.6	16.38	16.38	4.	0.	0.01	0.04	16.34	16.34	5.	-3.	0.03	0.00
175	0.6	16.38	16.38	4.	0.	0.01	0.09	16.34	16.34	5.	-2.	0.03	0.00
176	0.6	10.21	10.21	5.	0.	0.01	0.11	16.34	16.34	5.	-2.	0.02	0.02
177	0.6	10.21	10.21	0.	4.	0.00	0.88	16.34	16.34	13.	-4.	0.05	0.03
178	0.6	10.21	10.21	3.	-1.	0.02	0.02	16.34	16.34	13.	-3.	0.05	0.03
179	0.6	10.21	10.21	4.	-1.	0.02	0.03	16.34	16.34	12.	-3.	0.04	0.03
180	0.6	10.21	10.21	4.	0.	0.01	0.06	16.34	16.34	12.	-3.	0.04	0.04
181	0.6	10.21	10.21	0.	0.	0.00	0.10	16.34	16.34	16.	-4.	0.06	0.04
182	0.6	10.21	10.21	3.	-1.	0.01	0.02	16.34	16.34	16.	-4.	0.05	0.05
183	0.6	10.21	10.21	3.	-1.	0.01	0.02	16.34	16.34	14.	-3.	0.05	0.05
184	0.6	10.21	10.21	3.	0.	0.01	0.03	16.34	16.34	14.	-3.	0.05	0.05
185	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	17.	-4.	0.06	0.05
186	0.6	10.21	10.21	2.	0.	0.01	0.01	16.34	16.34	17.	-3.	0.06	0.06
187	0.6	10.21	10.21	2.	0.	0.01	0.04	16.34	16.34	17.	-3.	0.05	0.06
188	0.6	10.21	10.21	2.	0.	0.00	0.08	16.34	16.34	17.	-3.	0.05	0.06
189	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	19.	-4.	0.06	0.06
190	0.6	10.21	10.21	1.	0.	0.00	0.10	16.34	16.34	19.	-3.	0.06	0.06
191	0.6	10.21	10.21	2.	1.	0.00	0.15	16.34	16.34	18.	-3.	0.06	0.06
192	0.6	10.21	10.21	2.	1.	0.00	0.16	16.34	16.34	18.	-3.	0.05	0.06
193	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	20.	-3.	0.06	0.07
194	0.6	10.21	10.21	1.	1.	0.00	0.12	16.34	16.34	21.	-3.	0.06	0.07
195	0.6	10.21	10.21	2.	1.	0.00	0.19	16.34	16.34	21.	-3.	0.06	0.07
196	0.6	10.21	10.21	3.	1.	0.00	0.19	16.34	16.34	20.	-3.	0.06	0.08
197	0.6	10.21	10.21	0.	0.	0.00	0.04	16.34	16.34	22.	-3.	0.06	0.08
198	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	22.	-3.	0.06	0.08
199	0.6	10.21	10.21	2.	1.	0.00	0.19	16.34	16.34	22.	-3.	0.06	0.08
200	0.6	10.21	10.21	3.	1.	0.00	0.18	16.34	16.34	22.	-3.	0.06	0.08
201	0.6	10.21	10.21	0.	0.	0.00	0.07	16.34	16.34	24.	-3.	0.06	0.10
202	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	23.	-3.	0.06	0.09
203	0.6	10.21	10.21	1.	1.	0.00	0.16	16.34	16.34	23.	-3.	0.06	0.09
204	0.6	10.21	10.21	4.	0.	0.00	0.13	16.34	16.34	23.	-3.	0.06	0.09
205	0.6	10.21	10.21	0.	1.	0.00	0.12	16.34	16.34	19.	-2.	0.05	0.08
206	0.6	10.21	10.21	0.	1.	0.00	0.15	16.34	16.34	20.	-3.	0.05	0.08
207	0.6	10.21	10.21	1.	1.	0.00	0.13	16.34	16.34	20.	-3.	0.06	0.07
208	0.6	10.21	10.21	4.	0.	0.00	0.08	16.34	16.34	20.	-3.	0.06	0.07
209	0.6	10.21	10.21	0.	1.	0.00	0.15	16.34	16.34	8.	-1.	0.02	0.03
210	0.6	10.21	10.21	0.	1.	0.00	0.16	16.34	16.34	9.	-2.	0.03	0.03
211	0.6	10.21	10.21	1.	0.	0.00	0.11	16.34	16.34	10.	-2.	0.04	0.03
212	0.6	10.21	10.21	4.	0.	0.01	0.06	16.34	16.34	11.	-3.	0.04	0.03
213	0.6	10.21	10.21	0.	1.	0.00	0.17	16.34	16.34	2.	-1.	0.02	0.01
214	0.6	10.21	10.21	0.	1.	0.00	0.17	16.34	16.34	0.	-2.	0.02	-0.02
215	0.6	10.21	10.21	0.	0.	0.00	0.07	16.34	16.34	0.	-3.	0.02	-0.02
216	0.6	10.21	10.21	3.	0.	0.01	0.04	16.34	16.34	0.	-3.	0.03	-0.03
217	0.6	10.21	10.21	1.	0.	0.00	0.06	16.34	16.34	0.	3.	0.00	0.45
218	0.6	10.21	10.21	1.	0.	0.00	0.05	16.34	16.34	6.	0.	0.01	0.11
219	0.6	10.21	10.21	1.	0.	0.00	0.05	16.34	16.34	12.	-2.	0.04	0.05
220	0.6	10.21	10.21	1.	0.	0.00	0.03	16.34	16.34	15.	-2.	0.04	0.06
221	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	17.	-2.	0.05	0.07
222	0.6	10.21	10.21	1.	0.	0.00	0.02	16.34	16.34	18.	-3.	0.05	0.07
223	0.6	10.21	10.21	1.	0.	0.00	0.02	16.34	16.34	20.	-3.	0.06	0.08
224	0.6	10.21	10.21	1.	0.	0.00	0.02	16.34	16.34	21.	-3.	0.06	0.08
225	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	22.	-3.	0.06	0.08
226	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	21.	-3.	0.06	0.07
227	0.6	10.21	10.21	1.	0.	0.00	0.03	16.34	16.34	15.	-4.	0.05	0.04
228	0.6	10.21	10.21	1.	0.	0.01	0.03	16.34	16.34	2.	-4.	0.04	-0.03
354	0.6	16.38	16.38	0.	10.	0.00	1.45	16.34	16.34	0.	-1.	0.01	0.09
355	0.6	16.38	16.38	5.	3.	0.00	0.45	16.34	16.34	2.	-2.	0.02	0.01
356	0.6	16.38	16.38	6.	3.	0.00	0.46	16.34	16.34	2.	-2.	0.02	0.01
358	0.6	10.21	10.21	1.	0.	0.00	0.07	16.34	16.34	5.	0.	0.01	0.10
759	0.6	10.21	10.21	6.	1.	0.00	0.22	16.34	16.34	3.	-1.	0.02	0.01
761	0.6	10.21	10.21	8.	3.	0.00	0.67	16.34	16.34	3.	-2.	0.02	0.01

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
169	0.6	16.38	16.38	1.	7.	0.00	1.09	16.34	16.34	14.	-1.	0.03	0.11
170	0.6	16.38	16.38	6.	1.	0.01	0.14	16.34	16.34	13.	-2.	0.04	0.07
171	0.6	16.38	16.38	10.	2.	0.00	0.28	16.34	16.34	12.	-2.	0.04	0.06
172	0.6	10.21	10.21	12.	1.	0.00	0.33	16.34	16.34	10.	3.	0.02	0.52
173	0.6	16.38	16.38	1.	5.	0.00	0.80	16.34	16.34	13.	-3.	0.05	0.06
174	0.6	16.38	16.38	6.	0.	0.01	0.05	16.34	16.34	10.	-3.	0.04	0.04
175	0.6	16.38	16.38	8.	0.	0.01	0.11	16.34	16.34	10.	-2.	0.04	0.04
176	0.6	10.21	10.21	10.	0.	0.02	0.16	16.34	16.34	11.	-2.	0.03	0.04
177	0.6	10.21	10.21	1.	4.	0.00	0.89	16.34	16.34	20.	-4.	0.06	0.06
178	0.6	10.21	10.21	3.	-1.	0.02	0.03	16.34	16.34	18.	-3.	0.06	0.06
179	0.6	10.21	10.21	4.	-1.	0.02	0.05	16.34	16.34	16.	-3.	0.05	0.06
180	0.6	10.21	10.21	8.	0.	0.02	0.10	16.34	16.34	16.	-3.	0.05	0.06
181	0.6	10.21	10.21	1.	0.	0.00	0.10	16.34	16.34	21.	-4.	0.07	0.07
182	0.6	10.21	10.21	3.	-1.	0.01	0.02	16.34	16.34	20.	-4.	0.06	0.07
183	0.6	10.21	10.21	3.	-1.	0.01	0.02	16.34	16.34	18.	-3.	0.05	0.06
184	0.6	10.21	10.21	4.	0.	0.01	0.05	16.34	16.34	18.	-3.	0.05	0.07
185	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	20.	-4.	0.06	0.06
186	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	18.	-3.	0.06	0.06

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
187	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	18.	-3.	0.06	0.06	
188	0.6	10.21	10.21	0.	0.	0.00	0.06	16.34	16.34	17.	-3.	0.05	0.06	
189	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	19.	-4.	0.06	0.06	
190	0.6	10.21	10.21	0.	0.	0.00	0.09	16.34	16.34	19.	-3.	0.06	0.06	
191	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	18.	-3.	0.06	0.07	
192	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	18.	-3.	0.06	0.07	
193	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	17.	-3.	0.06	0.06	
194	0.6	10.21	10.21	0.	1.	0.00	0.12	16.34	16.34	17.	-3.	0.05	0.06	
195	0.6	10.21	10.21	0.	1.	0.00	0.18	16.34	16.34	18.	-3.	0.05	0.06	
196	0.6	10.21	10.21	0.	1.	0.00	0.16	16.34	16.34	17.	-3.	0.05	0.06	
197	0.6	10.21	10.21	0.	0.	0.00	0.04	16.34	16.34	16.	-3.	0.05	0.05	
198	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	16.	-3.	0.05	0.05	
199	0.6	10.21	10.21	0.	1.	0.00	0.17	16.34	16.34	16.	-3.	0.05	0.05	
200	0.6	10.21	10.21	0.	1.	0.00	0.15	16.34	16.34	16.	-3.	0.05	0.05	
201	0.6	10.21	10.21	0.	0.	0.00	0.08	16.34	16.34	12.	-3.	0.04	0.04	
202	0.6	10.21	10.21	0.	1.	0.00	0.14	16.34	16.34	13.	-3.	0.05	0.04	
203	0.6	10.21	10.21	0.	1.	0.00	0.15	16.34	16.34	13.	-3.	0.05	0.04	
204	0.6	10.21	10.21	0.	0.	0.00	0.10	16.34	16.34	14.	-3.	0.05	0.04	
205	0.6	10.21	10.21	1.	1.	0.00	0.12	16.34	16.34	8.	-2.	0.03	0.02	
206	0.6	10.21	10.21	1.	1.	0.00	0.16	16.34	16.34	9.	-3.	0.04	0.02	
207	0.6	10.21	10.21	0.	1.	0.00	0.12	16.34	16.34	10.	-3.	0.04	0.02	
208	0.6	10.21	10.21	0.	0.	0.00	0.05	16.34	16.34	10.	-3.	0.04	0.02	
209	0.6	10.21	10.21	1.	1.	0.00	0.16	16.34	16.34	3.	-1.	0.02	0.01	
210	0.6	10.21	10.21	1.	1.	0.00	0.17	16.34	16.34	6.	-2.	0.03	0.01	
211	0.6	10.21	10.21	0.	0.	0.00	0.10	16.34	16.34	6.	-2.	0.03	0.01	
212	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	7.	-3.	0.04	0.01	
213	0.6	10.21	10.21	1.	1.	0.00	0.18	16.34	16.34	0.	-1.	0.01	-0.01	
214	0.6	10.21	10.21	1.	1.	0.00	0.19	16.34	16.34	1.	-2.	0.02	-0.01	
215	0.6	10.21	10.21	0.	0.	0.00	0.07	16.34	16.34	4.	-3.	0.03	-0.01	
216	0.6	10.21	10.21	0.	0.	0.00	0.00	16.34	16.34	5.	-3.	0.04	-0.01	
217	0.6	10.21	10.21	1.	0.	0.00	0.05	16.34	16.34	9.	3.	0.00	0.50	
218	0.6	10.21	10.21	1.	0.	0.00	0.04	16.34	16.34	9.	0.	0.02	0.12	
219	0.6	10.21	10.21	1.	0.	0.00	0.04	16.34	16.34	14.	-2.	0.04	0.06	
220	0.6	10.21	10.21	1.	0.	0.00	0.03	16.34	16.34	17.	-2.	0.05	0.07	
221	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	17.	-2.	0.05	0.07	
222	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	18.	-3.	0.05	0.07	
223	0.6	10.21	10.21	0.	0.	0.00	0.01	16.34	16.34	18.	-3.	0.05	0.07	
224	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	17.	-3.	0.05	0.06	
225	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	14.	-3.	0.05	0.04	
226	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	11.	-3.	0.05	0.03	
227	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	9.	-4.	0.04	0.02	
228	0.6	10.21	10.21	0.	0.	0.00	0.02	16.34	16.34	14.	-4.	0.06	0.03	
354	0.6	16.38	16.38	2.	10.	0.00	1.46	16.34	16.34	7.	-1.	0.02	0.11	
355	0.6	16.38	16.38	8.	3.	0.00	0.47	16.34	16.34	6.	-2.	0.03	0.03	
356	0.6	16.38	16.38	13.	3.	0.00	0.51	16.34	16.34	6.	-2.	0.03	0.02	
358	0.6	10.21	10.21	0.	0.	0.00	0.06	16.34	16.34	8.	0.	0.01	0.11	
759	0.6	10.21	10.21	14.	1.	0.00	0.30	16.34	16.34	7.	-1.	0.02	0.03	
761	0.6	10.21	10.21	19.	3.	0.00	0.78	16.34	16.34	6.	-2.	0.03	0.03	

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO ($R_d > E_d$)

6.4.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF
169	16.38	16.38	6.91	4.46	0.00	145.	2.86	3.46	0.145
170	16.38	16.38	5.42	-0.25	0.14	1.	2.35	0.57	0.024
171	16.38	16.38	5.71	0.81	0.00	32.	1.27	0.83	0.035
172	10.21	10.21	6.08	0.36	0.00	31.	2.29	0.72	0.088
173	16.38	16.38	7.68	3.23	0.00	109.	3.09	2.86	0.121
174	16.38	16.38	6.36	-0.18	0.17	3.	2.78	0.35	0.016
175	16.38	16.38	6.56	0.22	0.12	15.	1.93	0.57	0.024
176	10.21	10.21	6.88	0.16	0.20	22.	2.77	0.44	0.056
177	10.21	10.21	9.02	1.46	0.00	91.	3.53	1.76	0.214
178	10.21	10.21	7.80	-1.42	0.35	-2.	3.38	-0.50	0.000
179	10.21	10.21	7.72	-0.21	0.25	6.	2.58	0.14	0.021
180	10.21	10.21	7.76	0.02	0.26	17.	3.05	0.27	0.037
181	10.21	10.21	10.87	-0.40	0.32	5.	4.08	-0.14	0.003
182	10.21	10.21	9.68	-0.71	0.27	0.	3.86	-0.69	0.000
183	10.21	10.21	9.21	-0.71	0.26	0.	3.34	-0.31	0.000
184	10.21	10.21	9.06	-0.22	0.29	8.	3.63	-0.05	0.006
185	10.21	10.21	11.52	-0.21	0.39	13.	4.16	-0.13	0.004
186	10.21	10.21	10.84	-0.41	0.32	5.	3.95	-0.04	0.008
187	10.21	10.21	10.30	-0.01	0.35	20.	3.89	-0.21	0.001
188	10.21	10.21	10.11	-0.18	0.34	12.	4.10	-0.17	0.002
189	10.21	10.21	11.86	-0.05	0.41	21.	4.11	-0.04	0.008
190	10.21	10.21	11.61	-0.05	0.40	21.	4.25	-0.07	0.006
191	10.21	10.21	11.11	-0.07	0.38	19.	4.27	-0.10	0.005
192	10.21	10.21	10.80	-0.01	0.37	21.	4.14	-0.10	0.005
193	10.21	10.21	12.14	0.00	0.42	24.	4.20	-0.01	0.010

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
194	10.21	10.21	12.06	0.05	0.41	27.	4.45	-0.01	0.010	0.31	0.06	0.00	0.007
195	10.21	10.21	11.50	0.07	0.39	27.	4.45	-0.01	0.011	0.55	0.11	0.00	0.013
196	10.21	10.21	11.44	0.09	0.37	27.	3.93	-0.02	0.009	0.81	0.12	0.00	0.015
197	10.21	10.21	12.13	0.00	0.41	24.	4.15	-0.01	0.010	0.14	0.00	0.00	0.001
198	10.21	10.21	12.15	0.05	0.41	26.	4.30	-0.02	0.010	0.26	0.06	0.00	0.008
199	10.21	10.21	11.41	0.06	0.38	26.	4.21	0.00	0.011	0.57	0.11	0.00	0.014
200	10.21	10.21	11.06	0.05	0.37	25.	3.62	-0.01	0.008	1.03	0.12	0.00	0.016
201	10.21	10.21	11.48	-0.02	0.39	22.	3.85	-0.02	0.009	0.08	0.00	0.00	0.001
202	10.21	10.21	11.48	-0.01	0.39	23.	3.94	-0.04	0.007	0.15	0.04	0.00	0.005
203	10.21	10.21	10.55	-0.02	0.36	20.	3.75	-0.04	0.007	0.48	0.07	0.00	0.009
204	10.21	10.21	10.20	-0.10	0.35	16.	3.31	-0.06	0.005	1.16	0.05	0.02	0.008
205	10.21	10.21	10.42	-0.03	0.36	19.	3.47	-0.02	0.007	0.00	0.01	0.00	0.001
206	10.21	10.21	10.53	-0.04	0.36	19.	3.57	-0.06	0.005	0.05	0.03	0.00	0.004
207	10.21	10.21	9.49	-0.08	0.33	15.	3.31	-0.06	0.005	0.45	0.05	0.00	0.006
208	10.21	10.21	9.24	-0.17	0.31	10.	2.99	-0.08	0.003	1.20	0.01	0.04	0.004
209	10.21	10.21	9.94	-0.04	0.34	18.	3.28	-0.03	0.006	0.00	0.01	0.00	0.001
210	10.21	10.21	10.03	-0.09	0.34	16.	3.37	0.00	0.009	0.00	0.01	0.00	0.002
211	10.21	10.21	8.94	-0.14	0.30	11.	3.06	-0.10	0.002	0.42	0.02	0.01	0.003
212	10.21	10.21	8.78	-0.26	0.27	6.	2.84	-0.12	0.001	1.33	-0.03	0.04	0.001
213	10.21	10.21	9.26	-0.05	0.32	16.	3.05	-0.01	0.007	0.00	0.00	0.00	0.001
214	10.21	10.21	9.28	-0.14	0.31	12.	3.11	-0.06	0.004	0.00	-0.01	0.00	0.000
215	10.21	10.21	7.76	-0.23	0.24	5.	2.65	-0.14	0.001	0.33	-0.02	0.01	0.000
216	10.21	10.21	7.85	-0.30	0.23	3.	2.61	-0.12	0.001	1.55	-0.06	0.05	0.001
217	10.21	10.21	11.83	0.00	0.40	24.	4.14	0.01	0.012	0.20	0.01	0.01	0.001
218	10.21	10.21	11.98	-0.01	0.41	23.	4.17	0.00	0.011	0.14	-0.01	0.00	0.000
219	10.21	10.21	12.03	0.04	0.41	26.	4.19	0.02	0.013	0.08	0.01	0.00	0.001
220	10.21	10.21	12.37	-0.01	0.42	24.	4.27	-0.01	0.010	0.04	-0.01	0.00	0.000
221	10.21	10.21	12.56	-0.04	0.43	23.	4.28	-0.02	0.009	0.00	-0.02	0.00	0.000
222	10.21	10.21	12.56	-0.02	0.43	24.	4.24	-0.02	0.010	0.00	-0.01	0.00	0.000
223	10.21	10.21	12.38	-0.01	0.42	24.	4.12	-0.01	0.010	0.02	0.00	0.00	0.000
224	10.21	10.21	11.93	-0.01	0.41	23.	3.90	0.00	0.010	0.04	0.00	0.00	0.000
225	10.21	10.21	10.81	-0.03	0.37	20.	3.48	-0.01	0.008	0.07	-0.01	0.00	0.000
226	10.21	10.21	9.86	-0.08	0.34	16.	3.14	-0.03	0.006	0.07	-0.03	0.01	0.000
227	10.21	10.21	9.26	-0.10	0.32	14.	2.91	-0.03	0.005	0.05	-0.04	0.01	0.000
228	10.21	10.21	8.46	-0.12	0.29	11.	2.60	-0.04	0.004	0.04	-0.05	0.01	0.000
354	16.38	16.38	5.81	6.41	0.00	203.	2.75	4.38	0.184	0.10	4.23	0.00	0.178
355	16.38	16.38	4.25	0.58	0.00	23.	2.16	1.03	0.043	0.18	0.89	0.00	0.038
356	16.38	16.38	4.72	1.48	0.00	51.	0.79	1.27	0.054	0.19	1.10	0.00	0.046
358	10.21	10.21	11.65	0.03	0.40	25.	4.10	0.03	0.013	0.27	0.02	0.00	0.003
759	10.21	10.21	5.72	0.40	0.00	32.	1.69	0.78	0.095	0.20	0.72	0.00	0.088
761	10.21	10.21	5.04	1.01	0.00	60.	1.11	1.13	0.137	0.20	1.00	0.00	0.122

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
169	16.34	16.34	0.00	-1.64	0.25	-4.	0.07	-0.16	0.000	0.01	-0.05	0.01	0.000
170	16.34	16.34	1.22	-2.06	0.34	-5.	0.65	-0.25	0.000	0.00	-0.10	0.02	0.000
171	16.34	16.34	2.01	-1.93	0.33	-4.	0.98	-0.26	0.000	0.00	-0.12	0.02	0.000
172	16.34	16.34	3.50	1.09	0.00	38.	1.44	1.92	0.115	0.00	2.03	0.00	0.122
173	16.34	16.34	4.47	-2.19	0.40	-4.	2.43	-0.24	0.000	0.10	-0.11	0.02	0.000
174	16.34	16.34	5.47	-2.25	0.43	-4.	2.73	-0.37	0.000	0.16	-0.25	0.04	0.000
175	16.34	16.34	6.02	-2.12	0.41	-4.	2.90	-0.36	0.000	0.16	-0.25	0.04	0.000
176	16.34	16.34	6.30	-1.24	0.28	-2.	2.96	0.16	0.012	0.16	0.21	0.00	0.013
177	16.34	16.34	7.44	-2.47	0.49	-4.	2.93	-0.57	0.000	0.33	-0.44	0.07	0.000
178	16.34	16.34	8.28	-2.31	0.48	-4.	3.29	-0.55	0.000	0.37	-0.43	0.07	0.000
179	16.34	16.34	8.66	-2.16	0.46	-4.	3.41	-0.50	0.000	0.36	-0.37	0.06	0.000
180	16.34	16.34	9.01	-1.78	0.40	-3.	3.61	-0.31	0.000	0.36	-0.15	0.03	0.000
181	16.34	16.34	9.81	-2.66	0.55	-5.	3.54	-0.77	0.000	0.42	-0.65	0.11	0.000
182	16.34	16.34	10.36	-2.40	0.52	-4.	3.75	-0.66	0.000	0.40	-0.54	0.09	0.000
183	16.34	16.34	10.61	-2.23	0.50	-3.	3.83	-0.59	0.000	0.37	-0.46	0.08	0.000
184	16.34	16.34	10.85	-1.98	0.46	-3.	3.95	-0.47	0.000	0.37	-0.33	0.06	0.000
185	16.34	16.34	11.39	-2.67	0.58	-4.	4.65	-0.88	0.000	0.38	-0.71	0.12	0.000
186	16.34	16.34	11.70	-2.41	0.54	-4.	4.59	-0.76	0.000	0.37	-0.60	0.10	0.000
187	16.34	16.34	11.85	-2.26	0.52	-3.	4.58	-0.68	0.000	0.35	-0.52	0.09	0.000
188	16.34	16.34	12.00	-2.07	0.49	-3.	4.56	-0.58	0.000	0.34	-0.43	0.07	0.000
189	16.34	16.34	12.95	-2.55	0.58	-4.	4.64	-0.93	0.000	0.38	-0.70	0.11	0.000
190	16.34	16.34	13.00	-2.36	0.55	-3.	4.59	-0.82	0.000	0.35	-0.61	0.10	0.000
191	16.34	16.34	13.04	-2.26	0.54	-3.	4.59	-0.75	0.000	0.34	-0.57	0.09	0.000
192	16.34	16.34	13.02	-2.12	0.52	-3.	4.55	-0.68	0.000	0.32	-0.50	0.08	0.000
193	16.34	16.34	13.86	-2.36	0.57	-3.	4.76	-0.92	0.000	0.44	-0.65	0.11	0.000
194	16.34	16.34	13.80	-2.27	0.55	-3.	4.71	-0.84	0.000	0.37	-0.62	0.10	0.000
195	16.34	16.34	13.78	-2.23	0.54	-3.	4.69	-0.79	0.000	0.36	-0.60	0.10	0.000
196	16.34	16.34	13.72	-2.15	0.53	-3.	4.64	-0.74	0.000	0.33	-0.56	0.09	0.000
197	16.34	16.34	14.83	-2.16	0.55	-3.	4.98	-0.90	0.000	0.54	-0.60	0.10	0.000
198	16.34	16.34	14.65	-2.18	0.55	-3.	4.91	-0.85	0.000	0.46	-0.61	0.10	0.000
199	16.34	16.34	14.55	-2.21	0.55	-3.	4.86	-0.83	0.000	0.43	-0.63	0.10	0.000
200	16.34	16.34	14.42	-2.18	0.55	-3.	4.80	-0.79	0.000	0.41	-0.62	0.10	0.000
201	16.34	16.34	16.09	-2.06	0.55	-2.	5.39	-0.93	0.000	0.60	-0.56	0.09	0.000
202	16.34	16.34	15.68	-2.16	0.56	-2.	5.24	-0.90	0.000	0.53	-0.62	0.10	0.000
203	16.34	16.34	15.47	-2.25	0.57	-3.	5.15	-0.90	0.000	0.49	-0.67	0.11	0.000
204	16.34	16.34	15.24	-2.26	0.57	-3.	5.06	-0.87	0.000	0.49	-0.68	0.11	0.000
205	16.34	16.34	17.79	-2.06	0.58	-2.	6.15	-1.02	0.000	0.44	-0.53	0.09	0.000
206	16.34	16.34	16.85	-2.22	0.59	-2.	5.77	-1.00	0.000	0.46	-0.63	0.10	0.000
207	16.34	16.34	16.41	-2.37	0.60	-3.	5.59	-1.01	0.000	0.42	-0.72	0.12	0.000
208	16.34	16.34	15.93	-2.43	0.61	-3.	5.41	-0.99	0.000	0.47	-0.75	0.12	0.000
209	16.34	16.34	19.03	-2.05	0.59	-2.	6.84	-1.07	0.000	0.00	-0.54	0.08	0.000

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
210	16.34	16.34	16.80	-2.27	0.59	-2.	6.05	-1.06	0.000	0.00	-0.66	0.10	0.000
211	16.34	16.34	15.74	-2.52	0.62	-3.	5.69	-1.11	0.000	0.00	-0.80	0.12	0.000
212	16.34	16.34	14.53	-2.60	0.61	-4.	5.28	-1.08	0.000	0.06	-0.84	0.13	0.000
213	16.34	16.34	17.45	-2.12	0.58	-2.	6.01	-1.09	0.000	0.00	-0.57	0.09	0.000
214	16.34	16.34	11.32	-2.32	0.52	-3.	4.19	-1.07	0.000	0.00	-0.67	0.10	0.000
215	16.34	16.34	8.29	-2.72	0.54	-5.	3.34	-1.18	0.000	0.00	-0.88	0.14	0.000
216	16.34	16.34	4.14	-2.80	0.49	-6.	1.98	-1.10	0.000	0.00	-0.95	0.15	0.000
217	16.34	16.34	4.94	0.34	0.00	17.	1.88	1.11	0.067	0.00	1.23	0.00	0.074
218	16.34	16.34	7.32	-0.55	0.19	0.	3.03	0.60	0.037	0.16	0.55	0.00	0.033
219	16.34	16.34	9.74	-1.42	0.36	-2.	3.79	-0.05	0.003	0.39	0.00	0.01	0.000
220	16.34	16.34	11.37	-1.56	0.41	-2.	4.23	-0.27	0.000	0.37	-0.12	0.02	0.000
221	16.34	16.34	12.32	-1.72	0.44	-2.	4.53	-0.40	0.000	0.31	-0.26	0.04	0.000
222	16.34	16.34	12.98	-1.88	0.48	-2.	4.48	-0.54	0.000	0.28	-0.38	0.06	0.000
223	16.34	16.34	13.62	-2.01	0.51	-2.	4.56	-0.64	0.000	0.28	-0.49	0.08	0.000
224	16.34	16.34	14.21	-2.15	0.54	-3.	4.70	-0.73	0.000	0.37	-0.60	0.10	0.000
225	16.34	16.34	14.81	-2.31	0.57	-3.	4.89	-0.82	0.000	0.49	-0.71	0.12	0.000
226	16.34	16.34	14.99	-2.54	0.61	-3.	5.06	-0.95	0.000	0.55	-0.82	0.13	0.000
227	16.34	16.34	12.20	-2.76	0.60	-4.	4.50	-1.04	0.000	0.23	-0.93	0.15	0.000
228	16.34	16.34	0.00	-3.00	0.46	-7.	0.05	-1.07	0.000	0.00	-1.06	0.16	0.000
354	16.34	16.34	1.23	-0.81	0.14	-2.	0.00	-0.45	0.000	0.02	-0.29	0.04	0.000
355	16.34	16.34	2.27	-1.59	0.28	-3.	0.54	-0.66	0.000	0.01	-0.51	0.08	0.000
356	16.34	16.34	2.70	-1.46	0.26	-3.	0.74	-0.61	0.000	0.00	-0.47	0.07	0.000
358	16.34	16.34	4.39	0.23	0.02	13.	1.42	0.78	0.047	0.02	0.93	0.00	0.056
759	16.34	16.34	3.95	-1.29	0.26	-2.	1.26	-0.38	0.000	0.04	-0.27	0.04	0.000
761	16.34	16.34	3.03	-1.98	0.35	-4.	0.93	-0.93	0.000	0.01	-0.78	0.12	0.000

ARMATURA SUPERIORE ORIZZONTALE

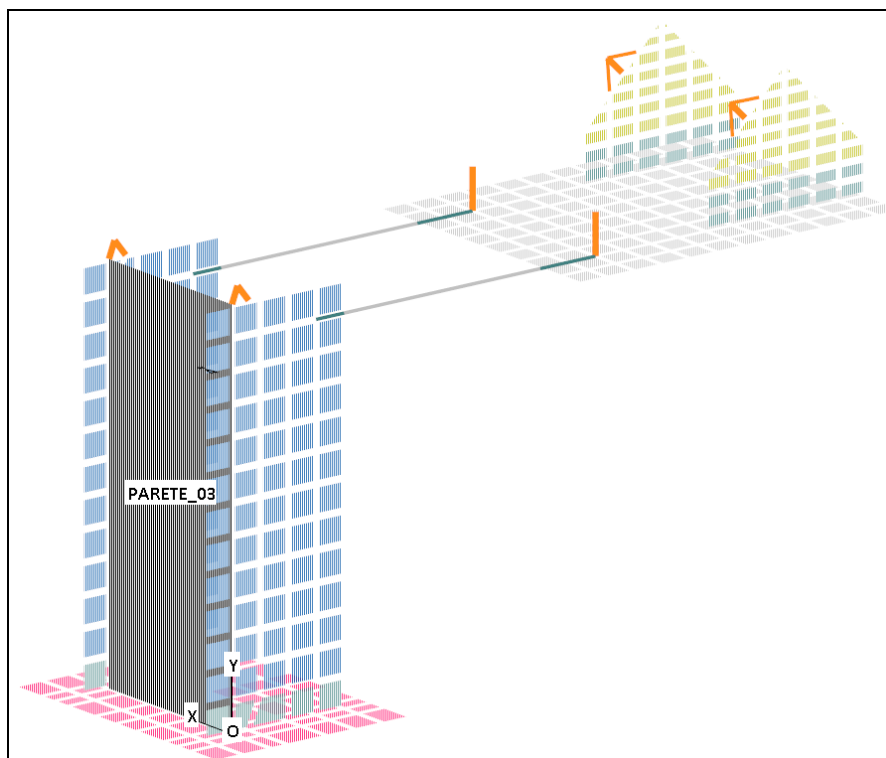
GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
169	16.38	16.38	8.99	4.46	0.00	148.	3.12	3.46	0.145	0.00	3.36	0.00	0.142
170	16.38	16.38	11.14	-0.25	0.31	7.	3.52	0.57	0.025	0.00	0.41	0.00	0.017
171	16.38	16.38	12.87	0.81	0.00	42.	4.77	0.83	0.036	0.00	0.64	0.00	0.027
172	10.21	10.21	13.77	0.36	0.39	46.	4.53	0.72	0.090	0.05	0.61	0.00	0.074
173	16.38	16.38	9.57	3.23	0.00	111.	3.32	2.86	0.121	0.00	2.79	0.00	0.118
174	16.38	16.38	11.48	-0.18	0.32	9.	3.62	0.35	0.016	0.00	0.21	0.00	0.009
175	16.38	16.38	13.05	0.22	0.32	23.	4.60	0.57	0.026	0.00	0.40	0.00	0.017
176	10.21	10.21	13.86	0.16	0.45	36.	4.34	0.44	0.058	0.00	0.33	0.00	0.040
177	10.21	10.21	10.38	1.46	0.00	94.	3.60	1.76	0.214	0.00	1.76	0.00	0.214
178	10.21	10.21	11.77	-1.42	0.05	-5.	3.67	-0.50	0.000	0.00	-0.70	0.11	0.000
179	10.21	10.21	13.05	-0.21	0.44	16.	4.41	0.14	0.025	0.00	-0.05	0.01	0.000
180	10.21	10.21	14.25	0.02	0.49	30.	4.50	0.27	0.040	0.00	0.13	0.00	0.015
181	10.21	10.21	11.80	-0.40	0.35	6.	4.09	-0.14	0.003	0.00	-0.10	0.02	0.000
182	10.21	10.21	12.25	-0.71	0.33	1.	3.89	-0.69	0.000	0.00	-0.62	0.10	0.000
183	10.21	10.21	13.27	-0.71	0.36	2.	4.28	-0.31	0.000	0.00	-0.50	0.08	0.000
184	10.21	10.21	14.28	-0.22	0.48	18.	4.38	-0.05	0.008	0.00	-0.11	0.02	0.000
185	10.21	10.21	12.06	-0.21	0.40	14.	4.11	-0.13	0.003	0.00	-0.10	0.02	0.000
186	10.21	10.21	12.47	-0.41	0.38	7.	4.04	-0.04	0.008	0.00	-0.18	0.03	0.000
187	10.21	10.21	13.39	-0.01	0.46	26.	4.13	-0.21	0.001	0.00	-0.13	0.02	0.000
188	10.21	10.21	14.21	-0.18	0.48	20.	4.24	-0.17	0.002	0.00	-0.04	0.01	0.000
189	10.21	10.21	11.99	-0.05	0.41	22.	3.99	-0.04	0.008	0.00	-0.03	0.00	0.000
190	10.21	10.21	12.32	-0.05	0.42	22.	3.93	-0.07	0.006	0.00	0.00	0.00	0.000
191	10.21	10.21	13.15	-0.07	0.45	23.	3.92	-0.10	0.004	0.00	0.00	0.00	0.000
192	10.21	10.21	14.04	-0.01	0.48	27.	4.32	-0.10	0.005	0.00	0.03	0.00	0.003
193	10.21	10.21	11.71	0.00	0.40	23.	3.88	-0.01	0.009	0.01	0.00	0.00	0.000
194	10.21	10.21	11.88	0.05	0.40	26.	3.73	-0.01	0.009	0.00	0.06	0.00	0.007
195	10.21	10.21	12.72	0.07	0.43	29.	3.69	-0.01	0.009	0.00	0.11	0.00	0.013
196	10.21	10.21	13.44	0.09	0.45	31.	4.35	-0.02	0.010	0.00	0.12	0.00	0.015
197	10.21	10.21	11.00	0.00	0.38	22.	3.60	-0.01	0.009	0.07	0.00	0.00	0.001
198	10.21	10.21	11.00	0.05	0.37	24.	3.43	-0.02	0.008	0.00	0.06	0.00	0.007
199	10.21	10.21	11.91	0.06	0.40	27.	3.48	0.00	0.009	0.00	0.11	0.00	0.014
200	10.21	10.21	12.50	0.05	0.42	27.	4.24	-0.01	0.010	0.00	0.12	0.00	0.015
201	10.21	10.21	9.54	-0.02	0.33	18.	3.08	-0.02	0.007	0.12	0.00	0.00	0.001
202	10.21	10.21	9.31	-0.01	0.32	18.	2.88	-0.04	0.005	0.10	0.04	0.00	0.005
203	10.21	10.21	10.34	-0.02	0.35	19.	3.03	-0.04	0.005	0.00	0.07	0.00	0.006
204	10.21	10.21	10.93	-0.10	0.37	17.	3.64	-0.06	0.006	0.00	0.05	0.00	0.009
205	10.21	10.21	7.08	-0.03	0.24	13.	1.97	-0.02	0.004	0.14	0.01	0.00	0.001
206	10.21	10.21	7.85	-0.04	0.27	14.	2.40	-0.06	0.003	0.15	0.03	0.00	0.004
207	10.21	10.21	8.83	-0.08	0.30	14.	2.60	-0.06	0.003	0.00	0.05	0.00	0.006
208	10.21	10.21	9.55	-0.17	0.32	11.	3.12	-0.08	0.003	0.00	0.01	0.00	0.001
209	10.21	10.21	4.78	-0.04	0.16	8.	1.28	-0.03	0.001	0.14	0.01	0.00	0.001
210	10.21	10.21	6.70	-0.09	0.23	9.	1.62	0.00	0.004	0.18	0.01	0.00	0.002
211	10.21	10.21	7.91	-0.14	0.27	9.	2.36	-0.10	0.001	0.00	0.02	0.00	0.002
212	10.21	10.21	8.53	-0.26	0.26	6.	2.72	-0.12	0.001	0.00	-0.03	0.01	0.000
213	10.21	10.21	2.64	-0.05	0.09	3.	0.65	-0.01	0.001	0.14	0.00	0.00	0.001
214	10.21	10.21	3.78	-0.14	0.11	2.	0.82	-0.06	0.000	0.21	-0.01	0.01	0.000
215	10.21	10.21	7.15	-0.23	0.22	4.	2.16	-0.14	0.000	0.00	-0.02	0.00	0.000
216	10.21	10.21	7.00	-0.30	0.20	2.	2.18	-0.12	0.000	0.00	-0.06	0.01	0.000
217	10.21	10.21	6.20	0.00	0.21	12.	2.18	0.01	0.007	0.20	0.01	0.01	0.001
218	10.21	10.21	7.19	-0.01	0.25	14.	2.53	0.00	0.007	0.17	-0.01	0.01	0.000
219	10.21	10.21	8.81	0.04	0.30	19.	3.07	0.02	0.010	0.16	0.01	0.00	0.001
220	10.21	10.21	10.59	-0.01	0.36	20.	3.68	-0.01	0.009	0.13	-0.01	0.00	0.000
221	10.21	10.21	11.61	-0.04	0.40	21.	4.03	-0.02	0.009	0.05	-0.02	0.00	0.000
222	10.21	10.21	12.17	-0.02	0.42	23.	4.21	-0.02	0.010	0.03	-0.01	0.00	0.000
223	10.21	10.21	12.40	-0.01	0.42	24.	4.26	-0.01	0.010	0.03	0.00	0.00	0.000
224	10.21	10.21	12.26	-0.01	0.42	24.	4.18	0.00	0.010	0.09	0.00	0.00	0.000
225	10.21	10.21	11.36	-0.03	0.39	21.	3.86	-0.01	0.009	0.22	-0.01	0.01	0.000

GUSCI				COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf		Mom	Nor	wkF	Mom	Nor	σc	wkP
226	10.21	10.21	10.10	-0.08	0.35	16.		3.44	-0.03	0.007	0.23	-0.03	0.00	0.000
227	10.21	10.21	9.51	-0.10	0.33	14.		3.24	-0.03	0.006	0.29	-0.04	0.00	0.000
228	10.21	10.21	8.58	-0.12	0.29	11.		2.92	-0.04	0.005	0.37	-0.05	0.00	0.000
354	16.38	16.38	8.18	6.41	0.00	206.		2.91	4.38	0.184	0.00	4.23	0.00	0.179
355	16.38	16.38	10.66	0.58	0.04	32.		3.27	1.03	0.044	0.00	0.89	0.00	0.038
356	16.38	16.38	12.68	1.48	0.00	62.		4.78	1.27	0.054	0.04	1.10	0.00	0.046
358	10.21	10.21	4.85	0.03	0.16	11.		1.69	0.03	0.007	0.18	0.02	0.00	0.003
759	10.21	10.21	11.89	0.40	0.29	44.		4.27	0.78	0.097	0.27	0.72	0.00	0.088
761	10.21	10.21	15.12	1.01	0.00	81.		5.72	1.13	0.140	0.30	1.00	0.00	0.122

ARMATURA SUPERIORE VERTICALE

GUSCI				COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf		Mom	Nor	wkF	Mom	Nor	σc	wkP
169	16.34	16.34	15.85	-1.64	0.02	-6.		5.31	-0.16	0.002	0.21	-0.05	0.01	0.000
170	16.34	16.34	14.92	-2.06	0.10	-7.		4.89	-0.25	0.001	0.34	-0.10	0.01	0.000
171	16.34	16.34	14.07	-1.93	0.09	-7.		4.55	-0.26	0.000	0.37	-0.12	0.01	0.000
172	16.34	16.34	12.51	1.09	0.00	50.		3.92	1.92	0.115	0.40	2.03	0.00	0.122
173	16.34	16.34	15.24	-2.19	0.12	-8.		5.06	-0.24	0.001	0.00	-0.11	0.02	0.000
174	16.34	16.34	14.56	-2.25	0.13	-8.		4.77	-0.37	0.000	0.04	-0.25	0.04	0.000
175	16.34	16.34	14.02	-2.12	0.12	-7.		4.55	-0.36	0.000	0.08	-0.25	0.04	0.000
176	16.34	16.34	13.40	-1.24	0.00	-5.		4.33	0.16	0.014	0.10	0.21	0.00	0.013
177	16.34	16.34	14.21	-2.47	0.17	-8.		4.54	-0.57	0.000	0.00	-0.44	0.07	0.000
178	16.34	16.34	13.69	-2.31	0.16	-8.		4.33	-0.55	0.000	0.00	-0.43	0.07	0.000
179	16.34	16.34	13.36	-2.16	0.14	-7.		4.24	-0.50	0.000	0.00	-0.37	0.06	0.000
180	16.34	16.34	13.06	-1.78	0.08	-6.		4.14	-0.31	0.000	0.00	-0.15	0.02	0.000
181	16.34	16.34	13.57	-2.66	0.21	-8.		4.34	-0.77	0.000	0.00	-0.65	0.10	0.000
182	16.34	16.34	13.21	-2.40	0.18	-8.		4.21	-0.66	0.000	0.00	-0.54	0.08	0.000
183	16.34	16.34	12.99	-2.23	0.15	-7.		4.17	-0.59	0.000	0.00	-0.46	0.07	0.000
184	16.34	16.34	12.81	-1.98	0.12	-7.		4.10	-0.47	0.000	0.00	-0.33	0.05	0.000
185	16.34	16.34	13.07	-2.67	0.22	-8.		4.15	-0.88	0.000	0.00	-0.71	0.11	0.000
186	16.34	16.34	12.88	-2.41	0.18	-8.		4.15	-0.76	0.000	0.00	-0.60	0.09	0.000
187	16.34	16.34	12.75	-2.26	0.16	-7.		4.14	-0.68	0.000	0.00	-0.52	0.08	0.000
188	16.34	16.34	12.66	-2.07	0.13	-7.		4.14	-0.58	0.000	0.00	-0.43	0.07	0.000
189	16.34	16.34	12.31	-2.55	0.21	-8.		4.03	-0.93	0.000	0.00	-0.70	0.11	0.000
190	16.34	16.34	12.33	-2.36	0.18	-8.		4.08	-0.82	0.000	0.00	-0.61	0.09	0.000
191	16.34	16.34	12.28	-2.26	0.17	-7.		4.08	-0.75	0.000	0.00	-0.57	0.09	0.000
192	16.34	16.34	12.31	-2.12	0.15	-7.		4.12	-0.68	0.000	0.00	-0.50	0.08	0.000
193	16.34	16.34	11.26	-2.36	0.20	-7.		3.68	-0.92	0.000	0.00	-0.65	0.10	0.000
194	16.34	16.34	11.47	-2.27	0.18	-7.		3.80	-0.84	0.000	0.00	-0.62	0.09	0.000
195	16.34	16.34	11.51	-2.23	0.18	-7.		3.83	-0.79	0.000	0.00	-0.60	0.09	0.000
196	16.34	16.34	11.61	-2.15	0.16	-7.		3.89	-0.74	0.000	0.00	-0.56	0.09	0.000
197	16.34	16.34	9.62	-2.16	0.19	-7.		3.09	-0.90	0.000	0.00	-0.60	0.09	0.000
198	16.34	16.34	10.04	-2.18	0.19	-7.		3.29	-0.85	0.000	0.00	-0.61	0.09	0.000
199	16.34	16.34	10.19	-2.21	0.19	-7.		3.36	-0.83	0.000	0.00	-0.63	0.10	0.000
200	16.34	16.34	10.36	-2.18	0.19	-7.		3.45	-0.79	0.000	0.00	-0.62	0.10	0.000
201	16.34	16.34	7.23	-2.06	0.21	-6.		2.18	-0.93	0.000	0.00	-0.56	0.09	0.000
202	16.34	16.34	7.89	-2.16	0.22	-6.		2.47	-0.90	0.000	0.00	-0.62	0.10	0.000
203	16.34	16.34	8.19	-2.25	0.23	-7.		2.60	-0.90	0.000	0.00	-0.67	0.10	0.000
204	16.34	16.34	8.46	-2.26	0.23	-7.		2.71	-0.87	0.000	0.00	-0.68	0.11	0.000
205	16.34	16.34	3.61	-2.06	0.26	-5.		0.74	-1.02	0.000	0.00	-0.53	0.08	0.000
206	16.34	16.34	4.68	-2.22	0.27	-6.		1.15	-1.00	0.000	0.00	-0.63	0.10	0.000
207	16.34	16.34	5.27	-2.37	0.29	-6.		1.37	-1.01	0.000	0.00	-0.72	0.11	0.000
208	16.34	16.34	5.77	-2.43	0.29	-7.		1.55	-0.99	0.000	0.00	-0.75	0.12	0.000
209	16.34	16.34	0.00	-2.05	0.32	-5.		0.00	-1.07	0.000	0.33	-0.54	0.08	0.000
210	16.34	16.34	0.45	-2.27	0.34	-5.		0.00	-1.06	0.000	0.23	-0.66	0.10	0.000
211	16.34	16.34	1.78	-2.52	0.36	-6.		0.00	-1.11	0.000	0.29	-0.80	0.12	0.000
212	16.34	16.34	2.94	-2.60	0.36	-6.		0.17	-1.08	0.000	0.24	-0.84	0.13	0.000
213	16.34	16.34	0.00	-2.12	0.33	-5.		0.00	-1.09	0.000	1.63	-0.57	0.06	0.000
214	16.34	16.34	0.00	-2.32	0.36	-5.		0.00	-1.07	0.000	1.61	-0.67	0.08	0.000
215	16.34	16.34	0.00	-2.72	0.42	-6.		0.00	-1.18	0.000	1.57	-0.88	0.11	0.000
216	16.34	16.34	1.98	-2.80	0.40	-7.		0.00	-1.10	0.000	1.61	-0.95	0.12	0.000
217	16.34	16.34	11.49	0.34	0.23	25.		3.51	1.11	0.067	0.50	1.23	0.00	0.074
218	16.34	16.34	12.58	-0.55	0.32	3.		3.94	0.60	0.037	0.17	0.55	0.00	0.033
219	16.34	16.34	12.51	-1.42	0.04	-5.		3.92	-0.05	0.004	0.00	0.00	0.00	0.000
220	16.34	16.34	12.48	-1.56	0.06	-6.		3.99	-0.27	0.096	0.00	-0.12	0.02	0.000
221	16.34	16.34	12.52	-1.72	0.08	-6.		4.12	-0.40	0.000	0.00	-0.26	0.04	0.000
222	16.34	16.34	12.38	-1.88	0.11	-6.		4.18	-0.54	0.000	0.00	-0.38	0.06	0.000
223	16.34	16.34	11.84	-2.01	0.14	-7.		4.02	-0.64	0.000	0.00	-0.49	0.08	0.000
224	16.34	16.34	10.74	-2.15	0.17	-7.		3.63	-0.73	0.000	0.00	-0.60	0.09	0.000
225	16.34	16.34	9.03	-2.31	0.22	-7.		2.95	-0.82	0.000	0.00	-0.71	0.11	0.000
226	16.34	16.34	6.78	-2.54	0.29	-7.		1.93	-0.95	0.000	0.00	-0.82	0.13	0.000
227	16.34	16.34	5.33	-2.76	0.35	-7.		0.95	-1.04	0.000	0.15	-0.93	0.14	0.000
228	16.34	16.34	7.82	-3.00	0.35	-8.		1.08	-1.07	0.000	1.71	-1.06	0.14	0.000
354	16.34	16.34	8.62	-0.81	0.00	-3.		2.80	-0.45	0.000	0.34	-0.29	0.04	0.000
355	16.34	16.34	8.13	-1.59	0.13	-5.		2.63	-0.66	0.000	0.37	-0.51	0.07	0.000
356	16.34	16.34	7.43	-1.46	0.12	-5.		2.39	-0.61	0.000	0.35	-0.47	0.07	0.000
358	16.34	16.34	7.95	0.23	0.16	17.		2.57	0.78	0.047	0.44	0.93	0.00	0.056
759	16.34	16.34	7.58	-1.29	0.09	-4.		2.44	-0.38	0.000	0.37	-0.27	0.04	0.000
761	16.34	16.34	7.69	-1.98	0.19	-6.		2.50	-0.93	0.000	0.37	-0.78	0.11	0.000

6.5. PARETE 03



G365	G366	G367	G368	G369	G762
G371	G372	G373	G374	G375	G376
G377	G378	G379	G380	G381	G382
G383	G384	G385	G386	G387	G388
G389	G390	G391	G392	G393	G394
G395	G396	G397	G398	G399	G400
G401	G402	G403	G404	G405	G406
G407	G408	G409	G410	G411	G412
G413	G414	G415	G416	G417	G418
G419	G420	G421	G422	G423	G424
G425	G426	G427	G428	G429	G430
G431	G432	G433	G434	G435	G436
G437	G438	G439	G440	G441	G442

6.5.1. Verifica SLU

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
365	0.6	10.21	10.21	18.	0.	0.00	0.27	16.83	16.83	72.	-2.	0.13	0.36	
366	0.6	10.21	10.21	6.	1.	0.00	0.19	16.83	16.83	57.	-2.	0.11	0.28	
367	0.6	10.21	10.21	3.	0.	0.00	0.12	16.83	16.83	44.	-2.	0.09	0.20	
368	0.6	10.21	10.21	1.	0.	0.00	0.10	16.83	16.83	33.	-2.	0.07	0.14	
369	0.6	10.21	10.21	2.	1.	0.00	0.15	16.83	16.83	14.	-2.	0.04	0.06	
371	0.6	10.21	10.21	18.	0.	0.00	0.27	16.83	16.83	15.	-2.	0.04	0.06	
372	0.6	10.21	10.21	5.	0.	0.00	0.16	16.83	16.83	13.	-2.	0.04	0.06	
373	0.6	10.21	10.21	2.	0.	0.00	0.09	16.83	16.83	14.	-2.	0.04	0.06	
374	0.6	10.21	10.21	2.	0.	0.00	0.07	16.83	16.83	14.	-2.	0.04	0.06	
375	0.6	10.21	10.21	1.	0.	0.00	0.12	16.83	16.83	13.	-2.	0.04	0.05	
376	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	14.	-2.	0.04	0.06	
377	0.6	10.21	10.21	17.	0.	0.00	0.25	16.83	16.83	12.	-2.	0.04	0.05	
378	0.6	10.21	10.21	4.	0.	0.00	0.13	16.83	16.83	12.	-2.	0.04	0.04	
379	0.6	10.21	10.21	1.	0.	0.00	0.07	16.83	16.83	13.	-2.	0.04	0.05	
380	0.6	10.21	10.21	2.	0.	0.00	0.06	16.83	16.83	13.	-2.	0.04	0.05	
381	0.6	10.21	10.21	1.	0.	0.00	0.10	16.83	16.83	14.	-2.	0.04	0.05	
382	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	14.	-2.	0.04	0.06	
383	0.6	10.21	10.21	14.	0.	0.00	0.20	16.83	16.83	12.	-2.	0.04	0.05	
384	0.6	10.21	10.21	2.	0.	0.00	0.09	16.83	16.83	12.	-2.	0.04	0.04	
385	0.6	10.21	10.21	0.	0.	0.00	0.05	16.83	16.83	13.	-2.	0.04	0.04	
386	0.6	10.21	10.21	1.	0.	0.00	0.05	16.83	16.83	13.	-2.	0.04	0.04	
387	0.6	10.21	10.21	1.	0.	0.00	0.08	16.83	16.83	12.	-2.	0.04	0.05	
388	0.6	10.21	10.21	1.	0.	0.00	0.05	16.83	16.83	12.	-2.	0.04	0.05	
389	0.6	10.21	10.21	10.	0.	0.00	0.14	16.83	16.83	11.	-2.	0.04	0.04	
390	0.6	10.21	10.21	1.	0.	0.00	0.04	16.83	16.83	11.	-2.	0.04	0.04	
391	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	11.	-3.	0.04	0.03	
392	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	11.	-3.	0.04	0.03	
393	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	11.	-2.	0.04	0.04	
394	0.6	10.21	10.21	1.	0.	0.00	0.05	16.83	16.83	11.	-2.	0.04	0.04	
395	0.6	10.21	10.21	10.	0.	0.00	0.13	16.83	16.83	10.	-3.	0.04	0.03	
396	0.6	10.21	10.21	0.	0.	0.00	0.03	16.83	16.83	13.	-3.	0.04	0.04	
397	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	12.	-3.	0.04	0.04	
398	0.6	10.21	10.21	0.	0.	0.00	0.01	16.83	16.83	12.	-3.	0.04	0.04	
399	0.6	10.21	10.21	0.	0.	0.00	0.03	16.83	16.83	13.	-3.	0.04	0.04	
400	0.6	10.21	10.21	1.	0.	0.00	0.04	16.83	16.83	15.	-3.	0.05	0.05	
401	0.6	10.21	10.21	10.	0.	0.00	0.13	16.83	16.83	21.	-3.	0.06	0.08	
402	0.6	10.21	10.21	0.	0.	0.00	0.01	16.83	16.83	22.	-3.	0.06	0.08	
403	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	22.	-3.	0.06	0.08	
404	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	23.	-3.	0.06	0.08	
405	0.6	10.21	10.21	0.	0.	0.00	0.01	16.83	16.83	25.	-3.	0.07	0.09	
406	0.6	10.21	10.21	1.	0.	0.00	0.04	16.83	16.83	25.	-3.	0.07	0.09	
407	0.6	10.21	10.21	5.	0.	0.00	0.07	16.83	16.83	21.	-3.	0.06	0.07	
408	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	21.	-3.	0.06	0.07	
409	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	21.	-3.	0.06	0.07	
410	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	21.	-3.	0.06	0.07	
411	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	22.	-3.	0.06	0.07	
412	0.6	10.21	10.21	2.	0.	0.00	0.03	16.83	16.83	22.	-4.	0.06	0.08	
413	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	16.	-4.	0.06	0.05	
414	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	17.	-4.	0.06	0.05	
415	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	17.	-4.	0.06	0.05	
416	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	18.	-4.	0.06	0.05	
417	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	19.	-4.	0.06	0.05	
418	0.6	10.21	10.21	3.	0.	0.01	0.02	16.83	16.83	19.	-4.	0.06	0.06	
419	0.6	10.21	10.21	4.	0.	0.01	0.03	16.83	16.83	11.	-4.	0.05	0.02	
420	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	12.	-4.	0.05	0.02	
421	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	13.	-4.	0.05	0.03	
422	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	13.	-4.	0.05	0.03	
423	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	14.	-4.	0.06	0.03	
424	0.6	10.21	10.21	3.	0.	0.01	0.02	16.83	16.83	15.	-4.	0.06	0.04	
425	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	5.	-4.	0.04	-0.03	
426	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	6.	-4.	0.04	-0.03	
427	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	7.	-4.	0.05	-0.02	
428	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	7.	-4.	0.05	-0.02	
429	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	8.	-4.	0.05	-0.02	
430	0.6	10.21	10.21	3.	0.	0.01	0.02	16.83	16.83	9.	-4.	0.05	-0.01	
431	0.6	10.21	10.21	4.	0.	0.01	0.04	16.83	16.83	0.	-5.	0.04	-0.04	
432	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
433	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
434	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
435	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.03	-0.03	
436	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	0.	-4.	0.03	-0.03	
437	0.6	10.21	10.21	5.	0.	0.01	0.04	16.83	16.83	0.	-4.	0.04	-0.04	
438	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
439	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
440	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.04	-0.04	
441	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	0.	-4.	0.03	-0.03	
442	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	0.	-4.	0.03	-0.03	
762	0.6	10.21	10.21	0.	0.	0.00	0.05	16.83	16.83	14.	-2.	0.04	0.06	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
365	0.6	10.21	10.21	0.	1.	0.00	0.12	16.83	16.83	0.	-2.	0.02	-0.02	
366	0.6	10.21	10.21	0.	1.	0.00	0.14	16.83	16.83	0.	-2.	0.02	-0.02	
367	0.6	10.21	10.21	0.	0.	0.00	0.09	16.83	16.83	0.	-2.	0.02	-0.02	

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
368	0.6	10.21	10.21	0.	0.	0.00	0.09	16.83	16.83	0.	-2.	0.02	-0.02	
369	0.6	10.21	10.21	3.	1.	0.00	0.16	16.83	16.83	2.	-2.	0.02	-0.02	
371	0.6	10.21	10.21	0.	0.	0.00	0.10	16.83	16.83	1.	-2.	0.02	-0.01	
372	0.6	10.21	10.21	0.	0.	0.00	0.11	16.83	16.83	1.	-2.	0.02	-0.02	
373	0.6	10.21	10.21	0.	0.	0.00	0.07	16.83	16.83	3.	-2.	0.02	-0.02	
374	0.6	10.21	10.21	0.	0.	0.00	0.07	16.83	16.83	3.	-2.	0.02	-0.02	
375	0.6	10.21	10.21	2.	0.	0.00	0.12	16.83	16.83	4.	-2.	0.02	-0.01	
376	0.6	10.21	10.21	4.	0.	0.00	0.07	16.83	16.83	5.	-2.	0.02	0.01	
377	0.6	10.21	10.21	0.	0.	0.00	0.09	16.83	16.83	5.	-2.	0.02	0.01	
378	0.6	10.21	10.21	0.	0.	0.00	0.10	16.83	16.83	7.	-2.	0.03	0.02	
379	0.6	10.21	10.21	0.	0.	0.00	0.06	16.83	16.83	7.	-2.	0.03	0.02	
380	0.6	10.21	10.21	0.	0.	0.00	0.06	16.83	16.83	8.	-2.	0.03	0.02	
381	0.6	10.21	10.21	1.	0.	0.00	0.10	16.83	16.83	9.	-2.	0.03	0.03	
382	0.6	10.21	10.21	2.	0.	0.00	0.06	16.83	16.83	9.	-2.	0.03	0.03	
383	0.6	10.21	10.21	0.	0.	0.00	0.07	16.83	16.83	7.	-2.	0.03	0.02	
384	0.6	10.21	10.21	0.	0.	0.00	0.07	16.83	16.83	7.	-2.	0.03	0.02	
385	0.6	10.21	10.21	0.	0.	0.00	0.05	16.83	16.83	7.	-2.	0.03	0.02	
386	0.6	10.21	10.21	0.	0.	0.00	0.05	16.83	16.83	8.	-2.	0.03	0.02	
387	0.6	10.21	10.21	1.	0.	0.00	0.08	16.83	16.83	8.	-2.	0.03	0.02	
388	0.6	10.21	10.21	1.	0.	0.00	0.04	16.83	16.83	8.	-2.	0.03	0.03	
389	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	10.	-2.	0.04	0.03	
390	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	10.	-2.	0.04	0.03	
391	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	10.	-3.	0.04	0.03	
392	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	10.	-2.	0.04	0.03	
393	0.6	10.21	10.21	1.	0.	0.00	0.04	16.83	16.83	10.	-2.	0.04	0.03	
394	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	10.	-2.	0.03	0.03	
395	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	14.	-3.	0.04	0.05	
396	0.6	10.21	10.21	0.	0.	0.00	0.03	16.83	16.83	13.	-3.	0.04	0.04	
397	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	13.	-3.	0.04	0.04	
398	0.6	10.21	10.21	2.	0.	0.00	0.02	16.83	16.83	13.	-3.	0.04	0.04	
399	0.6	10.21	10.21	1.	0.	0.00	0.03	16.83	16.83	13.	-3.	0.04	0.04	
400	0.6	10.21	10.21	0.	0.	0.00	0.03	16.83	16.83	13.	-3.	0.04	0.04	
401	0.6	10.21	10.21	0.	0.	0.00	0.04	16.83	16.83	17.	-3.	0.05	0.06	
402	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	16.	-3.	0.05	0.06	
403	0.6	10.21	10.21	2.	0.	0.00	0.02	16.83	16.83	16.	-3.	0.05	0.05	
404	0.6	10.21	10.21	2.	0.	0.01	0.02	16.83	16.83	16.	-3.	0.05	0.05	
405	0.6	10.21	10.21	1.	0.	0.00	0.02	16.83	16.83	16.	-3.	0.05	0.05	
406	0.6	10.21	10.21	0.	0.	0.00	0.03	16.83	16.83	15.	-3.	0.05	0.05	
407	0.6	10.21	10.21	0.	0.	0.00	0.02	16.83	16.83	19.	-3.	0.06	0.06	
408	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	19.	-3.	0.06	0.06	
409	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	18.	-3.	0.06	0.06	
410	0.6	10.21	10.21	4.	0.	0.01	0.03	16.83	16.83	18.	-3.	0.06	0.06	
411	0.6	10.21	10.21	2.	0.	0.01	0.02	16.83	16.83	18.	-3.	0.06	0.06	
412	0.6	10.21	10.21	0.	0.	0.00	0.02	16.83	16.83	18.	-4.	0.06	0.05	
413	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	21.	-4.	0.06	0.07	
414	0.6	10.21	10.21	2.	0.	0.01	0.02	16.83	16.83	21.	-4.	0.06	0.07	
415	0.6	10.21	10.21	4.	0.	0.01	0.04	16.83	16.83	21.	-4.	0.06	0.06	
416	0.6	10.21	10.21	5.	0.	0.01	0.04	16.83	16.83	20.	-4.	0.06	0.06	
417	0.6	10.21	10.21	3.	0.	0.01	0.03	16.83	16.83	20.	-4.	0.06	0.06	
418	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	20.	-4.	0.06	0.06	
419	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	24.	-4.	0.07	0.07	
420	0.6	10.21	10.21	4.	0.	0.01	0.03	16.83	16.83	23.	-4.	0.07	0.07	
421	0.6	10.21	10.21	6.	0.	0.01	0.05	16.83	16.83	23.	-4.	0.07	0.07	
422	0.6	10.21	10.21	6.	0.	0.02	0.05	16.83	16.83	23.	-4.	0.07	0.07	
423	0.6	10.21	10.21	4.	0.	0.01	0.04	16.83	16.83	23.	-4.	0.07	0.07	
424	0.6	10.21	10.21	1.	0.	0.00	0.00	16.83	16.83	23.	-4.	0.07	0.07	
425	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	29.	-4.	0.08	0.09	
426	0.6	10.21	10.21	5.	0.	0.01	0.04	16.83	16.83	29.	-4.	0.08	0.09	
427	0.6	10.21	10.21	6.	0.	0.02	0.06	16.83	16.83	28.	-4.	0.08	0.09	
428	0.6	10.21	10.21	7.	0.	0.02	0.06	16.83	16.83	27.	-4.	0.08	0.09	
429	0.6	10.21	10.21	5.	0.	0.01	0.04	16.83	16.83	27.	-4.	0.08	0.09	
430	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	27.	-4.	0.08	0.09	
431	0.6	10.21	10.21	0.	0.	0.00	0.00	16.83	16.83	31.	-5.	0.09	0.10	
432	0.6	10.21	10.21	5.	0.	0.01	0.05	16.83	16.83	32.	-4.	0.09	0.10	
433	0.6	10.21	10.21	7.	0.	0.02	0.06	16.83	16.83	31.	-4.	0.09	0.10	
434	0.6	10.21	10.21	8.	0.	0.02	0.06	16.83	16.83	30.	-4.	0.08	0.10	
435	0.6	10.21	10.21	5.	0.	0.02	0.04	16.83	16.83	29.	-4.	0.08	0.10	
436	0.6	10.21	10.21	1.	0.	0.00	0.01	16.83	16.83	29.	-4.	0.08	0.10	
437	0.6	10.21	10.21	1.	0.	0.00	0.00	16.83	16.83	44.	-4.	0.11	0.16	
438	0.6	10.21	10.21	6.	0.	0.02	0.05	16.83	16.83	40.	-4.	0.10	0.14	
439	0.6	10.21	10.21	9.	0.	0.02	0.07	16.83	16.83	38.	-4.	0.10	0.13	
440	0.6	10.21	10.21	9.	0.	0.02	0.07	16.83	16.83	36.	-4.	0.09	0.13	
441	0.6	10.21	10.21	7.	0.	0.02	0.05	16.83	16.83	34.	-4.	0.09	0.12	
442	0.6	10.21	10.21	1.	0.	0.01	0.01	16.83	16.83	32.	-4.	0.09	0.11	
762	0.6	10.21	10.21	6.	0.	0.00	0.10	16.83	16.83	5.	-2.	0.02	0.01	

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO (Rd > Ed)

6.5.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE													
			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkf	Mom	Nor	σc	wkP
365	10.21	10.21	13.22	0.20	0.42	36.	5.29	-0.01	0.013	4.73	0.01	0.16	0.013

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
366	10.21	10.21	17.13	0.19	0.56	43.	5.38	0.03	0.016	1.23	0.00	0.04	0.003
367	10.21	10.21	14.43	0.06	0.49	32.	5.17	-0.06	0.009	0.75	-0.01	0.02	0.001
368	10.21	10.21	11.42	-0.04	0.39	21.	3.87	-0.04	0.007	0.31	-0.01	0.01	0.000
369	10.21	10.21	7.57	0.03	0.26	17.	2.16	-0.04	0.003	0.28	0.00	0.01	0.001
371	10.21	10.21	13.84	0.19	0.45	37.	3.94	-0.01	0.009	3.89	0.01	0.13	0.011
372	10.21	10.21	17.14	0.16	0.57	42.	5.50	0.04	0.017	0.99	0.01	0.03	0.004
373	10.21	10.21	14.52	0.05	0.49	31.	5.11	-0.04	0.011	0.52	0.01	0.02	0.002
374	10.21	10.21	11.64	-0.01	0.40	23.	3.93	-0.01	0.010	0.15	0.01	0.00	0.001
375	10.21	10.21	8.15	0.02	0.28	17.	2.42	-0.04	0.004	0.22	0.01	0.00	0.002
376	10.21	10.21	3.20	-0.06	0.11	4.	0.16	0.00	0.000	0.20	0.02	0.00	0.002
377	10.21	10.21	14.69	0.19	0.48	39.	4.46	-0.01	0.011	3.28	0.01	0.11	0.009
378	10.21	10.21	17.06	0.15	0.57	42.	5.56	0.04	0.018	0.79	0.02	0.02	0.004
379	10.21	10.21	14.53	0.05	0.49	31.	4.85	-0.01	0.012	0.36	0.02	0.00	0.003
380	10.21	10.21	11.79	-0.02	0.40	23.	3.96	-0.02	0.009	0.07	0.02	0.00	0.003
381	10.21	10.21	8.62	0.02	0.29	18.	2.61	-0.02	0.006	0.14	0.02	0.00	0.003
382	10.21	10.21	4.38	-0.01	0.15	8.	0.71	0.00	0.002	0.23	0.01	0.00	0.002
383	10.21	10.21	19.73	0.16	0.66	47.	7.01	0.01	0.019	1.15	0.03	0.03	0.006
384	10.21	10.21	16.81	0.18	0.55	42.	5.92	0.03	0.018	0.24	0.02	0.00	0.003
385	10.21	10.21	14.32	0.00	0.49	29.	4.65	0.01	0.013	0.09	0.02	0.00	0.002
386	10.21	10.21	11.87	-0.03	0.41	22.	4.01	-0.01	0.010	0.00	0.02	0.00	0.002
387	10.21	10.21	9.18	0.00	0.31	18.	2.90	0.00	0.007	0.09	0.03	0.00	0.004
388	10.21	10.21	6.18	0.02	0.21	13.	1.59	0.02	0.006	0.37	0.02	0.00	0.004
389	10.21	10.21	18.55	0.16	0.62	45.	6.60	0.02	0.019	0.51	0.02	0.01	0.003
390	10.21	10.21	16.87	0.15	0.56	41.	5.93	0.05	0.020	0.15	0.04	0.00	0.005
391	10.21	10.21	14.29	0.03	0.49	30.	4.58	0.05	0.016	0.00	0.04	0.00	0.005
392	10.21	10.21	12.07	-0.04	0.41	22.	4.08	0.03	0.013	0.00	0.04	0.00	0.005
393	10.21	10.21	10.00	0.01	0.34	20.	3.27	0.03	0.011	0.05	0.04	0.00	0.005
394	10.21	10.21	8.20	0.01	0.28	17.	2.54	0.02	0.008	0.48	0.02	0.01	0.003
395	10.21	10.21	17.68	0.18	0.58	44.	6.30	0.04	0.020	0.55	0.02	0.01	0.004
396	10.21	10.21	15.84	0.12	0.53	38.	5.51	0.06	0.019	0.06	0.05	0.00	0.006
397	10.21	10.21	13.67	0.05	0.46	30.	4.31	0.06	0.017	0.00	0.05	0.00	0.006
398	10.21	10.21	11.95	0.01	0.41	24.	4.01	0.05	0.015	0.00	0.05	0.00	0.006
399	10.21	10.21	10.55	0.02	0.36	22.	3.47	0.04	0.013	0.00	0.05	0.00	0.006
400	10.21	10.21	9.62	0.02	0.33	20.	3.14	0.02	0.010	0.49	0.02	0.01	0.004
401	10.21	10.21	16.97	0.16	0.56	42.	6.05	0.05	0.020	0.53	0.03	0.01	0.004
402	10.21	10.21	14.65	0.07	0.49	33.	5.08	0.05	0.017	0.00	0.04	0.00	0.005
403	10.21	10.21	12.65	0.02	0.43	26.	3.92	0.06	0.016	0.00	0.05	0.00	0.006
404	10.21	10.21	11.40	0.00	0.39	23.	3.78	0.05	0.014	0.00	0.04	0.00	0.005
405	10.21	10.21	10.65	0.01	0.36	22.	3.50	0.04	0.013	0.00	0.04	0.00	0.005
406	10.21	10.21	10.43	0.03	0.35	22.	3.45	0.02	0.011	0.46	0.03	0.00	0.004
407	10.21	10.21	16.22	0.09	0.55	37.	5.76	0.04	0.018	0.58	0.02	0.01	0.004
408	10.21	10.21	13.24	-0.01	0.45	26.	4.56	0.03	0.014	0.00	0.02	0.00	0.003
409	10.21	10.21	11.25	-0.05	0.39	20.	3.41	0.04	0.012	0.00	0.02	0.00	0.003
410	10.21	10.21	10.38	-0.05	0.36	18.	3.40	0.03	0.011	0.00	0.02	0.00	0.003
411	10.21	10.21	10.25	-0.01	0.35	20.	3.35	0.03	0.011	0.00	0.02	0.00	0.002
412	10.21	10.21	10.80	0.02	0.37	22.	3.59	0.02	0.011	0.49	0.02	0.01	0.004
413	10.21	10.21	15.59	-0.02	0.53	30.	5.51	0.01	0.015	0.66	0.00	0.02	0.002
414	10.21	10.21	11.45	-0.12	0.39	17.	3.85	-0.01	0.009	0.00	-0.01	0.00	0.000
415	10.21	10.21	9.39	-0.14	0.32	12.	2.86	0.00	0.007	0.00	-0.01	0.00	0.000
416	10.21	10.21	8.76	-0.01	0.30	17.	2.76	0.00	0.007	0.00	-0.01	0.00	0.000
417	10.21	10.21	9.08	-0.09	0.31	14.	2.86	0.00	0.007	0.00	-0.01	0.00	0.000
418	10.21	10.21	10.55	-0.03	0.36	19.	3.51	0.01	0.009	0.55	0.00	0.02	0.002
419	10.21	10.21	14.66	-0.14	0.50	22.	5.16	-0.02	0.012	0.45	-0.03	0.01	0.000
420	10.21	10.21	9.47	-0.22	0.31	9.	3.10	-0.04	0.005	0.00	-0.04	0.01	0.000
421	10.21	10.21	7.38	-0.24	0.23	4.	2.24	-0.04	0.003	0.00	-0.02	0.00	0.000
422	10.21	10.21	6.73	-0.08	0.23	10.	1.97	-0.04	0.003	0.00	-0.03	0.00	0.000
423	10.21	10.21	7.16	-0.14	0.24	8.	1.65	-0.03	0.002	0.00	-0.04	0.01	0.000
424	10.21	10.21	9.18	-0.09	0.31	14.	2.78	-0.02	0.006	0.40	-0.03	0.01	0.000
425	10.21	10.21	11.12	-0.22	0.37	12.	4.23	-0.05	0.008	0.33	-0.05	0.01	0.000
426	10.21	10.21	6.33	-0.29	0.18	2.	2.18	-0.07	0.002	0.00	-0.01	0.00	0.000
427	10.21	10.21	5.17	-0.05	0.18	8.	1.58	-0.07	0.000	0.00	-0.05	0.01	0.000
428	10.21	10.21	5.29	-0.12	0.17	5.	1.42	-0.01	0.003	0.00	-0.06	0.01	0.000
429	10.21	10.21	5.94	-0.15	0.19	5.	0.66	-0.05	0.000	0.00	-0.01	0.00	0.000
430	10.21	10.21	8.25	-0.16	0.27	9.	2.27	-0.01	0.005	0.27	-0.05	0.01	0.000
431	10.21	10.21	9.32	-0.28	0.29	6.	3.48	-0.07	0.005	0.37	-0.07	0.02	0.000
432	10.21	10.21	3.57	-0.01	0.12	7.	1.06	-0.09	0.000	0.00	-0.03	0.00	0.000
433	10.21	10.21	1.95	-0.10	0.05	0.	0.29	-0.10	0.000	0.00	-0.07	0.01	0.000
434	10.21	10.21	1.93	-0.15	0.05	0.	0.17	-0.03	0.000	0.00	-0.08	0.01	0.000
435	10.21	10.21	3.89	-0.17	0.11	1.	0.00	-0.07	0.000	0.00	-0.03	0.00	0.000
436	10.21	10.21	7.60	-0.15	0.25	8.	1.21	-0.03	0.001	0.30	-0.07	0.02	0.000
437	10.21	10.21	7.98	-0.33	0.23	3.	2.98	-0.08	0.003	0.57	-0.02	0.02	0.001
438	10.21	10.21	1.26	-0.07	0.03	0.	0.18	-0.11	0.000	0.00	-0.05	0.01	0.000
439	10.21	10.21	0.00	-0.14	0.02	0.	0.00	-0.02	0.000	0.00	-0.10	0.02	0.000
440	10.21	10.21	0.00	-0.18	0.03	0.	0.00	-0.05	0.000	0.00	-0.10	0.02	0.000
441	10.21	10.21	0.68	-0.19	0.04	0.	0.00	-0.10	0.000	0.00	-0.06	0.01	0.000
442	10.21	10.21	5.21	-0.13	0.17	5.	0.55	-0.05	0.000	0.47	-0.02	0.01	0.000
762	10.21	10.21	1.57	-0.05	0.05	1.	0.00	-0.01	0.000	0.01	0.02	0.00	0.002

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
365	16.83	16.83	34.96	-1.04	0.93	16.	10.74	-0.42	0.003	11.04	-0.47	0.28	0.003
366	16.83	16.83	30.64	-1.09	0.80	11.	9.31	-0.39	0.002	8.85	-0.43	0.22	0.001
367	16.83	16.83	27.64	-1.46	0.69	3.	8.08	-0.47	0.001	7.16	-0.50	0.19	0.000
368	16.83	16.83	19.90	-1.42	0.52	0.	5.02	-0.45	0.000	4.39	-0.46	0.13	0.000
369	16.83	16.83	13.69	-1.20	0.38	0.	2.87	-0.35	0.000	1.48	-0.35	0.07	0.000

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
371	16.83	16.83	22.96	-1.11	0.58	4.	7.10	-0.39	0.001	2.19	-0.43	0.10	0.000
372	16.83	16.83	21.96	-1.22	0.55	2.	6.75	-0.39	0.001	2.05	-0.39	0.09	0.000
373	16.83	16.83	20.91	-1.43	0.54	1.	6.27	-0.41	0.000	1.89	-0.43	0.09	0.000
374	16.83	16.83	20.36	-1.44	0.53	0.	6.07	-0.40	0.000	1.84	-0.42	0.09	0.000
375	16.83	16.83	19.17	-1.32	0.49	1.	5.71	-0.34	0.000	1.66	-0.34	0.08	0.000
376	16.83	16.83	18.04	-1.48	0.49	0.	5.24	-0.36	0.000	1.46	-0.37	0.08	0.000
377	16.83	16.83	22.21	-1.18	0.56	3.	7.20	-0.38	0.001	2.94	-0.36	0.10	0.000
378	16.83	16.83	21.90	-1.29	0.55	2.	7.18	-0.38	0.001	2.78	-0.36	0.10	0.000
379	16.83	16.83	21.36	-1.39	0.54	1.	7.04	-0.37	0.001	2.61	-0.38	0.10	0.000
380	16.83	16.83	21.15	-1.42	0.54	1.	7.00	-0.36	0.001	2.67	-0.38	0.10	0.000
381	16.83	16.83	21.04	-1.43	0.54	1.	7.07	-0.34	0.001	2.91	-0.34	0.09	0.000
382	16.83	16.83	20.51	-1.53	0.54	0.	6.95	-0.33	0.001	3.05	-0.33	0.09	0.000
383	16.83	16.83	23.35	-1.31	0.58	2.	8.43	-0.39	0.002	3.98	-0.39	0.12	0.000
384	16.83	16.83	23.04	-1.41	0.58	1.	8.39	-0.39	0.002	3.81	-0.40	0.12	0.000
385	16.83	16.83	22.67	-1.48	0.58	1.	8.36	-0.37	0.002	3.84	-0.39	0.12	0.000
386	16.83	16.83	22.42	-1.53	0.58	1.	8.35	-0.36	0.002	3.85	-0.39	0.12	0.000
387	16.83	16.83	22.12	-1.61	0.58	0.	8.31	-0.36	0.002	3.86	-0.39	0.12	0.000
388	16.83	16.83	21.82	-1.68	0.57	0.	8.31	-0.35	0.002	4.06	-0.37	0.12	0.000
389	16.83	16.83	22.48	-1.51	0.58	1.	8.66	-0.43	0.001	3.95	-0.46	0.13	0.000
390	16.83	16.83	22.22	-1.61	0.58	0.	8.59	-0.44	0.001	3.93	-0.47	0.13	0.000
391	16.83	16.83	21.92	-1.67	0.57	0.	8.55	-0.43	0.001	4.00	-0.46	0.13	0.000
392	16.83	16.83	21.74	-1.72	0.58	0.	8.53	-0.43	0.001	4.01	-0.46	0.13	0.000
393	16.83	16.83	21.48	-1.83	0.59	-1.	8.45	-0.45	0.001	3.96	-0.47	0.13	0.000
394	16.83	16.83	21.21	-1.90	0.60	-1.	8.40	-0.44	0.001	3.99	-0.46	0.13	0.000
395	16.83	16.83	19.98	-1.76	0.56	-1.	7.91	-0.50	0.000	3.30	-0.53	0.13	0.000
396	16.83	16.83	19.89	-1.85	0.57	-1.	7.87	-0.52	0.000	3.29	-0.55	0.13	0.000
397	16.83	16.83	19.70	-1.91	0.58	-1.	7.82	-0.52	0.000	3.32	-0.55	0.13	0.000
398	16.83	16.83	19.64	-1.96	0.59	-1.	7.80	-0.53	0.000	3.32	-0.55	0.13	0.000
399	16.83	16.83	19.57	-2.07	0.60	-2.	7.76	-0.55	0.000	3.33	-0.55	0.13	0.000
400	16.83	16.83	19.43	-2.12	0.61	-2.	7.72	-0.56	0.000	3.38	-0.53	0.13	0.000
401	16.83	16.83	16.79	-2.04	0.56	-2.	6.74	-0.61	0.000	2.32	-0.63	0.13	0.000
402	16.83	16.83	16.93	-2.12	0.57	-2.	6.79	-0.63	0.000	2.33	-0.65	0.13	0.000
403	16.83	16.83	16.92	-2.19	0.58	-2.	6.77	-0.63	0.000	2.32	-0.67	0.14	0.000
404	16.83	16.83	16.96	-2.23	0.59	-2.	6.78	-0.64	0.000	2.33	-0.67	0.14	0.000
405	16.83	16.83	17.12	-2.33	0.61	-3.	6.83	-0.67	0.000	2.36	-0.66	0.14	0.000
406	16.83	16.83	17.20	-2.34	0.61	-3.	6.85	-0.68	0.000	2.37	-0.63	0.13	0.000
407	16.83	16.83	13.41	-2.34	0.55	-3.	5.47	-0.73	0.000	1.40	-0.75	0.14	0.000
408	16.83	16.83	13.81	-2.41	0.57	-3.	5.62	-0.75	0.000	1.39	-0.78	0.14	0.000
409	16.83	16.83	14.05	-2.46	0.58	-3.	5.69	-0.76	0.000	1.36	-0.80	0.14	0.000
410	16.83	16.83	14.19	-2.50	0.59	-3.	5.74	-0.77	0.000	1.36	-0.81	0.14	0.000
411	16.83	16.83	14.56	-2.57	0.61	-4.	5.87	-0.79	0.000	1.39	-0.78	0.14	0.000
412	16.83	16.83	14.92	-2.58	0.61	-3.	6.00	-0.80	0.000	1.38	-0.75	0.14	0.000
413	16.83	16.83	10.07	-2.66	0.56	-4.	4.28	-0.88	0.000	0.59	-0.89	0.14	0.000
414	16.83	16.83	10.67	-2.70	0.57	-4.	4.50	-0.89	0.000	0.52	-0.92	0.15	0.000
415	16.83	16.83	11.16	-2.75	0.58	-4.	4.66	-0.90	0.000	0.48	-0.94	0.15	0.000
416	16.83	16.83	11.40	-2.77	0.59	-4.	4.75	-0.90	0.000	0.48	-0.95	0.15	0.000
417	16.83	16.83	11.95	-2.81	0.61	-4.	4.95	-0.92	0.000	0.49	-0.92	0.15	0.000
418	16.83	16.83	12.54	-2.85	0.62	-4.	5.16	-0.93	0.000	0.52	-0.89	0.14	0.000
419	16.83	16.83	6.20	-2.96	0.54	-6.	2.89	-1.02	0.000	0.00	-1.03	0.16	0.000
420	16.83	16.83	6.92	-2.96	0.56	-6.	3.15	-1.02	0.000	0.00	-1.05	0.16	0.000
421	16.83	16.83	7.63	-2.99	0.57	-6.	3.42	-1.03	0.000	0.00	-1.08	0.17	0.000
422	16.83	16.83	7.92	-2.99	0.58	-6.	3.53	-1.03	0.000	0.00	-1.09	0.17	0.000
423	16.83	16.83	8.51	-3.00	0.58	-5.	3.74	-1.03	0.000	0.00	-1.06	0.16	0.000
424	16.83	16.83	9.26	-3.01	0.60	-5.	4.02	-1.04	0.000	0.00	-1.03	0.16	0.000
425	16.83	16.83	0.35	-3.19	0.50	-7.	0.76	-1.14	0.000	0.00	-1.17	0.18	0.000
426	16.83	16.83	1.01	-3.16	0.50	-7.	1.01	-1.13	0.000	0.00	-1.19	0.18	0.000
427	16.83	16.83	1.99	-3.17	0.52	-7.	1.34	-1.14	0.000	0.00	-1.22	0.19	0.000
428	16.83	16.83	2.32	-3.15	0.52	-7.	1.43	-1.14	0.000	0.00	-1.22	0.19	0.000
429	16.83	16.83	2.67	-3.09	0.51	-7.	1.53	-1.13	0.000	0.00	-1.19	0.18	0.000
430	16.83	16.83	3.48	-3.09	0.53	-7.	1.84	-1.13	0.000	0.00	-1.18	0.18	0.000
431	16.83	16.83	0.00	-3.37	0.52	-8.	0.00	-1.24	0.000	0.00	-1.30	0.20	0.000
432	16.83	16.83	0.00	-3.31	0.51	-8.	0.00	-1.24	0.000	0.00	-1.31	0.20	0.000
433	16.83	16.83	0.00	-3.30	0.51	-8.	0.00	-1.25	0.000	0.00	-1.33	0.20	0.000
434	16.83	16.83	0.00	-3.26	0.50	-8.	0.00	-1.26	0.000	0.00	-1.33	0.20	0.000
435	16.83	16.83	0.00	-3.17	0.49	-7.	0.00	-1.25	0.000	0.00	-1.32	0.20	0.000
436	16.83	16.83	0.00	-3.16	0.49	-7.	0.00	-1.26	0.000	0.00	-1.31	0.20	0.000
437	16.83	16.83	0.00	-3.38	0.52	-8.	0.00	-1.29	0.000	0.00	-1.35	0.21	0.000
438	16.83	16.83	0.00	-3.33	0.51	-8.	0.00	-1.32	0.000	0.00	-1.37	0.21	0.000
439	16.83	16.83	0.00	-3.31	0.51	-8.	0.00	-1.34	0.000	0.00	-1.37	0.21	0.000
440	16.83	16.83	0.00	-3.28	0.50	-8.	0.00	-1.34	0.000	0.00	-1.37	0.21	0.000
441	16.83	16.83	0.00	-3.22	0.50	-7.	0.00	-1.36	0.000	0.00	-1.37	0.21	0.000
442	16.83	16.83	0.00	-3.22	0.50	-7.	0.00	-1.39	0.000	0.00	-1.35	0.21	0.000
762	16.83	16.83	13.78	-1.30	0.40	-1.	3.38	-0.42	0.000	0.39	-0.36	0.06	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
365	10.21	10.21	0.00	0.20	0.00	10.	0.00	-0.01	0.000	1.25	0.01	0.04	0.004
366	10.21	10.21	3.19	0.19	0.00	16.	0.26	0.03	0.003	0.01	0.00	0.00	0.000
367	10.21	10.21	9.66	0.06	0.32	22.	3.23	-0.06	0.004	0.00	-0.01	0.00	0.000
368	10.21	10.21	14.85	-0.04	0.51	27.	5.25	-0.04	0.011	0.00	-0.01	0.00	0.000
369	10.21	10.21	19.25	0.03	0.66	40.	7.03	-0.04	0.015	0.00	0.00	0.00	0.000
371	10.21	10.21	0.00	0.19	0.00	9.	0.00	-0.01	0.000	0.69	0.01	0.02	0.003
372	10.21	10.21	4.84	0.16	0.12	18.	1.08	0.04	0.006	0.00	0.01	0.00	0.001
373	10.21	10.21	10.49	0.05	0.35	23.	3.54	-0.04	0.007	0.00	0.01	0.00	0.001
374	10.21	10.21	15.07	-0.01	0.52	30.	5.37	-0.01	0.013	0.00	0.01	0.00	0.001

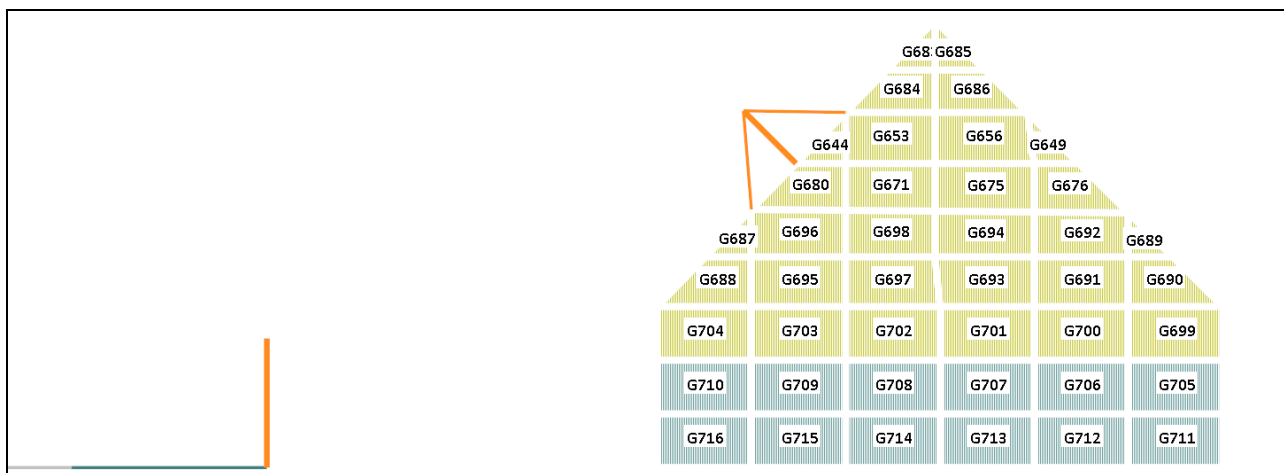
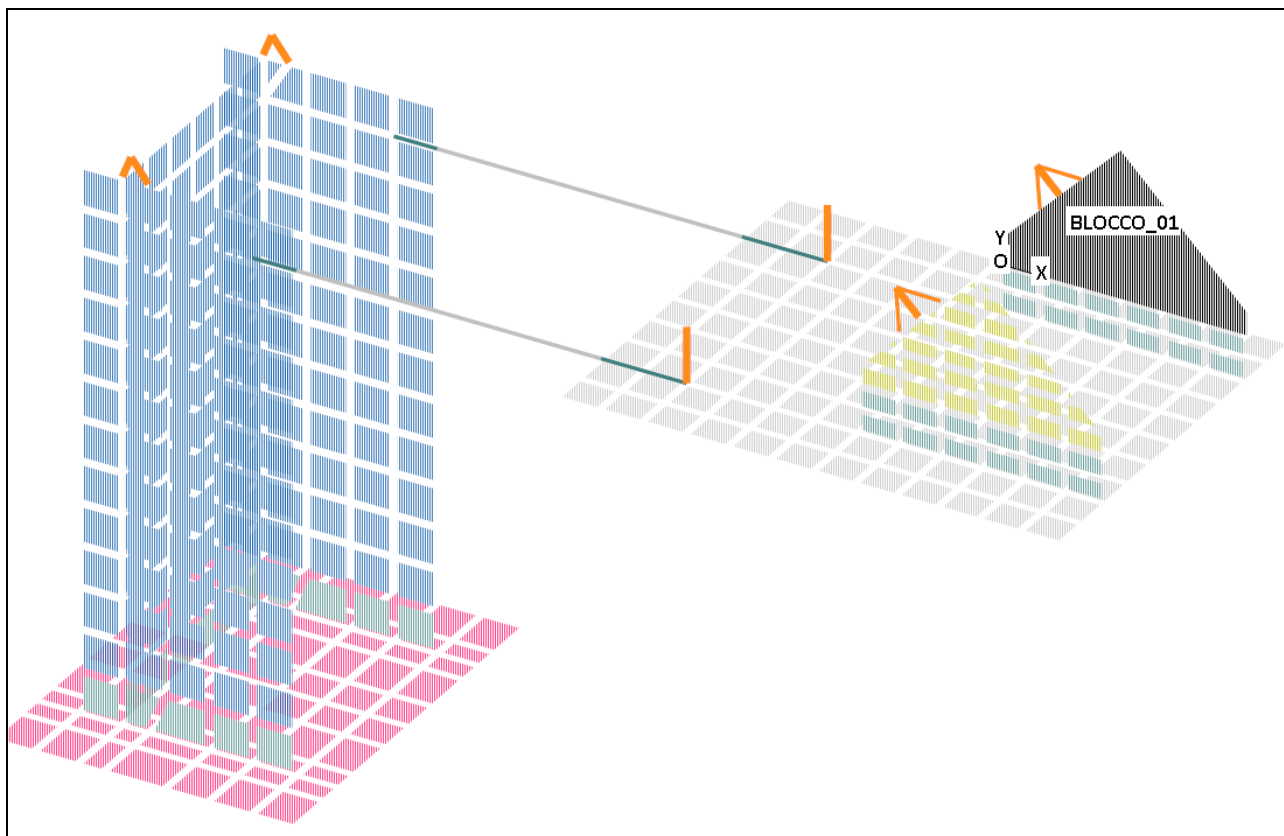
GUSCI	Af Afc		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
375	10.21	10.21	18.74	0.02	0.64	38.	6.88	-0.04	0.015	0.00	0.01	0.00	0.002
376	10.21	10.21	21.06	-0.06	0.72	39.	7.80	0.00	0.020	0.00	0.02	0.00	0.002
377	10.21	10.21	0.00	0.19	0.00	9.	0.00	-0.01	0.000	0.36	0.01	0.01	0.002
378	10.21	10.21	6.02	0.15	0.17	20.	1.61	0.04	0.008	0.00	0.02	0.00	0.003
379	10.21	10.21	11.09	0.05	0.37	25.	3.70	-0.01	0.009	0.02	0.02	0.00	0.002
380	10.21	10.21	15.14	-0.02	0.52	29.	5.41	-0.02	0.012	0.03	0.02	0.00	0.003
381	10.21	10.21	18.27	0.02	0.62	37.	6.69	-0.02	0.016	0.00	0.02	0.00	0.003
382	10.21	10.21	20.06	-0.01	0.69	39.	7.38	0.00	0.019	0.00	0.01	0.00	0.002
383	10.21	10.21	0.77	0.16	0.00	9.	0.00	0.01	0.002	0.00	0.03	0.00	0.003
384	10.21	10.21	8.47	0.18	0.26	26.	2.64	0.03	0.010	0.08	0.02	0.00	0.003
385	10.21	10.21	12.07	0.00	0.41	24.	4.01	0.01	0.011	0.13	0.02	0.00	0.002
386	10.21	10.21	15.37	-0.03	0.53	29.	5.49	-0.01	0.013	0.14	0.02	0.00	0.002
387	10.21	10.21	17.69	0.00	0.60	35.	6.46	0.00	0.016	0.01	0.03	0.00	0.004
388	10.21	10.21	18.40	0.02	0.63	38.	6.87	0.02	0.020	0.00	0.02	0.00	0.003
389	10.21	10.21	6.18	0.16	0.18	20.	1.60	0.02	0.006	0.00	0.02	0.00	0.002
390	10.21	10.21	9.83	0.15	0.31	27.	3.14	0.05	0.013	0.00	0.04	0.00	0.005
391	10.21	10.21	12.95	0.03	0.44	27.	4.34	0.05	0.015	0.22	0.04	0.00	0.005
392	10.21	10.21	15.53	-0.04	0.53	29.	5.57	0.03	0.016	0.27	0.04	0.00	0.005
393	10.21	10.21	16.96	0.01	0.58	34.	6.23	0.03	0.018	0.08	0.04	0.00	0.005
394	10.21	10.21	16.85	0.01	0.57	34.	6.24	0.02	0.018	0.00	0.02	0.00	0.002
395	10.21	10.21	7.71	0.18	0.23	24.	2.19	0.04	0.009	0.00	0.02	0.00	0.003
396	10.21	10.21	10.64	0.12	0.35	27.	3.49	0.06	0.014	0.10	0.05	0.00	0.006
397	10.21	10.21	13.41	0.05	0.45	29.	4.54	0.06	0.018	0.38	0.05	0.00	0.007
398	10.21	10.21	15.53	0.01	0.53	31.	5.58	0.05	0.019	0.41	0.05	0.00	0.007
399	10.21	10.21	16.47	0.02	0.56	34.	6.00	0.04	0.019	0.16	0.05	0.00	0.006
400	10.21	10.21	16.02	0.02	0.55	33.	5.78	0.02	0.016	0.00	0.02	0.00	0.003
401	10.21	10.21	8.37	0.16	0.26	25.	2.53	0.05	0.011	0.00	0.03	0.00	0.003
402	10.21	10.21	11.12	0.07	0.37	26.	3.74	0.05	0.014	0.24	0.04	0.00	0.005
403	10.21	10.21	13.72	0.02	0.47	28.	4.69	0.06	0.017	0.59	0.05	0.00	0.006
404	10.21	10.21	15.56	0.00	0.53	31.	5.57	0.05	0.019	0.60	0.04	0.00	0.006
405	10.21	10.21	16.17	0.01	0.55	33.	5.81	0.04	0.018	0.26	0.04	0.00	0.005
406	10.21	10.21	15.41	0.03	0.52	32.	5.44	0.02	0.016	0.00	0.03	0.00	0.003
407	10.21	10.21	8.20	0.09	0.27	21.	2.57	0.04	0.010	0.00	0.02	0.00	0.003
408	10.21	10.21	11.34	-0.01	0.39	22.	3.87	0.03	0.012	0.43	0.02	0.00	0.003
409	10.21	10.21	14.03	-0.05	0.48	26.	4.82	0.04	0.016	0.86	0.02	0.02	0.004
410	10.21	10.21	15.71	-0.05	0.54	29.	5.60	0.03	0.017	0.86	0.02	0.02	0.004
411	10.21	10.21	16.03	-0.01	0.55	32.	5.69	0.03	0.017	0.43	0.02	0.01	0.003
412	10.21	10.21	14.90	0.02	0.51	31.	5.16	0.02	0.015	0.00	0.02	0.00	0.003
413	10.21	10.21	7.45	-0.02	0.26	14.	2.38	0.01	0.007	0.00	0.00	0.00	0.001
414	10.21	10.21	11.71	-0.12	0.40	18.	4.03	-0.01	0.010	0.87	-0.01	0.03	0.002
415	10.21	10.21	14.49	-0.14	0.50	22.	5.04	0.00	0.013	1.30	-0.01	0.04	0.003
416	10.21	10.21	15.90	-0.01	0.54	31.	5.63	0.00	0.014	1.22	-0.01	0.04	0.002
417	10.21	10.21	15.85	-0.09	0.54	27.	5.50	0.00	0.014	0.80	-0.01	0.03	0.001
418	10.21	10.21	14.19	-0.03	0.49	27.	4.73	0.01	0.013	0.00	0.00	0.00	0.000
419	10.21	10.21	6.98	-0.14	0.23	7.	2.28	-0.02	0.004	0.00	-0.03	0.00	0.000
420	10.21	10.21	12.54	-0.22	0.42	15.	4.38	-0.04	0.009	1.12	-0.04	0.03	0.001
421	10.21	10.21	15.09	-0.24	0.51	19.	5.33	-0.04	0.011	1.66	-0.02	0.06	0.003
422	10.21	10.21	15.96	-0.08	0.55	28.	5.63	-0.04	0.012	1.68	-0.03	0.06	0.003
423	10.21	10.21	15.48	-0.14	0.53	24.	4.83	-0.03	0.010	1.10	-0.04	0.03	0.001
424	10.21	10.21	13.03	-0.09	0.45	22.	3.66	-0.02	0.008	0.00	-0.03	0.00	0.000
425	10.21	10.21	6.72	-0.22	0.21	4.	2.23	-0.05	0.003	0.00	-0.05	0.01	0.000
426	10.21	10.21	12.64	-0.29	0.41	12.	4.44	-0.07	0.007	1.31	-0.01	0.05	0.003
427	10.21	10.21	15.33	-0.05	0.53	28.	5.42	-0.07	0.009	1.90	-0.05	0.06	0.002
428	10.21	10.21	15.89	-0.12	0.55	26.	5.59	-0.01	0.013	1.98	-0.06	0.06	0.002
429	10.21	10.21	15.12	-0.15	0.52	23.	4.48	-0.05	0.008	1.35	-0.01	0.05	0.003
430	10.21	10.21	12.34	-0.16	0.42	17.	3.20	-0.01	0.008	0.00	-0.05	0.01	0.000
431	10.21	10.21	6.16	-0.28	0.17	2.	2.05	-0.07	0.002	0.00	-0.07	0.01	0.000
432	10.21	10.21	12.94	-0.01	0.44	25.	4.57	-0.09	0.006	1.48	-0.03	0.05	0.002
433	10.21	10.21	15.69	-0.10	0.54	27.	5.56	-0.10	0.008	2.14	-0.07	0.06	0.001
434	10.21	10.21	15.99	-0.15	0.55	25.	5.62	-0.03	0.012	2.27	-0.08	0.07	0.002
435	10.21	10.21	14.94	-0.17	0.51	22.	4.24	-0.07	0.006	1.61	-0.03	0.05	0.002
436	10.21	10.21	11.70	-0.15	0.40	16.	2.73	-0.03	0.005	0.00	-0.07	0.01	0.000
437	10.21	10.21	4.80	-0.33	0.13	0.	1.58	-0.08	0.000	0.00	-0.02	0.00	0.000
438	10.21	10.21	13.13	-0.07	0.45	23.	4.67	-0.11	0.006	1.72	-0.05	0.05	0.001
439	10.21	10.21	16.13	-0.14	0.55	25.	5.73	-0.02	0.014	2.47	-0.10	0.07	0.001
440	10.21	10.21	15.99	-0.18	0.55	23.	5.60	-0.05	0.011	2.61	-0.10	0.08	0.001
441	10.21	10.21	14.44	-0.19	0.49	20.	3.86	-0.10	0.004	1.88	-0.06	0.06	0.002
442	10.21	10.21	10.52	-0.13	0.36	15.	1.85	-0.05	0.002	0.00	-0.02	0.00	0.000
762	10.21	10.21	22.44	-0.05	0.77	43.	8.35	-0.01	0.021	0.09	0.02	0.00	0.002

ARMATURA SUPERIORE VERTICALE

GUSCI	Af Afc		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
365	16.83	16.83	0.00	-1.04	0.16	-2.	0.00	-0.42	0.000	0.00	-0.47	0.07	0.000
366	16.83	16.83	0.00	-1.09	0.17	-3.	0.00	-0.39	0.000	0.00	-0.43	0.07	0.000
367	16.83	16.83	0.00	-1.46	0.22	-3.	0.00	-0.47	0.000	0.00	-0.50	0.08	0.000
368	16.83	16.83	0.00	-1.42	0.22	-3.	0.00	-0.45	0.000	0.00	-0.46	0.07	0.000
369	16.83	16.83	6.07	-1.20	0.10	-4.	2.08	-0.35	0.000	0.46	-0.35	0.05	0.000
371	16.83	16.83	1.83	-1.11	0.14	-3.	1.54	-0.39	0.000	0.00	-0.43	0.07	0.000
372	16.83	16.83	3.08	-1.22	0.14	-3.	1.97	-0.39	0.000	0.00	-0.39	0.06	0.000
373	16.83	16.83	3.76	-1.43	0.16	-4.	2.32	-0.41	0.000	0.00	-0.43	0.07	0.000
374	16.83	16.83	4.34	-1.44	0.16	-4.	2.54	-0.40	0.000	0.00	-0.42	0.07	0.000
375	16.83	16.83	5.53	-1.32	0.12	-4.	2.90	-0.34	0.000	0.00	-0.34	0.05	0.000
376	16.83	16.83	6.45	-1.48	0.13	-4.	3.28	-0.36	0.000	0.00	-0.37	0.06	0.000
377	16.83	16.83	2.85	-1.18	0.14	-3.	1.13	-0.38	0.000	0.00	-0.36	0.06	0.000
378	16.83	16.83	3.62	-1.29	0.15	-4.	1.50	-0.38	0.000	0.00	-0.36	0.06	0.000

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
379	16.83	16.83	4.12	-1.39	0.15	-4.	1.78	-0.37	0.000	0.00	-0.38	0.06	0.000
380	16.83	16.83	4.48	-1.42	0.15	-4.	1.95	-0.36	0.000	0.00	-0.38	0.06	0.000
381	16.83	16.83	5.33	-1.43	0.14	-4.	2.32	-0.34	0.000	0.00	-0.34	0.05	0.000
382	16.83	16.83	5.99	-1.53	0.15	-5.	2.66	-0.33	0.000	0.00	-0.33	0.05	0.000
383	16.83	16.83	3.32	-1.31	0.15	-4.	0.52	-0.39	0.000	0.00	-0.39	0.06	0.000
384	16.83	16.83	3.82	-1.41	0.16	-4.	0.79	-0.39	0.000	0.00	-0.40	0.06	0.000
385	16.83	16.83	4.01	-1.48	0.17	-4.	0.84	-0.37	0.000	0.00	-0.39	0.06	0.000
386	16.83	16.83	4.27	-1.53	0.17	-4.	0.89	-0.36	0.000	0.00	-0.39	0.06	0.000
387	16.83	16.83	4.94	-1.61	0.18	-5.	1.20	-0.36	0.000	0.00	-0.39	0.06	0.000
388	16.83	16.83	5.27	-1.68	0.18	-5.	1.34	-0.35	0.000	0.00	-0.37	0.06	0.000
389	16.83	16.83	5.29	-1.51	0.16	-4.	0.83	-0.43	0.000	0.00	-0.46	0.07	0.000
390	16.83	16.83	5.45	-1.61	0.17	-5.	0.93	-0.44	0.000	0.00	-0.47	0.07	0.000
391	16.83	16.83	5.41	-1.67	0.18	-5.	0.84	-0.43	0.000	0.00	-0.46	0.07	0.000
392	16.83	16.83	5.50	-1.72	0.18	-5.	0.82	-0.43	0.000	0.00	-0.46	0.07	0.000
393	16.83	16.83	5.79	-1.83	0.20	-5.	0.95	-0.45	0.000	0.00	-0.47	0.07	0.000
394	16.83	16.83	5.83	-1.90	0.21	-5.	0.94	-0.44	0.000	0.00	-0.46	0.07	0.000
395	16.83	16.83	7.89	-1.76	0.16	-5.	1.48	-0.50	0.000	0.00	-0.53	0.08	0.000
396	16.83	16.83	7.82	-1.85	0.17	-6.	1.50	-0.52	0.000	0.00	-0.55	0.08	0.000
397	16.83	16.83	7.70	-1.91	0.18	-6.	1.46	-0.52	0.000	0.00	-0.55	0.08	0.000
398	16.83	16.83	7.69	-1.96	0.19	-6.	1.47	-0.53	0.000	0.00	-0.55	0.09	0.000
399	16.83	16.83	7.69	-2.07	0.21	-6.	1.46	-0.55	0.000	0.00	-0.55	0.08	0.000
400	16.83	16.83	7.58	-2.12	0.22	-6.	1.48	-0.56	0.000	0.00	-0.53	0.08	0.000
401	16.83	16.83	10.35	-2.04	0.16	-6.	2.43	-0.61	0.000	0.00	-0.63	0.10	0.000
402	16.83	16.83	10.19	-2.12	0.18	-7.	2.40	-0.63	0.000	0.00	-0.65	0.10	0.000
403	16.83	16.83	10.06	-2.19	0.19	-7.	2.37	-0.63	0.000	0.00	-0.67	0.10	0.000
404	16.83	16.83	9.97	-2.23	0.20	-7.	2.34	-0.64	0.000	0.00	-0.67	0.10	0.000
405	16.83	16.83	9.81	-2.33	0.22	-7.	2.25	-0.67	0.000	0.00	-0.66	0.10	0.000
406	16.83	16.83	9.66	-2.34	0.22	-7.	2.25	-0.68	0.000	0.00	-0.63	0.10	0.000
407	16.83	16.83	12.12	-2.34	0.18	-7.	3.19	-0.73	0.000	0.00	-0.75	0.12	0.000
408	16.83	16.83	12.01	-2.41	0.20	-8.	3.17	-0.75	0.000	0.00	-0.78	0.12	0.000
409	16.83	16.83	11.92	-2.46	0.21	-8.	3.15	-0.76	0.000	0.00	-0.80	0.12	0.000
410	16.83	16.83	11.79	-2.50	0.21	-8.	3.10	-0.77	0.000	0.00	-0.81	0.12	0.000
411	16.83	16.83	11.56	-2.57	0.23	-8.	3.01	-0.79	0.000	0.00	-0.78	0.12	0.000
412	16.83	16.83	11.50	-2.58	0.23	-8.	3.01	-0.80	0.000	0.00	-0.75	0.12	0.000
413	16.83	16.83	13.88	-2.66	0.21	-8.	3.90	-0.88	0.000	0.00	-0.89	0.14	0.000
414	16.83	16.83	13.79	-2.70	0.22	-9.	3.88	-0.89	0.000	0.00	-0.92	0.14	0.000
415	16.83	16.83	13.67	-2.75	0.22	-9.	3.84	-0.90	0.000	0.00	-0.94	0.15	0.000
416	16.83	16.83	13.52	-2.77	0.23	-9.	3.79	-0.90	0.000	0.00	-0.95	0.15	0.000
417	16.83	16.83	13.34	-2.81	0.24	-9.	3.74	-0.92	0.000	0.00	-0.92	0.14	0.000
418	16.83	16.83	13.29	-2.85	0.24	-9.	3.72	-0.93	0.000	0.00	-0.89	0.14	0.000
419	16.83	16.83	15.79	-2.96	0.23	-9.	4.59	-1.02	0.000	0.86	-1.03	0.15	0.000
420	16.83	16.83	15.75	-2.96	0.23	-9.	4.59	-1.02	0.000	0.73	-1.05	0.15	0.000
421	16.83	16.83	15.54	-2.99	0.23	-9.	4.52	-1.03	0.000	0.60	-1.08	0.16	0.000
422	16.83	16.83	15.36	-2.99	0.24	-9.	4.46	-1.03	0.000	0.58	-1.09	0.16	0.000
423	16.83	16.83	15.28	-3.00	0.24	-9.	4.45	-1.03	0.000	0.62	-1.06	0.15	0.000
424	16.83	16.83	15.23	-3.01	0.24	-9.	4.44	-1.04	0.000	0.74	-1.03	0.15	0.000
425	16.83	16.83	19.33	-3.19	0.21	-11.	5.95	-1.14	0.000	2.48	-1.17	0.14	0.000
426	16.83	16.83	19.22	-3.16	0.21	-10.	5.92	-1.13	0.000	2.43	-1.19	0.15	0.000
427	16.83	16.83	18.73	-3.17	0.22	-10.	5.73	-1.14	0.000	2.24	-1.22	0.15	0.000
428	16.83	16.83	18.50	-3.15	0.22	-10.	5.64	-1.14	0.000	2.22	-1.22	0.16	0.000
429	16.83	16.83	18.53	-3.09	0.21	-10.	5.66	-1.13	0.000	2.32	-1.19	0.15	0.000
430	16.83	16.83	18.28	-3.09	0.21	-10.	5.57	-1.13	0.000	2.37	-1.18	0.15	0.000
431	16.83	16.83	27.94	-3.37	0.11	-12.	9.42	-1.24	0.000	5.65	-1.30	0.12	0.000
432	16.83	16.83	27.36	-3.31	0.11	-12.	9.21	-1.24	0.000	5.65	-1.31	0.12	0.000
433	16.83	16.83	26.15	-3.30	0.13	-12.	8.69	-1.25	0.000	5.48	-1.33	0.12	0.000
434	16.83	16.83	25.73	-3.26	0.13	-12.	8.45	-1.26	0.000	5.51	-1.33	0.12	0.000
435	16.83	16.83	25.63	-3.17	0.12	-12.	8.40	-1.25	0.000	5.75	-1.32	0.12	0.000
436	16.83	16.83	24.60	-3.16	0.13	-11.	7.96	-1.26	0.000	5.77	-1.31	0.12	0.000
437	16.83	16.83	46.08	-3.38	1.21	0.	16.79	-1.29	0.000	12.62	-1.35	0.02	0.000
438	16.83	16.83	43.90	-3.33	1.16	0.	15.65	-1.32	0.000	12.23	-1.37	0.03	0.000
439	16.83	16.83	41.67	-3.31	0.10	-15.	14.91	-1.34	0.000	11.99	-1.37	0.04	0.000
440	16.83	16.83	40.49	-3.28	0.08	-14.	14.58	-1.34	0.000	12.10	-1.37	0.03	0.000
441	16.83	16.83	38.15	-3.22	0.06	-14.	13.67	-1.36	0.000	12.36	-1.37	0.03	0.000
442	16.83	16.83	36.02	-3.22	0.03	-13.	13.15	-1.39	0.000	12.79	-1.35	0.02	0.000
762	16.83	16.83	9.28	-1.30	0.06	-5.	3.83	-0.42	0.000	0.56	-0.36	0.05	0.000

6.6. BLOCCO ANCORAGGIO 01



6.6.1. Verifica SLU

GUSCI	spess	INFERIORE ORIZZONTALE							INFERIORE VERTICALE						
		Af	Afc	Mom	Nor	epsC	epsF		Af	Afc	Mom	Nor	epsC	epsF	
644	0.8	15.71	15.71	2.	5.	0.00	0.79		15.71	15.71	1.	1.	0.00	0.11	
649	0.8	15.71	15.71	0.	2.	0.00	0.28		15.71	15.71	1.	1.	0.00	0.11	
653	0.8	15.71	15.71	1.	5.	0.00	0.72		15.71	15.71	1.	1.	0.00	0.13	
656	0.8	15.71	15.71	0.	3.	0.00	0.43		15.71	15.71	1.	1.	0.00	0.13	
671	0.8	15.71	15.71	1.	5.	0.00	0.72		15.71	15.71	0.	6.	0.00	0.89	
675	0.8	15.71	15.71	0.	3.	0.00	0.44		15.71	15.71	0.	6.	0.00	0.89	
676	0.8	15.71	15.71	0.	2.	0.00	0.30		15.71	15.71	0.	6.	0.00	0.90	
680	0.8	15.71	15.71	1.	5.	0.00	0.80		15.71	15.71	0.	6.	0.00	0.88	
683	0.8	15.71	15.71	0.	4.	0.00	0.57		15.71	15.71	0.	0.	0.00	0.00	
684	0.8	15.71	15.71	1.	4.	0.00	0.68		15.71	15.71	0.	0.	0.00	0.02	
685	0.8	15.71	15.71	0.	2.	0.00	0.36		15.71	15.71	0.	0.	0.00	0.00	
686	0.8	15.71	15.71	0.	3.	0.00	0.42		15.71	15.71	0.	0.	0.00	0.02	
687	0.8	15.71	15.71	1.	0.	0.00	0.04		15.71	15.71	0.	4.	0.00	0.66	
688	0.8	15.71	15.71	1.	1.	0.00	0.10		15.71	15.71	0.	4.	0.00	0.60	
689	0.8	15.71	15.71	0.	1.	0.00	0.17		15.71	15.71	0.	4.	0.00	0.65	
690	0.8	15.71	15.71	0.	1.	0.00	0.17		15.71	15.71	0.	4.	0.00	0.59	
691	0.8	15.71	15.71	0.	2.	0.00	0.30		15.71	15.71	0.	4.	0.00	0.57	

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
692	0.8	15.71	15.71	0.	2.	0.00	0.30	15.71	15.71	0.	4.	0.00	0.65
693	0.8	15.71	15.71	0.	3.	0.00	0.44	15.71	15.71	0.	4.	0.00	0.53
694	0.8	15.71	15.71	0.	3.	0.00	0.44	15.71	15.71	0.	4.	0.00	0.65
695	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	0.	4.	0.00	0.55
696	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	0.	4.	0.00	0.65
697	0.8	15.71	15.71	1.	5.	0.00	0.72	15.71	15.71	0.	4.	0.00	0.53
698	0.8	15.71	15.71	1.	5.	0.00	0.72	15.71	15.71	0.	4.	0.00	0.65
699	0.8	15.71	15.71	0.	1.	0.00	0.17	15.71	15.71	0.	4.	0.00	0.57
700	0.8	15.71	15.71	0.	2.	0.00	0.30	15.71	15.71	0.	4.	0.00	0.53
701	0.8	15.71	15.71	0.	3.	0.00	0.44	15.71	15.71	0.	3.	0.00	0.47
702	0.8	15.71	15.71	1.	5.	0.00	0.72	15.71	15.71	0.	3.	0.00	0.47
703	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	0.	3.	0.00	0.49
704	0.8	15.71	15.71	1.	1.	0.00	0.10	15.71	15.71	0.	3.	0.00	0.52

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
644	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	1.	1.	0.00	0.11
649	0.8	15.71	15.71	2.	2.	0.00	0.29	15.71	15.71	1.	1.	0.00	0.11
653	0.8	15.71	15.71	2.	5.	0.00	0.72	15.71	15.71	1.	1.	0.00	0.12
656	0.8	15.71	15.71	2.	3.	0.00	0.44	15.71	15.71	1.	1.	0.00	0.12
671	0.8	15.71	15.71	2.	5.	0.00	0.72	15.71	15.71	2.	6.	0.00	0.90
675	0.8	15.71	15.71	2.	3.	0.00	0.44	15.71	15.71	2.	6.	0.00	0.90
676	0.8	15.71	15.71	2.	2.	0.00	0.30	15.71	15.71	2.	6.	0.00	0.91
680	0.8	15.71	15.71	2.	5.	0.00	0.80	15.71	15.71	3.	6.	0.00	0.89
683	0.8	15.71	15.71	1.	4.	0.00	0.58	15.71	15.71	0.	0.	0.00	0.00
684	0.8	15.71	15.71	2.	4.	0.00	0.68	15.71	15.71	1.	0.	0.00	0.02
685	0.8	15.71	15.71	1.	2.	0.00	0.37	15.71	15.71	0.	0.	0.00	0.00
686	0.8	15.71	15.71	2.	3.	0.00	0.42	15.71	15.71	1.	0.	0.00	0.02
687	0.8	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	3.	4.	0.00	0.68
688	0.8	15.71	15.71	0.	1.	0.00	0.09	15.71	15.71	3.	4.	0.00	0.61
689	0.8	15.71	15.71	2.	1.	0.00	0.18	15.71	15.71	3.	4.	0.00	0.66
690	0.8	15.71	15.71	2.	1.	0.00	0.18	15.71	15.71	3.	4.	0.00	0.60
691	0.8	15.71	15.71	2.	2.	0.00	0.30	15.71	15.71	3.	4.	0.00	0.58
692	0.8	15.71	15.71	2.	2.	0.00	0.30	15.71	15.71	3.	4.	0.00	0.66
693	0.8	15.71	15.71	2.	3.	0.00	0.44	15.71	15.71	3.	4.	0.00	0.54
694	0.8	15.71	15.71	2.	3.	0.00	0.44	15.71	15.71	3.	4.	0.00	0.66
695	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	3.	4.	0.00	0.57
696	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	3.	4.	0.00	0.66
697	0.8	15.71	15.71	2.	5.	0.00	0.72	15.71	15.71	3.	4.	0.00	0.54
698	0.8	15.71	15.71	2.	5.	0.00	0.72	15.71	15.71	3.	4.	0.00	0.66
699	0.8	15.71	15.71	2.	1.	0.00	0.18	15.71	15.71	3.	4.	0.00	0.58
700	0.8	15.71	15.71	2.	2.	0.00	0.30	15.71	15.71	3.	4.	0.00	0.55
701	0.8	15.71	15.71	2.	3.	0.00	0.44	15.71	15.71	3.	3.	0.00	0.49
702	0.8	15.71	15.71	2.	5.	0.00	0.72	15.71	15.71	3.	3.	0.00	0.49
703	0.8	15.71	15.71	2.	5.	0.00	0.79	15.71	15.71	3.	3.	0.00	0.51
704	0.8	15.71	15.71	0.	1.	0.00	0.10	15.71	15.71	3.	3.	0.00	0.53

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO ($R_d > E_d$)

6.6.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
644	15.71	15.71	0.89	3.86	0.00	124.	0.08	1.34	0.095	0.07	1.29	0.00	0.092
649	15.71	15.71	0.00	1.41	0.00	45.	0.00	0.62	0.044	0.05	0.61	0.00	0.043
653	15.71	15.71	0.31	3.19	0.00	102.	0.01	1.18	0.084	0.07	1.15	0.00	0.082
656	15.71	15.71	0.13	2.01	0.00	64.	0.00	0.80	0.057	0.07	0.79	0.00	0.056
671	15.71	15.71	0.31	3.19	0.00	102.	0.01	1.18	0.084	0.07	1.15	0.00	0.082
675	15.71	15.71	0.12	2.03	0.00	65.	0.00	0.81	0.057	0.07	0.79	0.00	0.056
676	15.71	15.71	0.00	1.44	0.00	46.	0.00	0.63	0.044	0.05	0.62	0.00	0.044
680	15.71	15.71	1.04	3.65	0.00	117.	0.08	1.26	0.090	0.06	1.21	0.00	0.086
683	15.71	15.71	0.25	2.83	0.00	90.	0.00	1.06	0.075	0.07	1.03	0.00	0.073
684	15.71	15.71	0.29	3.00	0.00	96.	0.01	1.12	0.079	0.07	1.08	0.00	0.077
685	15.71	15.71	0.14	1.78	0.00	57.	0.00	0.72	0.051	0.06	0.70	0.00	0.049
686	15.71	15.71	0.14	1.90	0.00	61.	0.00	0.76	0.054	0.07	0.74	0.00	0.053
687	15.71	15.71	0.48	0.16	0.00	5.	0.04	0.03	0.002	0.01	0.03	0.00	0.002
688	15.71	15.71	0.44	0.15	0.00	5.	0.05	0.02	0.001	0.02	0.02	0.00	0.002
689	15.71	15.71	0.00	0.83	0.00	27.	0.00	0.42	0.030	0.01	0.41	0.00	0.029
690	15.71	15.71	0.00	0.79	0.00	25.	0.00	0.39	0.028	0.00	0.38	0.00	0.027
691	15.71	15.71	0.00	1.47	0.00	47.	0.00	0.64	0.045	0.04	0.64	0.00	0.045
692	15.71	15.71	0.00	1.47	0.00	47.	0.00	0.64	0.045	0.04	0.64	0.00	0.045
693	15.71	15.71	0.12	2.03	0.00	65.	0.00	0.81	0.058	0.07	0.80	0.00	0.056
694	15.71	15.71	0.12	2.03	0.00	65.	0.00	0.81	0.057	0.07	0.79	0.00	0.056
695	15.71	15.71	1.13	2.50	0.00	81.	0.11	0.87	0.061	0.06	0.84	0.00	0.059
696	15.71	15.71	1.13	2.50	0.00	81.	0.11	0.87	0.061	0.06	0.84	0.00	0.059
697	15.71	15.71	0.31	3.17	0.00	101.	0.01	1.18	0.084	0.07	1.14	0.00	0.081
698	15.71	15.71	0.31	3.19	0.00	102.	0.01	1.18	0.084	0.07	1.15	0.00	0.082
699	15.71	15.71	0.13	0.69	0.00	22.	0.00	0.34	0.024	0.00	0.33	0.00	0.024
700	15.71	15.71	0.00	1.47	0.00	47.	0.00	0.64	0.045	0.04	0.64	0.00	0.045
701	15.71	15.71	0.12	2.04	0.00	65.	0.00	0.81	0.058	0.07	0.80	0.00	0.057
702	15.71	15.71	0.31	3.15	0.00	100.	0.01	1.17	0.083	0.07	1.13	0.00	0.080
703	15.71	15.71	1.13	2.50	0.00	81.	0.11	0.87	0.061	0.06	0.84	0.00	0.059
704	15.71	15.71	0.36	0.46	0.00	15.	0.06	0.05	0.003	0.03	0.06	0.00	0.005

ARMATURA INFERIORE VERTICALE

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
644	15.71	15.71	0.63	0.52	0.00	17.	0.11	0.16	0.011	0.02	0.15	0.00	0.011
649	15.71	15.71	0.63	0.52	0.00	17.	0.11	0.16	0.011	0.02	0.15	0.00	0.011
653	15.71	15.71	0.60	0.54	0.00	18.	0.10	0.17	0.012	0.02	0.16	0.00	0.011
656	15.71	15.71	0.60	0.54	0.00	18.	0.10	0.17	0.012	0.02	0.16	0.00	0.011
671	15.71	15.71	0.16	3.50	0.00	112.	0.00	1.15	0.082	0.03	1.09	0.00	0.078
675	15.71	15.71	0.16	3.52	0.00	112.	0.00	1.16	0.082	0.03	1.10	0.00	0.078
676	15.71	15.71	0.16	3.55	0.00	113.	0.00	1.16	0.083	0.03	1.11	0.00	0.079
680	15.71	15.71	0.16	3.48	0.00	111.	0.00	1.14	0.081	0.03	1.08	0.00	0.077
683	15.71	15.71	0.03	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
684	15.71	15.71	0.13	0.09	0.00	3.	0.02	0.01	0.001	0.01	0.01	0.00	0.001
685	15.71	15.71	0.03	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
686	15.71	15.71	0.13	0.09	0.00	3.	0.02	0.01	0.001	0.01	0.01	0.00	0.001
687	15.71	15.71	0.00	3.24	0.00	103.	0.00	1.01	0.072	0.04	0.97	0.00	0.069
688	15.71	15.71	0.00	2.82	0.00	90.	0.00	0.81	0.057	0.05	0.78	0.00	0.055
689	15.71	15.71	0.00	3.16	0.00	101.	0.00	1.01	0.072	0.05	0.96	0.00	0.068
690	15.71	15.71	0.00	2.84	0.00	90.	0.00	0.86	0.061	0.08	0.83	0.00	0.059
691	15.71	15.71	0.00	2.57	0.00	82.	0.00	0.77	0.054	0.06	0.74	0.00	0.052
692	15.71	15.71	0.00	3.14	0.00	100.	0.00	0.99	0.070	0.04	0.94	0.00	0.067
693	15.71	15.71	0.00	2.55	0.00	81.	0.00	0.76	0.054	0.06	0.73	0.00	0.052
694	15.71	15.71	0.00	3.14	0.00	100.	0.00	0.99	0.070	0.04	0.94	0.00	0.067
695	15.71	15.71	0.00	2.56	0.00	82.	0.00	0.76	0.054	0.06	0.74	0.00	0.052
696	15.71	15.71	0.00	3.14	0.00	100.	0.00	0.99	0.070	0.04	0.94	0.00	0.067
697	15.71	15.71	0.00	2.55	0.00	81.	0.00	0.76	0.054	0.06	0.73	0.00	0.052
698	15.71	15.71	0.00	3.14	0.00	100.	0.00	0.99	0.070	0.04	0.94	0.00	0.067
699	15.71	15.71	0.00	2.72	0.00	87.	0.00	0.72	0.051	0.12	0.77	0.00	0.054
700	15.71	15.71	0.00	2.40	0.00	77.	0.00	0.61	0.043	0.08	0.65	0.00	0.046
701	15.71	15.71	0.00	2.24	0.00	71.	0.00	0.57	0.040	0.07	0.61	0.00	0.043
702	15.71	15.71	0.00	2.24	0.00	71.	0.00	0.57	0.040	0.07	0.61	0.00	0.043
703	15.71	15.71	0.00	2.30	0.00	73.	0.00	0.57	0.041	0.07	0.62	0.00	0.044
704	15.71	15.71	0.00	2.45	0.00	78.	0.00	0.55	0.039	0.06	0.61	0.00	0.043

ARMATURA SUPERIORE ORIZZONTALE

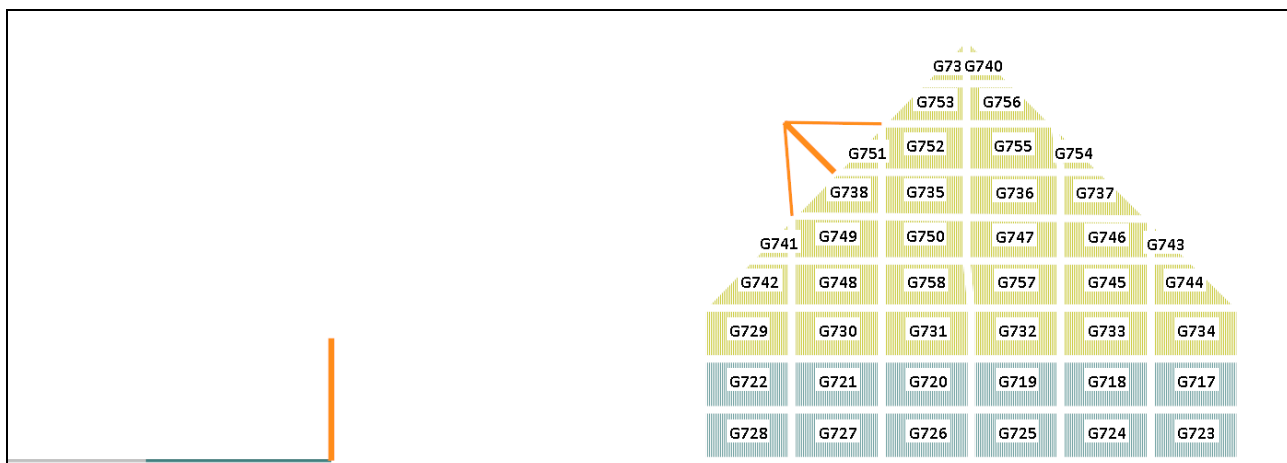
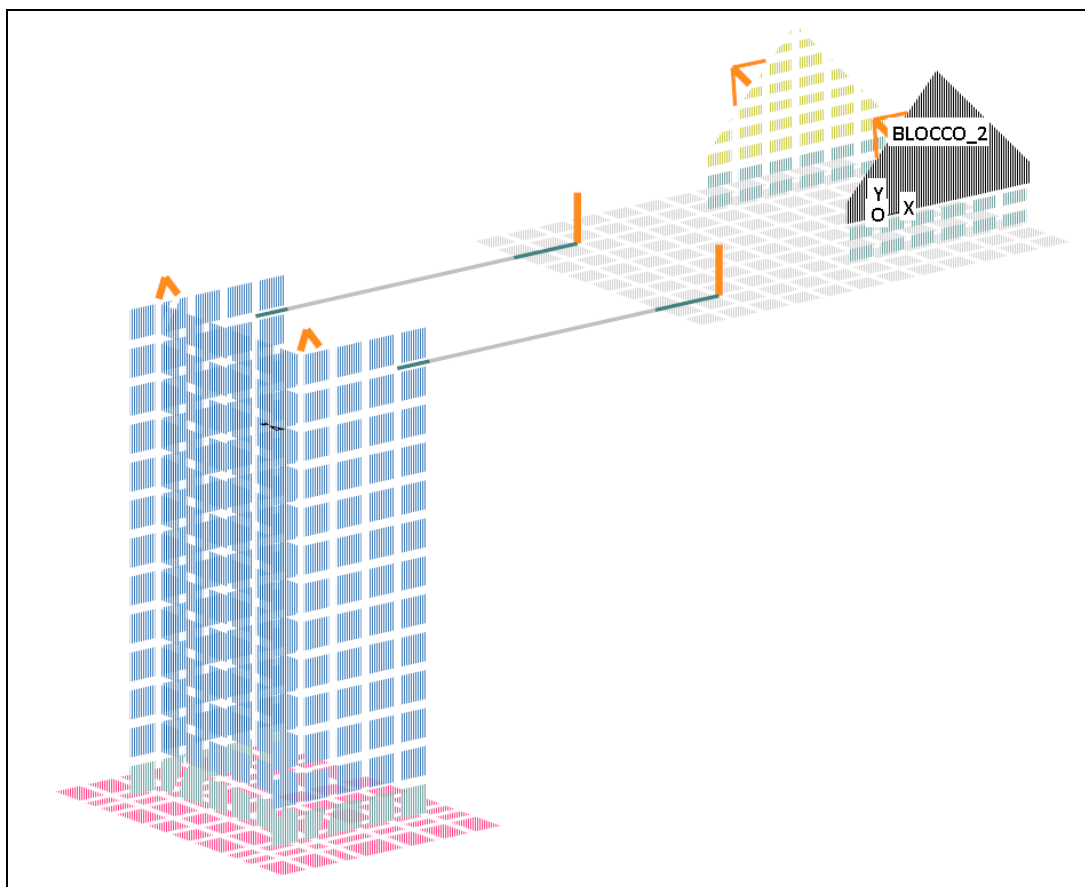
GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
644	15.71	15.71	1.01	3.86	0.00	124.	0.12	1.34	0.095	0.04	1.29	0.00	0.092
649	15.71	15.71	1.22	1.41	0.00	46.	0.07	0.62	0.044	0.05	0.61	0.00	0.043
653	15.71	15.71	0.88	3.19	0.00	103.	0.08	1.18	0.084	0.03	1.15	0.00	0.082
656	15.71	15.71	1.00	2.01	0.00	65.	0.05	0.80	0.057	0.04	0.79	0.00	0.056
671	15.71	15.71	0.88	3.19	0.00	103.	0.08	1.18	0.084	0.03	1.15	0.00	0.082
675	15.71	15.71	1.01	2.03	0.00	65.	0.05	0.81	0.057	0.04	0.79	0.00	0.056
676	15.71	15.71	1.23	1.44	0.00	47.	0.06	0.63	0.044	0.05	0.62	0.00	0.044
680	15.71	15.71	0.83	3.65	0.00	117.	0.08	1.26	0.090	0.04	1.21	0.00	0.086
683	15.71	15.71	0.84	2.83	0.00	91.	0.07	1.06	0.075	0.02	1.03	0.00	0.073
684	15.71	15.71	0.86	3.00	0.00	96.	0.07	1.12	0.079	0.03	1.08	0.00	0.077
685	15.71	15.71	0.90	1.78	0.00	58.	0.07	0.72	0.051	0.03	0.70	0.00	0.049
686	15.71	15.71	0.95	1.90	0.00	61.	0.06	0.76	0.054	0.03	0.74	0.00	0.053
687	15.71	15.71	0.00	0.16	0.00	5.	0.02	0.03	0.002	0.09	0.03	0.00	0.002
688	15.71	15.71	0.00	0.15	0.00	5.	0.04	0.02	0.001	0.09	0.02	0.00	0.002
689	15.71	15.71	1.27	0.83	0.00	28.	0.12	0.42	0.029	0.02	0.41	0.00	0.029
690	15.71	15.71	1.15	0.79	0.00	26.	0.11	0.39	0.027	0.02	0.38	0.00	0.027
691	15.71	15.71	1.22	1.47	0.00	48.	0.05	0.64	0.045	0.05	0.64	0.00	0.045
692	15.71	15.71	1.22	1.47	0.00	48.	0.05	0.64	0.045	0.05	0.64	0.00	0.045
693	15.71	15.71	1.01	2.03	0.00	66.	0.05	0.81	0.058	0.04	0.80	0.00	0.057
694	15.71	15.71	1.01	2.03	0.00	65.	0.05	0.81	0.057	0.04	0.79	0.00	0.056
695	15.71	15.71	0.58	2.50	0.00	80.	0.03	0.87	0.061	0.05	0.84	0.00	0.059
696	15.71	15.71	0.58	2.50	0.00	80.	0.03	0.87	0.061	0.05	0.84	0.00	0.059
697	15.71	15.71	0.88	3.17	0.00	102.	0.08	1.18	0.084	0.03	1.14	0.00	0.081
698	15.71	15.71	0.88	3.19	0.00	103.	0.08	1.18	0.084	0.03	1.15	0.00	0.082
699	15.71	15.71	0.97	0.69	0.00	23.	0.10	0.34	0.024	0.03	0.33	0.00	0.023
700	15.71	15.71	1.22	1.47	0.00	48.	0.05	0.64	0.045	0.05	0.64	0.00	0.045
701	15.71	15.71	1.01	2.04	0.00	66.	0.05	0.81	0.058	0.04	0.80	0.00	0.057
702	15.71	15.71	0.88	3.15	0.00	101.	0.08	1.17	0.083	0.03	1.13	0.00	0.080
703	15.71	15.71	0.58	2.50	0.00	80.	0.03	0.87	0.061	0.05	0.84	0.00	0.059
704	15.71	15.71	0.00	0.46	0.00	15.	0.05	0.05	0.003	0.09	0.06	0.00	0.004

ARMATURA SUPERIORE VERTICALE

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
644	15.71	15.71	0.68	0.52	0.00	17.	0.12	0.16	0.011	0.02	0.15	0.00	0.011
649	15.71	15.71	0.68	0.52	0.00	17.	0.12	0.16	0.011	0.02	0.15	0.00	0.011
653	15.71	15.71	0.62	0.54	0.00	18.	0.11	0.17	0.012	0.02	0.16	0.00	0.011
656	15.71	15.71	0.62	0.54	0.00	18.	0.11	0.17	0.012	0.02	0.16	0.00	0.011
671	15.71	15.71	1.68	3.50	0.00	113.	0.33	1.15	0.081	0.03	1.09	0.00	0.078
675	15.71	15.71	1.67	3.52	0.00	114.	0.32	1.16	0.082	0.03	1.10	0.00	0.078
676	15.71	15.71	1.66	3.55	0.00	115.	0.32	1.16	0.082	0.03	1.11	0.00	0.079
680	15.71	15.71	1.68	3.48	0.00	112.	0.33	1.14	0.081	0.03	1.08	0.00	0.077
683	15.71	15.71	0.08	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
684	15.71	15.71	0.20	0.09	0.00	3.	0.03	0.01	0.001	0.01	0.01	0.00	0.001
685	15.71	15.71	0.08	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
686	15.71	15.71	0.20	0.09	0.00	3.	0.03	0.01	0.001	0.01	0.01	0.00	0.001
687	15.71	15.71	1.57	3.24	0.00	105.	0.28	1.01	0.071	0.06	0.97	0.00	0.069

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
688	15.71	15.71	1.60	2.82	0.00	91.	0.24	0.81	0.057	0.08	0.78	0.00	0.055
689	15.71	15.71	1.57	3.16	0.00	102.	0.26	1.01	0.071	0.05	0.96	0.00	0.068
690	15.71	15.71	1.69	2.84	0.00	92.	0.20	0.86	0.061	0.04	0.83	0.00	0.059
691	15.71	15.71	1.61	2.57	0.00	83.	0.23	0.77	0.054	0.06	0.74	0.00	0.052
692	15.71	15.71	1.57	3.14	0.00	101.	0.27	0.99	0.070	0.05	0.94	0.00	0.067
693	15.71	15.71	1.60	2.55	0.00	83.	0.23	0.76	0.054	0.06	0.73	0.00	0.052
694	15.71	15.71	1.57	3.14	0.00	101.	0.27	0.99	0.070	0.05	0.94	0.00	0.067
695	15.71	15.71	1.60	2.56	0.00	83.	0.23	0.76	0.054	0.06	0.74	0.00	0.052
696	15.71	15.71	1.56	3.14	0.00	101.	0.27	0.99	0.070	0.05	0.94	0.00	0.067
697	15.71	15.71	1.60	2.55	0.00	83.	0.23	0.76	0.054	0.06	0.73	0.00	0.052
698	15.71	15.71	1.57	3.14	0.00	101.	0.27	0.99	0.070	0.05	0.94	0.00	0.067
699	15.71	15.71	1.90	2.72	0.00	88.	0.16	0.72	0.051	0.03	0.77	0.00	0.054
700	15.71	15.71	1.83	2.40	0.00	78.	0.25	0.61	0.043	0.07	0.65	0.00	0.046
701	15.71	15.71	1.79	2.24	0.00	73.	0.27	0.57	0.040	0.08	0.61	0.00	0.043
702	15.71	15.71	1.79	2.24	0.00	73.	0.27	0.57	0.040	0.08	0.61	0.00	0.043
703	15.71	15.71	1.80	2.30	0.00	75.	0.28	0.57	0.040	0.09	0.62	0.00	0.044
704	15.71	15.71	1.78	2.45	0.00	80.	0.34	0.55	0.039	0.12	0.61	0.00	0.043

6.7. BLOCCO ANCORAGGIO 02



6.7.1. Verifica SLU

		INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
729	0.8	15.71	15.71	1.	1.	0.00	0.10	15.71	15.71	0.	3.	0.00	0.51
730	0.8	15.71	15.71	0.	5.	0.00	0.78	15.71	15.71	0.	3.	0.00	0.49
731	0.8	15.71	15.71	0.	5.	0.00	0.71	15.71	15.71	0.	3.	0.00	0.47
732	0.8	15.71	15.71	1.	3.	0.00	0.43	15.71	15.71	0.	3.	0.00	0.47
733	0.8	15.71	15.71	1.	2.	0.00	0.30	15.71	15.71	1.	3.	0.00	0.53
734	0.8	15.71	15.71	1.	1.	0.00	0.17	15.71	15.71	1.	4.	0.00	0.57
735	0.8	15.71	15.71	0.	5.	0.00	0.71	15.71	15.71	0.	6.	0.00	0.88
736	0.8	15.71	15.71	1.	3.	0.00	0.43	15.71	15.71	0.	6.	0.00	0.88
737	0.8	15.71	15.71	1.	2.	0.00	0.30	15.71	15.71	0.	6.	0.00	0.89
738	0.8	15.71	15.71	0.	5.	0.00	0.78	15.71	15.71	0.	6.	0.00	0.87
739	0.8	15.71	15.71	0.	4.	0.00	0.57	15.71	15.71	0.	0.	0.00	0.00
740	0.8	15.71	15.71	0.	2.	0.00	0.36	15.71	15.71	0.	0.	0.00	0.00
741	0.8	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	0.	4.	0.00	0.66
742	0.8	15.71	15.71	1.	1.	0.00	0.09	15.71	15.71	0.	4.	0.00	0.59
743	0.8	15.71	15.71	1.	1.	0.00	0.17	15.71	15.71	0.	4.	0.00	0.64
744	0.8	15.71	15.71	1.	1.	0.00	0.17	15.71	15.71	0.	4.	0.00	0.59
745	0.8	15.71	15.71	1.	2.	0.00	0.30	15.71	15.71	0.	4.	0.00	0.56
746	0.8	15.71	15.71	1.	2.	0.00	0.30	15.71	15.71	0.	4.	0.00	0.65
747	0.8	15.71	15.71	1.	3.	0.00	0.43	15.71	15.71	0.	4.	0.00	0.65
748	0.8	15.71	15.71	0.	5.	0.00	0.78	15.71	15.71	0.	4.	0.00	0.55
749	0.8	15.71	15.71	0.	5.	0.00	0.78	15.71	15.71	0.	4.	0.00	0.65
750	0.8	15.71	15.71	0.	5.	0.00	0.71	15.71	15.71	0.	4.	0.00	0.65
751	0.8	15.71	15.71	0.	5.	0.00	0.78	15.71	15.71	1.	1.	0.00	0.11
752	0.8	15.71	15.71	0.	5.	0.00	0.71	15.71	15.71	1.	1.	0.00	0.12
753	0.8	15.71	15.71	0.	4.	0.00	0.67	15.71	15.71	0.	0.	0.00	0.02
754	0.8	15.71	15.71	1.	2.	0.00	0.29	15.71	15.71	1.	1.	0.00	0.11
755	0.8	15.71	15.71	1.	3.	0.00	0.43	15.71	15.71	1.	1.	0.00	0.12
756	0.8	15.71	15.71	1.	3.	0.00	0.42	15.71	15.71	0.	0.	0.00	0.02
757	0.8	15.71	15.71	1.	3.	0.00	0.43	15.71	15.71	0.	3.	0.00	0.53
758	0.8	15.71	15.71	0.	5.	0.00	0.71	15.71	15.71	0.	3.	0.00	0.53

		SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
729	0.8	15.71	15.71	1.	1.	0.00	0.10	15.71	15.71	4.	3.	0.00	0.53
730	0.8	15.71	15.71	1.	5.	0.00	0.78	15.71	15.71	3.	3.	0.00	0.51
731	0.8	15.71	15.71	1.	5.	0.00	0.71	15.71	15.71	3.	3.	0.00	0.48
732	0.8	15.71	15.71	0.	3.	0.00	0.43	15.71	15.71	3.	3.	0.00	0.48
733	0.8	15.71	15.71	0.	2.	0.00	0.29	15.71	15.71	3.	3.	0.00	0.54
734	0.8	15.71	15.71	0.	1.	0.00	0.17	15.71	15.71	3.	4.	0.00	0.58
735	0.8	15.71	15.71	1.	5.	0.00	0.71	15.71	15.71	2.	6.	0.00	0.89
736	0.8	15.71	15.71	0.	3.	0.00	0.43	15.71	15.71	2.	6.	0.00	0.89
737	0.8	15.71	15.71	0.	2.	0.00	0.29	15.71	15.71	2.	6.	0.00	0.90
738	0.8	15.71	15.71	1.	5.	0.00	0.79	15.71	15.71	2.	6.	0.00	0.88
739	0.8	15.71	15.71	1.	4.	0.00	0.57	15.71	15.71	0.	0.	0.00	0.00
740	0.8	15.71	15.71	1.	2.	0.00	0.36	15.71	15.71	0.	0.	0.00	0.00
741	0.8	15.71	15.71	0.	0.	0.00	0.04	15.71	15.71	3.	4.	0.00	0.67
742	0.8	15.71	15.71	0.	1.	0.00	0.09	15.71	15.71	3.	4.	0.00	0.61
743	0.8	15.71	15.71	0.	1.	0.00	0.17	15.71	15.71	3.	4.	0.00	0.66
744	0.8	15.71	15.71	0.	1.	0.00	0.17	15.71	15.71	3.	4.	0.00	0.60
745	0.8	15.71	15.71	0.	2.	0.00	0.29	15.71	15.71	3.	4.	0.00	0.58
746	0.8	15.71	15.71	0.	2.	0.00	0.29	15.71	15.71	3.	4.	0.00	0.66
747	0.8	15.71	15.71	0.	3.	0.00	0.43	15.71	15.71	3.	4.	0.00	0.66
748	0.8	15.71	15.71	1.	5.	0.00	0.78	15.71	15.71	3.	4.	0.00	0.56
749	0.8	15.71	15.71	1.	5.	0.00	0.78	15.71	15.71	3.	4.	0.00	0.66
750	0.8	15.71	15.71	1.	5.	0.00	0.71	15.71	15.71	3.	4.	0.00	0.66
751	0.8	15.71	15.71	1.	5.	0.00	0.78	15.71	15.71	1.	1.	0.00	0.11
752	0.8	15.71	15.71	1.	5.	0.00	0.71	15.71	15.71	1.	1.	0.00	0.12
753	0.8	15.71	15.71	1.	4.	0.00	0.68	15.71	15.71	1.	0.	0.00	0.02
754	0.8	15.71	15.71	1.	2.	0.00	0.28	15.71	15.71	1.	1.	0.00	0.11
755	0.8	15.71	15.71	0.	3.	0.00	0.43	15.71	15.71	1.	1.	0.00	0.12
756	0.8	15.71	15.71	1.	3.	0.00	0.42	15.71	15.71	1.	0.	0.00	0.02
757	0.8	15.71	15.71	0.	3.	0.00	0.43	15.71	15.71	3.	3.	0.00	0.54
758	0.8	15.71	15.71	1.	5.	0.00	0.71	15.71	15.71	3.	3.	0.00	0.54

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO (Rd > Ed)

6.7.2. Verifica SLE fessurazione

ARMATURA INFERIORE ORIZZONTALE

			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP	
729	15.71	15.71	0.31	0.46	0.00	15.	0.11	0.07	0.005	0.09	0.06	0.00	0.004	
730	15.71	15.71	0.75	2.47	0.00	79.	0.37	0.86	0.061	0.06	0.84	0.00	0.059	
731	15.71	15.71	0.24	3.08	0.00	98.	0.13	1.05	0.075	0.03	1.13	0.00	0.080	
732	15.71	15.71	0.17	1.93	0.00	61.	0.10	0.75	0.053	0.04	0.80	0.00	0.057	
733	15.71	15.71	0.19	1.39	0.00	44.	0.07	0.60	0.043	0.05	0.64	0.00	0.045	
734	15.71	15.71	0.15	0.66	0.00	21.	0.05	0.32	0.022	0.03	0.33	0.00	0.023	
735	15.71	15.71	0.24	3.13	0.00	100.	0.13	1.07	0.076	0.03	1.15	0.00	0.082	
736	15.71	15.71	0.16	1.92	0.00	61.	0.10	0.74	0.053	0.04	0.79	0.00	0.056	
737	15.71	15.71	0.13	1.36	0.00	43.	0.05	0.59	0.042	0.05	0.62	0.00	0.044	
738	15.71	15.71	0.65	3.60	0.00	115.	0.35	1.23	0.087	0.05	1.21	0.00	0.086	
739	15.71	15.71	0.17	2.77	0.00	88.	0.11	0.95	0.068	0.02	1.03	0.00	0.073	
740	15.71	15.71	0.14	1.68	0.00	54.	0.10	0.65	0.046	0.03	0.70	0.00	0.049	

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
741	15.71	15.71	0.26	0.16	0.00	5.	0.14	0.03	0.002	0.09	0.03	0.00	0.002
742	15.71	15.71	0.28	0.15	0.00	5.	0.13	0.03	0.002	0.10	0.02	0.00	0.002
743	15.71	15.71	0.08	0.79	0.00	25.	0.00	0.39	0.028	0.02	0.41	0.00	0.029
744	15.71	15.71	0.09	0.75	0.00	24.	0.01	0.36	0.026	0.02	0.38	0.00	0.027
745	15.71	15.71	0.19	1.39	0.00	44.	0.07	0.60	0.043	0.05	0.64	0.00	0.045
746	15.71	15.71	0.19	1.39	0.00	44.	0.07	0.60	0.043	0.05	0.64	0.00	0.045
747	15.71	15.71	0.16	1.92	0.00	61.	0.10	0.74	0.053	0.04	0.79	0.00	0.056
748	15.71	15.71	0.75	2.47	0.00	79.	0.37	0.86	0.061	0.06	0.84	0.00	0.059
749	15.71	15.71	0.75	2.47	0.00	79.	0.37	0.86	0.061	0.06	0.84	0.00	0.059
750	15.71	15.71	0.24	3.13	0.00	100.	0.13	1.07	0.076	0.03	1.15	0.00	0.082
751	15.71	15.71	0.71	3.82	0.00	122.	0.30	1.28	0.091	0.04	1.29	0.00	0.092
752	15.71	15.71	0.24	3.13	0.00	100.	0.13	1.07	0.076	0.03	1.15	0.00	0.082
753	15.71	15.71	0.22	2.94	0.00	94.	0.12	1.00	0.071	0.03	1.08	0.00	0.077
754	15.71	15.71	0.10	1.33	0.00	43.	0.04	0.58	0.041	0.05	0.61	0.00	0.043
755	15.71	15.71	0.16	1.90	0.00	61.	0.10	0.74	0.052	0.04	0.79	0.00	0.056
756	15.71	15.71	0.16	1.79	0.00	57.	0.10	0.70	0.049	0.04	0.74	0.00	0.053
757	15.71	15.71	0.17	1.92	0.00	61.	0.10	0.75	0.053	0.04	0.80	0.00	0.057
758	15.71	15.71	0.24	3.11	0.00	99.	0.13	1.06	0.075	0.03	1.14	0.00	0.081

ARMATURA INFERIORE VERTICALE

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
729	15.71	15.71	0.00	2.36	0.00	75.	0.00	0.55	0.039	0.11	0.61	0.00	0.043
730	15.71	15.71	0.00	2.22	0.00	71.	0.00	0.56	0.040	0.08	0.62	0.00	0.044
731	15.71	15.71	0.00	2.16	0.00	69.	0.00	0.55	0.039	0.07	0.61	0.00	0.043
732	15.71	15.71	0.00	2.16	0.00	69.	0.00	0.55	0.039	0.07	0.61	0.00	0.043
733	15.71	15.71	0.00	2.31	0.00	74.	0.00	0.59	0.042	0.06	0.65	0.00	0.046
734	15.71	15.71	0.00	2.61	0.00	83.	0.00	0.69	0.049	0.02	0.77	0.00	0.054
735	15.71	15.71	0.00	3.43	0.00	109.	0.05	1.10	0.078	0.03	1.09	0.00	0.078
736	15.71	15.71	0.00	3.45	0.00	110.	0.05	1.11	0.079	0.03	1.10	0.00	0.078
737	15.71	15.71	0.00	3.47	0.00	111.	0.05	1.11	0.079	0.03	1.11	0.00	0.079
738	15.71	15.71	0.00	3.40	0.00	108.	0.05	1.09	0.077	0.03	1.08	0.00	0.077
739	15.71	15.71	0.05	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
740	15.71	15.71	0.05	-0.02	0.00	0.	0.01	-0.02	0.000	0.00	-0.02	0.00	0.000
741	15.71	15.71	0.00	3.14	0.00	100.	0.00	0.95	0.067	0.05	0.97	0.00	0.069
742	15.71	15.71	0.00	2.73	0.00	87.	0.00	0.73	0.052	0.08	0.78	0.00	0.055
743	15.71	15.71	0.00	3.06	0.00	97.	0.00	0.93	0.066	0.04	0.96	0.00	0.068
744	15.71	15.71	0.00	2.74	0.00	87.	0.00	0.78	0.055	0.04	0.83	0.00	0.059
745	15.71	15.71	0.00	2.48	0.00	79.	0.00	0.70	0.050	0.06	0.74	0.00	0.052
746	15.71	15.71	0.00	3.03	0.00	97.	0.00	0.93	0.066	0.05	0.94	0.00	0.067
747	15.71	15.71	0.00	3.04	0.00	97.	0.00	0.94	0.066	0.05	0.94	0.00	0.067
748	15.71	15.71	0.00	2.48	0.00	79.	0.00	0.69	0.049	0.06	0.74	0.00	0.052
749	15.71	15.71	0.00	3.04	0.00	97.	0.00	0.94	0.066	0.05	0.94	0.00	0.067
750	15.71	15.71	0.00	3.04	0.00	97.	0.00	0.94	0.067	0.05	0.94	0.00	0.067
751	15.71	15.71	0.72	0.50	0.00	16.	0.23	0.14	0.010	0.02	0.15	0.00	0.011
752	15.71	15.71	0.67	0.52	0.00	17.	0.21	0.15	0.010	0.02	0.16	0.00	0.011
753	15.71	15.71	0.18	0.08	0.00	3.	0.05	0.00	0.000	0.01	0.01	0.00	0.001
754	15.71	15.71	0.72	0.50	0.00	16.	0.23	0.14	0.010	0.02	0.15	0.00	0.011
755	15.71	15.71	0.67	0.52	0.00	17.	0.21	0.15	0.010	0.02	0.16	0.00	0.011
756	15.71	15.71	0.18	0.08	0.00	3.	0.05	0.00	0.000	0.01	0.01	0.00	0.001
757	15.71	15.71	0.00	2.47	0.00	79.	0.00	0.69	0.049	0.06	0.73	0.00	0.052
758	15.71	15.71	0.00	2.47	0.00	79.	0.00	0.69	0.049	0.06	0.73	0.00	0.052

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
729	15.71	15.71	0.01	0.46	0.00	15.	0.00	0.07	0.005	0.03	0.06	0.00	0.005
730	15.71	15.71	0.49	2.47	0.00	79.	0.23	0.86	0.061	0.07	0.84	0.00	0.059
731	15.71	15.71	0.73	3.08	0.00	99.	0.33	1.05	0.074	0.07	1.13	0.00	0.080
732	15.71	15.71	0.55	1.93	0.00	62.	0.33	0.75	0.053	0.07	0.80	0.00	0.057
733	15.71	15.71	0.24	1.39	0.00	44.	0.29	0.60	0.042	0.05	0.64	0.00	0.045
734	15.71	15.71	0.00	0.66	0.00	21.	0.14	0.32	0.022	0.00	0.33	0.00	0.024
735	15.71	15.71	0.74	3.13	0.00	100.	0.33	1.07	0.075	0.07	1.15	0.00	0.082
736	15.71	15.71	0.55	1.92	0.00	62.	0.33	0.74	0.052	0.07	0.79	0.00	0.056
737	15.71	15.71	0.33	1.36	0.00	44.	0.31	0.59	0.041	0.05	0.62	0.00	0.044
738	15.71	15.71	0.81	3.60	0.00	115.	0.31	1.23	0.087	0.07	1.21	0.00	0.086
739	15.71	15.71	0.64	2.77	0.00	89.	0.31	0.95	0.067	0.07	1.03	0.00	0.073
740	15.71	15.71	0.57	1.68	0.00	54.	0.30	0.65	0.046	0.07	0.70	0.00	0.049
741	15.71	15.71	0.00	0.16	0.00	5.	0.00	0.03	0.002	0.01	0.03	0.00	0.002
742	15.71	15.71	0.00	0.15	0.00	5.	0.00	0.03	0.002	0.02	0.02	0.00	0.002
743	15.71	15.71	0.10	0.79	0.00	25.	0.25	0.39	0.027	0.01	0.41	0.00	0.029
744	15.71	15.71	0.00	0.75	0.00	24.	0.21	0.36	0.025	0.00	0.38	0.00	0.027
745	15.71	15.71	0.24	1.39	0.00	44.	0.29	0.60	0.042	0.05	0.64	0.00	0.045
746	15.71	15.71	0.24	1.39	0.00	44.	0.29	0.60	0.042	0.05	0.64	0.00	0.045
747	15.71	15.71	0.55	1.92	0.00	62.	0.33	0.74	0.052	0.07	0.79	0.00	0.056
748	15.71	15.71	0.49	2.47	0.00	79.	0.23	0.86	0.061	0.07	0.84	0.00	0.059
749	15.71	15.71	0.49	2.47	0.00	79.	0.23	0.86	0.061	0.07	0.84	0.00	0.059
750	15.71	15.71	0.74	3.13	0.00	100.	0.33	1.07	0.075	0.07	1.15	0.00	0.082
751	15.71	15.71	1.05	3.82	0.00	123.	0.38	1.28	0.091	0.07	1.29	0.00	0.092
752	15.71	15.71	0.74	3.13	0.00	100.	0.33	1.07	0.075	0.07	1.15	0.00	0.082
753	15.71	15.71	0.70	2.94	0.00	94.	0.32	1.00	0.071	0.07	1.08	0.00	0.077
754	15.71	15.71	0.42	1.33	0.00	43.	0.33	0.58	0.041	0.06	0.61	0.00	0.043
755	15.71	15.71	0.56	1.90	0.00	61.	0.33	0.74	0.052	0.07	0.79	0.00	0.056
756	15.71	15.71	0.56	1.79	0.00	58.	0.32	0.70	0.049	0.07	0.74	0.00	0.053
757	15.71	15.71	0.55	1.92	0.00	62.	0.33	0.75	0.053	0.07	0.80	0.00	0.056

			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
758	15.71	15.71	0.74	3.11	0.00	100.	0.33	1.06	0.075	0.07	1.14	0.00	0.081

ARMATURA SUPERIORE VERTICALE

			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
729	15.71	15.71	2.09	2.36	0.00	77.	0.66	0.55	0.038	0.07	0.61	0.00	0.043
730	15.71	15.71	1.84	2.22	0.00	72.	0.64	0.56	0.039	0.08	0.62	0.00	0.044
731	15.71	15.71	1.77	2.16	0.00	70.	0.63	0.55	0.039	0.08	0.61	0.00	0.043
732	15.71	15.71	1.77	2.16	0.00	70.	0.63	0.55	0.039	0.08	0.61	0.00	0.043
733	15.71	15.71	1.74	2.31	0.00	75.	0.64	0.59	0.042	0.09	0.65	0.00	0.046
734	15.71	15.71	1.55	2.61	0.00	85.	0.67	0.69	0.048	0.13	0.77	0.00	0.054
735	15.71	15.71	2.02	3.43	0.00	111.	0.59	1.10	0.077	0.04	1.09	0.00	0.078
736	15.71	15.71	2.01	3.45	0.00	112.	0.59	1.11	0.078	0.04	1.10	0.00	0.078
737	15.71	15.71	2.00	3.47	0.00	112.	0.58	1.11	0.079	0.04	1.11	0.00	0.079
738	15.71	15.71	2.02	3.40	0.00	110.	0.59	1.09	0.077	0.04	1.08	0.00	0.077
739	15.71	15.71	0.09	-0.02	0.00	0.	0.03	-0.02	0.000	0.00	-0.02	0.00	0.000
740	15.71	15.71	0.09	-0.02	0.00	0.	0.03	-0.02	0.000	0.00	-0.02	0.00	0.000
741	15.71	15.71	1.77	3.14	0.00	102.	0.54	0.95	0.067	0.05	0.97	0.00	0.069
742	15.71	15.71	1.81	2.73	0.00	89.	0.57	0.73	0.052	0.06	0.78	0.00	0.055
743	15.71	15.71	1.68	3.06	0.00	99.	0.54	0.93	0.066	0.06	0.96	0.00	0.068
744	15.71	15.71	1.60	2.74	0.00	89.	0.59	0.78	0.055	0.09	0.83	0.00	0.059
745	15.71	15.71	1.64	2.48	0.00	81.	0.56	0.70	0.049	0.07	0.74	0.00	0.052
746	15.71	15.71	1.74	3.03	0.00	98.	0.54	0.93	0.066	0.05	0.94	0.00	0.067
747	15.71	15.71	1.73	3.04	0.00	98.	0.54	0.94	0.066	0.05	0.94	0.00	0.067
748	15.71	15.71	1.64	2.48	0.00	80.	0.56	0.69	0.049	0.07	0.74	0.00	0.052
749	15.71	15.71	1.73	3.04	0.00	98.	0.53	0.94	0.066	0.05	0.94	0.00	0.067
750	15.71	15.71	1.73	3.04	0.00	98.	0.54	0.94	0.066	0.05	0.94	0.00	0.067
751	15.71	15.71	0.76	0.50	0.00	17.	0.24	0.14	0.010	0.03	0.15	0.00	0.011
752	15.71	15.71	0.69	0.52	0.00	17.	0.22	0.15	0.010	0.02	0.16	0.00	0.011
753	15.71	15.71	0.20	0.08	0.00	3.	0.07	0.00	0.000	0.01	0.01	0.00	0.001
754	15.71	15.71	0.76	0.50	0.00	17.	0.24	0.14	0.010	0.03	0.15	0.00	0.011
755	15.71	15.71	0.69	0.52	0.00	17.	0.22	0.15	0.010	0.02	0.16	0.00	0.011
756	15.71	15.71	0.20	0.08	0.00	3.	0.07	0.00	0.000	0.01	0.01	0.00	0.001
757	15.71	15.71	1.64	2.47	0.00	80.	0.56	0.69	0.049	0.07	0.73	0.00	0.052
758	15.71	15.71	1.64	2.47	0.00	80.	0.56	0.69	0.049	0.07	0.73	0.00	0.052

7. VERIFICHE GEOTECNICHE

Il calcolo della capacità portante viene eseguito secondo la formula trinomia, considerando separatamente i contributi dovuti alla coesione, al sovraccarico laterale ed al peso del terreno.

Per le verifiche in condizioni drenate, si utilizzano i coefficienti di capacità portante N_q (Prandtl, 1921), N_c (Reissner, 1924), N_γ (Vesic, 1973), i coefficienti correttivi dovuti alla forma della fondazione (s , Meyerhof, 1951 e 1963), all'approfondimento (d , Brinch Hansen, 1970), all'inclinazione del carico (i , Vesic, 1973), all'inclinazione del piano di posa (b , Vesic, 1973), all'inclinazione del piano campagna (g , Vesic, 1973).

Nel caso di terreno eterogeneo (litologie differenti, presenza di falda), i parametri meccanici utilizzati nel calcolo sono ottenuti come media ponderata dei valori rinvenuti all'interno del cuneo di rottura.

La resistenza a scorrimento, viene ottenuta sommando i contributi del carico normale al piano di posa moltiplicato per il coefficiente d'attrito, e dell'area del piano di posa (eventualmente ridotta per carico verticale eccentrico) per l'adesione fondazione-terreno. In condizioni drenate, l'attrito fondazione terreno è assunto pari all'angolo di resistenza al taglio del terreno moltiplicato per il coefficiente 0.75, l'adesione fondazione terreno è trascurata (assunta pari a 0). Si considera il contributo della pressione del terreno a lato della fondazione. La resistenza laterale del terreno è assunta pari alla resistenza passiva disponibile moltiplicata per 0.50.

Il cedimento di una fondazione nastriforme su suolo sabbioso viene valutato utilizzando il metodo di seguito descritto. Il metodo di Burland e Burbidge (1985), utilizza i dati raccolti con una prova SPT. Il valore medio di N_{spt} , entro la profondità di influenza al di sotto della base della fondazione, viene utilizzato per valutare un indice di compressibilità, che con il sovraccarico applicato e le dimensioni della fondazione concorre a valutare il cedimento totale.

Si verifica che il cedimento immediato sia minore di 0.04 [m], e che il cedimento a lungo termine sia minore di 0.05 [m].

7.1. DESCRIZIONE DEL TERRENO

La stratigrafia è eterogenea, presenta 2 strati							
n.	nome	z_i [m]	z_f [m]	γ_d [kN/m ³]	γ_t [kN/m ³]	c' [N/mm ²]	ϕ' [°]
1	Orizzonte 1	0	-6	19	21.5	0	29
2	Orizzonte 2	-6	-20	18.5	21.5	0	37
La stratigrafia non contiene una falda							

7.2. PLATEA INFERIORE

7.3. DESCRIZIONE DELLA FONDAZIONE

La fondazione ha piano di posa rettangolare, con lato X di 3.7 [m], lato Y di 4.8 [m], e centro alla quota $z = -5.9$ [m]. Il piano di posa è orizzontale.

7.3.1. Sollecitazioni al piano di posa.

Si riportano di seguito le componenti della sollecitazione applicata e la distanza del punto di applicazione dal centro del piano di posa della fondazione.

Rispetto al sistema di rif. globale:								
Caso	Fx [kN]	Fy [kN]	Fz [kN]	Mx [kN*m]	My [kN*m]	dx [m]	dy [m]	dz [m]
1-1	-627.52	0.5372	-4419.6712	-0.1522	-1993.2416	0	0	0.6
2-1	-252.92	65.3799	-3967.5212	-432.1889	-1045.0596	0	0	0.6
3-1	-419.43	23.631	-3525.6212	27.1371	-1147.8191	0	0	0.6
4-1	-526.03	65.9606	-3822.9412	-435.9851	-1481.5801	0	0	0.6
5-1	-419.63	70.799	-3525.7012	-425.6798	-1148.6891	0	0	0.6
6-1	-627.48	65.2193	-4419.0412	-434.6307	-1993.3432	0	0	0.6
Rispetto al sistema di rif. locale (centro piano di posa):								
Caso	Hx [kN]	Hy [kN]	Vz [kN]	Mx [kN*m]	My [kN*m]	dx [m]	dy [m]	dz [m]
1-1	-627.52	0.5372	-4419.6712	-0.4745	-2369.7536	-	-	-
2-1	-252.92	65.3799	-3967.5212	-471.4168	-1196.8116	-	-	-
3-1	-419.43	23.631	-3525.6212	12.9585	-1399.4771	-	-	-
4-1	-526.03	65.9606	-3822.9412	-475.5615	-1797.1981	-	-	-
5-1	-419.63	70.799	-3525.7012	-468.1592	-1400.4671	-	-	-
6-1	-627.48	65.2193	-4419.0412	-473.7623	-2369.8312	-	-	-

Le sollecitazioni applicate provocano un' eccentricità lungo X (max = 0.5363 [m]) e lungo Y (max = 0.1328 [m]), perciò le verifiche vengono eseguite sulla fondazione ridotta rettangolare.

Caso	ecc. X [m]	ecc. Y [m]	Asse B	Asse L
1-1	0.5362	0.0001	asse X	asse Y
2-1	0.3017	0.1188	asse X	asse Y
3-1	0.3969	0.0037	asse X	asse Y
4-1	0.4701	0.1244	asse X	asse Y
5-1	0.3972	0.1328	asse X	asse Y
6-1	0.5363	0.1072	asse X	asse Y

7.3.2. Capacità portante.

Le seguenti tabelle elencano il valore dell'angolo di resistenza al taglio, del peso di volume alleggerito, della coesione efficace, del sovraccarico alleggerito, e dei fattori e coefficienti introdotti nel calcolo della capacità portante.

Caso	γ_ϕ	γ_γ	ϕ [°]	γ' [kN/m³]	N_γ	S_γ	d_γ	$i_{b\gamma}$	$i_{i\gamma}$	b_γ	g_γ	$q'_{lim,\gamma}$ [N/mm²]
1-1	1.00	1.00	36.4	18.5	60.02	1.21	1.00	0.67	1.00	1.00	1.00	1.184
2-1	1.00	1.00	36.5	18.5	60.91	1.27	1.00	0.84	0.96	1.00	1.00	1.793
3-1	1.00	1.00	36.5	18.5	60.58	1.24	1.00	0.72	0.98	1.00	1.00	1.426
4-1	1.00	1.00	36.4	18.5	60.30	1.24	1.00	0.68	0.96	1.00	1.00	1.242
5-1	1.00	1.00	36.5	18.5	60.58	1.25	1.00	0.72	0.95	1.00	1.00	1.397

6-1	1.00	1.00	36.4	18.5	60.02	1.22	1.00	0.67	0.97	1.00	1.00	1.154
Caso	γ_c'	c' [N/mm ²]	N_c	S_c	d_c	i_{bc}	i_{ic}	b_c	g_c	$q'_{lim,c}$ [N/mm ²]		
1-1	1.00	0	52.51	1.43	1.29	0.77	1.00	1.00	1.00	0		
2-1	1.00	0	52.97	1.53	1.27	0.90	0.98	1.00	1.00	0		
3-1	1.00	0	52.80	1.48	1.28	0.81	0.99	1.00	1.00	0		
4-1	1.00	0	52.65	1.48	1.28	0.78	0.98	1.00	1.00	0		
5-1	1.00	0	52.80	1.50	1.28	0.81	0.97	1.00	1.00	0		
6-1	1.00	0	52.51	1.45	1.29	0.77	0.98	1.00	1.00	0		
Caso	q' [N/mm ²]	N_q	S_q	d_q	i_{bq}	i_{iq}	b_q	g_q	$q'_{lim,q}$ [N/mm ²]			
1-1	0.112	39.71	1.21	1.28	0.78	1.00	1.00	1.00	5.381			
2-1	0.112	40.17	1.27	1.26	0.90	0.98	1.00	1.00	6.345			
3-1	0.112	40.00	1.24	1.27	0.81	0.99	1.00	1.00	5.693			
4-1	0.112	39.86	1.24	1.28	0.79	0.98	1.00	1.00	5.419			
5-1	0.112	40.00	1.25	1.27	0.82	0.97	1.00	1.00	5.655			
6-1	0.112	39.71	1.22	1.28	0.78	0.98	1.00	1.00	5.325			

Segue il confronto fra la pressione limite ed applicata.

Caso	$\gamma_{R,v}$	q'_{lim} [N/mm ²]	A [m ²]	R_d [kN]	E_d [kN]	Verifica
1-1	2.30	2.917	12.612077	36793.353	4419.671	SI (36793.353/4419.671 = 8.32 >= 1.0)
2-1	2.30	3.602	14.128246	50884.468	3967.521	SI (50884.468/3967.521 = 12.83 >= 1.0)
3-1	2.30	3.158	13.927967	43990.735	3525.621	SI (43990.735/3525.621 = 12.48 >= 1.0)
4-1	2.30	2.96	12.56034	37173.831	3822.941	SI (37173.831/3822.941 = 9.72 >= 1.0)
5-1	2.30	3.13	13.175091	41235.97	3525.701	SI (41235.97/3525.701 = 11.70 >= 1.0)
6-1	2.30	2.88	12.048365	34705.008	4419.041	SI (34705.008/4419.041 = 7.85 >= 1.0)

7.3.3. Scorrimento.

Le seguenti tabelle elencano il valore dell'angolo di resistenza al taglio, della coesione efficace, dell'attrito e dell'aderenza fondazione-terreno, e della resistenza disponibile sul piano di posa e sulle pareti laterali.

Caso	γ_ϕ	γ_c'	ϕ [°]	c' [N/mm ²]	δ [°]	a [N/mm ²]	$\gamma_{R,h}$	$\gamma_{R,e}$	R_h [kN]	R_e [kN]
1-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1602.9727	744.881
2-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1438.9822	862.6492
3-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1278.7093	775.1204
4-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1386.5444	809.1763
5-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1278.7383	828.3773
6-1	1.00	1.00	29	0	21.7	0	1.10	1.00	1602.7442	799.0404

Segue il confronto fra la resistenza a scorrimento e l'azione applicata.

Caso	R_d [kN]	E_d [kN]	Verifica
1-1	2347.854	627.52	SI (2347.854/627.52 = 3.74 >= 1.0)
2-1	2301.631	261.234	SI (2301.631/261.234 = 8.81 >= 1.0)
3-1	2053.83	420.095	SI (2053.83/420.095 = 4.89 >= 1.0)
4-1	2195.721	530.149	SI (2195.721/530.149 = 4.14 >= 1.0)
5-1	2107.116	425.561	SI (2107.116/425.561 = 4.95 >= 1.0)
6-1	2401.785	630.86	SI (2401.785/630.86 = 3.81 >= 1.0)

7.3.4. Sollecitazioni x verifiche cedimento in esercizio

Il calcolo è stato eseguito considerando le seguenti condizioni di carico, costituite da una sollecitazione di sforzo normale, applicata alla fondazione in corrispondenza del centro della base.

Numero	Nome	N [kN]
1	Caso 10-1	3577.22
2	Caso 11-1	3547.03
3	Caso 16-1	2238.51

7.3.5. Cedimenti.

Segue l'elenco dei cedimenti corrispondenti a ciascuna condizione di carico. I cedimenti differiti sono calcolati per un tempo di 30.0 anni.

Cond. di carico	Ced. immediato [m]	Ver.	Ced. differito [m]	Ver.
1) Caso 10-1 (Bur.&Bur.)	0.0151	SI	0.0226	-
2) Caso 11-1 (Bur.&Bur.)	0.0149	SI	0.0224	-
3) Caso 16-1 (Bur.&Bur.)	0.0066	-	0.01	SI

La tabella successiva riassume i risultati del calcolo col metodo di Burland e Burbridge per la condizione di carico 1, a cui corrisponde il cedimento immediato maggiore.

$$w = \sigma'_{vp} B^{0.7} I_c / 3 + (q' - \sigma'_{vp}) B^{0.7} I_c$$

Il cedimento w viene moltiplicato per f_s f_h f_t .

Simbolo	Valore	Descrizione
Z_{fon}	-5.8 [m]	Quota di base della fondazione
B	3.5 [m]	Larghezza della base della fondazione
Z_i	2.6098 [m]	Profondità di influenza
q'	0.222 [N/mm ²]	Carico unitario applicato
σ'_{v0}	0.11 [N/mm ²]	Tensione verticale geostatica alla quota della base
σ'_{vp}	0.111 [N/mm ²]	Tensione verticale di preconsolidazione alla quota della base
N	15	Valore medio di N_{spt} nella profondità di influenza
I_c	0.038	Indice di compressibilità
f_s	1.10	Coefficiente per la forma della fondazione
f_h	1.00	Coefficiente per l'altezza dello strato comprimibile (6 [m])
f_t	1.50	Coefficiente per il cedimento differito (30.0 anni)

Il cedimento immediato è pari a 0.0151 [m] (Verificato).

Il cedimento differito a 30.0 anni, nel caso di carichi statici, vale 0.0226 [m].

7.4. PLATEA SUPERIORE

- Descrizione della fondazione.

La fondazione ha piano di posa rettangolare, con lato X di 3.625 [m], lato Y di 4.8 [m], e centro alla quota $z = -0.1$ [m]. Il piano di posa è orizzontale.

7.4.1. Sollecitazioni al piano di posa.

Si riportano di seguito le componenti della sollecitazione applicata e la distanza del punto di applicazione dal centro del piano di posa della fondazione.

Rispetto al sistema di rif. globale:								
Caso	Fx [kN]	Fy [kN]	Fz [kN]	Mx [kN*m]	My [kN*m]	dx [m]	dy [m]	dz [m]
1-1	0	0	-33.718	0.1973	-47.0672	0	0	0.85
2-1	0	0	-200.138	-40.256	-25.1706	0	0	0.85
3-1	0	0	-421.768	-21.8811	40.2935	0	0	0.85
4-1	0	0	-264.038	-40.4023	3.5673	0	0	0.85
5-1	0	0	-421.758	-43.887	40.3133	0	0	0.85
6-1	0	0	-33.838	-39.7504	-46.822	0	0	0.85
Rispetto al sistema di rif. locale (centro piano di posa):								
Caso	Hx [kN]	Hy [kN]	Vz [kN]	Mx [kN*m]	My [kN*m]	dx [m]	dy [m]	dz [m]
1-1	0	0	-33.718	0.1973	-47.0672	-	-	-
2-1	0	0	-200.138	-40.256	-25.1706	-	-	-
3-1	0	0	-421.768	-21.8811	40.2935	-	-	-
4-1	0	0	-264.038	-40.4023	3.5673	-	-	-
5-1	0	0	-421.758	-43.887	40.3133	-	-	-
6-1	0	0	-33.838	-39.7504	-46.822	-	-	-

Le sollecitazioni applicate provocano un' eccentricità lungo X (max = 1.3959 [m]) e lungo Y (max = 1.1747 [m]), perciò le verifiche vengono eseguite sulla fondazione ridotta rettangolare.

Caso	ecc. X [m]	ecc. Y [m]	Asse B	Asse L
1-1	1.3959	0.0059	asse X	asse Y
2-1	0.1258	0.2011	asse X	asse Y
3-1	0.0955	0.0519	asse X	asse Y
4-1	0.0135	0.153	asse X	asse Y
5-1	0.0956	0.1041	asse X	asse Y
6-1	1.3837	1.1747	asse X	asse Y

7.4.2. Capacità portante.

Le seguenti tabelle elencano il valore dell'angolo di resistenza al taglio, del peso di volume alleggerito, della coesione efficace, del sovraccarico alleggerito, e dei fattori e coefficienti introdotti nel calcolo della capacità portante.

Caso	γ_ϕ	γ_γ	ϕ [°]	γ' [kN/m³]	N_γ	S_γ	d_γ	$i_{b\gamma}$	$i_{t\gamma}$	b_γ	g_γ	$q'_{lim,\gamma}$ [N/mm²]
1-1	1.00	1.00	29	19	19.34	1.05	1.00	1.00	1.00	1.00	1.00	0.161
2-1	1.00	1.00	29	19	19.34	1.22	1.00	1.00	1.00	1.00	1.00	0.757
3-1	1.00	1.00	29	19	19.34	1.21	1.00	1.00	1.00	1.00	1.00	0.764
4-1	1.00	1.00	29	19	19.34	1.23	1.00	1.00	1.00	1.00	1.00	0.814
5-1	1.00	1.00	29	19	19.34	1.22	1.00	1.00	1.00	1.00	1.00	0.767
6-1	1.00	1.00	29	19	19.34	1.10	1.00	1.00	1.00	1.00	1.00	0.173

Caso	γ_c	c' [N/mm ²]	N_c	S_c	d_c	i_{bc}	i_{ic}	b_c	g_c	$q'_{lim,c}$ [N/mm ²]
1-1	1.00	0	27.86	1.10	1.04	1.00	1.00	1.00	1.00	0
2-1	1.00	0	27.86	1.44	1.01	1.00	1.00	1.00	1.00	0
3-1	1.00	0	27.86	1.42	1.01	1.00	1.00	1.00	1.00	0
4-1	1.00	0	27.86	1.46	1.01	1.00	1.00	1.00	1.00	0
5-1	1.00	0	27.86	1.43	1.01	1.00	1.00	1.00	1.00	0
6-1	1.00	0	27.86	1.20	1.04	1.00	1.00	1.00	1.00	0
Caso	q' [N/mm ²]	N_q	S_q	d_q	i_{bq}	i_{iq}	b_q	g_q	$q'_{lim,q}$ [N/mm ²]	
1-1	0 (trascurato)	16.44	1.05	1.04	1.00	1.00	1.00	1.00	0	
2-1	0 (trascurato)	16.44	1.22	1.01	1.00	1.00	1.00	1.00	0	
3-1	0 (trascurato)	16.44	1.21	1.01	1.00	1.00	1.00	1.00	0	
4-1	0 (trascurato)	16.44	1.23	1.01	1.00	1.00	1.00	1.00	0	
5-1	0 (trascurato)	16.44	1.22	1.01	1.00	1.00	1.00	1.00	0	
6-1	0 (trascurato)	16.44	1.10	1.03	1.00	1.00	1.00	1.00	0	

Segue il confronto fra la pressione limite ed applicata.

Caso	$\gamma_{r,v}$	q'_{lim} [N/mm ²]	A [m ²]	R_d [kN]	E_d [kN]	Verifica
1-1	2.30	0.07	3.98954	278.819	33.718	SI (278.819/33.718 = 8.27 >= 1.0)
2-1	2.30	0.329	14.835558	4881.256	200.138	SI (4881.256/200.138 = 24.39 >= 1.0)
3-1	2.30	0.332	16.126565	5355.381	421.768	SI (5355.381/421.768 = 12.70 >= 1.0)
4-1	2.30	0.354	16.169195	5719.02	264.038	SI (5719.02/264.038 = 21.66 >= 1.0)
5-1	2.30	0.333	15.767763	5256.764	421.758	SI (5256.764/421.758 = 12.46 >= 1.0)
6-1	2.30	0.075	2.101537	158.471	33.838	SI (158.471/33.838 = 4.68 >= 1.0)

7.4.3. Sollecitazioni per la verifica cedimenti

Il calcolo è stato eseguito considerando le seguenti condizioni di carico, costituite da una sollecitazione di sforzo normale, applicata alla fondazione in corrispondenza del centro della base.

Numero	Nome	N [kN]
1	Caso 10-1	21.35
2	Caso 11-1	41.26
3	Caso 16-1	605.73

7.4.4. Cedimenti.

Segue l'elenco dei cedimenti corrispondenti a ciascuna condizione di carico. Per il metodo di Burland e Burbidge, i cedimenti differiti sono calcolati per un tempo di 30.0 anni. Per il metodo di Schmertmann, i cedimenti differiti sono calcolati per un tempo di 30.0 anni.

Cond. di carico	Ced. immediato [m]	Ver.	Ced. differito [m]	Ver.
1) Caso 10-1 (Bur.&Bur.)	0.0004	SI	0.0006	-
1) Caso 10-1 (Schmer.)	Errore nei dati.	-	Errore nei dati.	-
2) Caso 11-1 (Bur.&Bur.)	0.0008	SI	0.0012	-
2) Caso 11-1 (Schmer.)	Errore nei dati.	-	Errore nei dati.	-
3) Caso 16-1 (Bur.&Bur.)	0.0113	-	0.0169	SI
3) Caso 16-1 (Schmer.)	Errore nei dati.	-	Errore nei dati.	-

La tabella successiva riassume i risultati del calcolo col metodo di Burland e Burbidge per la condizione di carico 3, a cui corrisponde il cedimento immediato maggiore.

$$w = \sigma'_{vp} B^{0.7} I_c / 3 + (q' - \sigma'_{vp}) B^{0.7} I_c$$

Il cedimento w viene moltiplicato per $f_s f_t$.

Simbolo	Valore	Descrizione
z_{fon}	0 [m]	Quota di base della fondazione
B	3.425 [m]	Larghezza della base della fondazione
z_i	2.5669 [m]	Profondità di influenza
q'	0.038 [N/mm ²]	Carico unitario applicato
σ'_{v0}	0 [N/mm ²]	Tensione verticale geostatica alla quota della base
σ'_{vp}	0 [N/mm ²]	Tensione verticale di preconsolidazione alla quota della base
N	7	Valore medio di N_{spt} nella profondità di influenza
I_c	0.112	Indice di compressibilità
f_s	1.11	Coefficiente per la forma della fondazione
f_t	1.50	Coefficiente per il cedimento differito (30.0 anni)

Il cedimento immediato è pari a 0.0113 [m].

Il cedimento differito a 30.0 anni, nel caso di carichi statici, vale 0.0169 [m] (Verificato).